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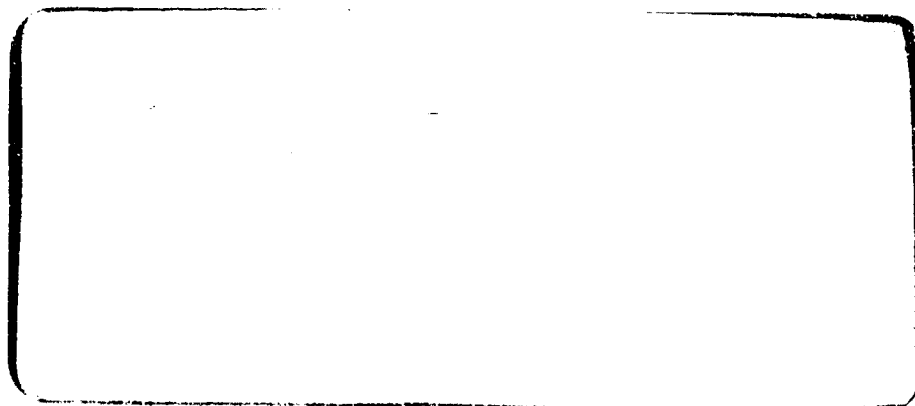
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COMPUTER ENGINEERING AND SCIENCE



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Investigation and Evaluation
of a Computer Program
to Minimize
Three-Dimensional Flight Time Tracks

NASA Grant NAG 3-101

FINAL REPORT

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**Investigation and Evaluation
of a Computer Program
to Minimize
Three-Dimensional Flight Time Tracks**

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15 September 1980 - 12 August 1981

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Frederic I. Parke

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**A Three-Dimensional Flight Planning
Model supporting for DC-10 Aircrafts**

GENERAL

The program for the DC8-D3 flight planning has been slightly modified for the three dimensional flight planning for DC10 aircrafts. Several test runs of the modified program over the North Atlantic and North America have been made for verifying the program in this project.

Reference is made to pages and formulas in 'Optimal Track Selection and 3-Dimensional Flight Planning' written by H. M. De Jong, No. 93.

MODIFICATION

1. Weather Information.

While Dr. De Jong used geopotential height and temperature in his program as a meteorological data, the modified program uses wind (direction and speed) and temperature received from National Weather Service.

A scanning program has been written to collect required weather information from the raw data received in a packed decimal format. Two sets of weather data, the 12-hour forecast and 24-hour forecast based on 0000 GMT, will be used for dynamic processes in our testruns. In order to save computing time only the weather data of the North Atlantic and North America is previously stored in a PCF file and then scanned one by one.

The element name (for weather data) of the PCF file is 'NWS' in our test runs.

Wind data is supplied in the form of grid point values of the vector wind

Vector wind is decomposed into x and y components to be applied to interpolation schemes.

Then it prepares spot values by interpolation with respect to the values of the wind components in the surrounding vertices of grid. See Fig. 1, Fig. 2 and Fig. 3.

2. Grid points.

While Dr. De Jong used weather data depicted from the grid points in a Cartesian grid superposed on a polar stereographic chart projection with standard parallel at 60 degree N, the modified program uses weather data depicted from the same grid points that National Weather Service uses.

See 'Aviation Digital Forecasts Program' issued by National Weather Service in Aug. 1978.

A blockette and grid points:

----- 7.5 degree

* *

* *

----- 0 degree

5 0

Each grid point contains its own weather data.

- a. In order to compute a great circle distance on earth between two points the following equation is used:

$$DIST = 60 \arccos(\sin LS \sin LD + \cos LS \cos LD \cos (RD - RS))$$

where LS=latitude of start,

LD=latitude of destination,

RS=longitude of start,

RD=longitude of destination,

DIST=great circle distance between start and destination.

(See equation 5.20, P. 64).

- b. To compute a true course it uses the following equation:

$$TC = \arccos((\sin LD - \sin LS \cos(DIST/60)) / (\sin(DIST/60) \cos LS))$$

{ if $\sin(RD-RS) > 0$ then $(360-TC)$ } is used

where TC= true course in degree.

- c. Computation of a drift angle uses the following equation:

$$DA = \arcsin(WV \sin(WD - TC) / TAS)$$

where DA=drift angle,

WD=wind direction (true)

WV=wind velocity,

TAS=true air speed.

- d. Heading= TC + DA (in degree).

3. Performance data for DC10.

- a. Specific range table as a function of weight and latitude.

This is an important economic index which is the air distance covered by a turbo-jet aircraft per unit of fuel consumption.

This data is almost independent of temperature and depends on the aircraft weight only at a prefixed flight level.

See table 1, P.116 and Fig. 4 in this documentation.

- b. Climb time table as a function of temperature and weight.

See Fig. 5

- c. Climb distance table as a function of temperature and weight.

See Fig. 6.

- d. Climb fuel table as a function of temperature and weight.

See Fig. 7.

- e. Max. weight table as a function of flight and temperature.

The maximally allowable weight depends on flight altitude and temperature deviation from standard.

See Fig. 4.

- f. Parameter r_1 and r_2 (See table 2. P. 116).

Parameter r_1 and r_2 are derived from the specific range table.

Here r_1 and r_2 denote the coefficients of a straight line fit in a (weight, $1/\text{entry value}$) graph at constant pressure altitude.

According to the specific range table for DC10 performance data,

r_1 and r_2 are as follow:

flight level	r_1	r_2
310	2.966	0.0000722
350	0.85	0.0000792
390	-0.83	0.0000890

- g. Extra burns for step-up and step-down.

While extra burn parameters for DCB-D3 were 100 kg/ 4000 ft for step-up and -80 kg/ 4000 ft for step-down, the new program uses 700 kg/4000 ft for step-up and -28 kg/4000 ft for step-down for the DC10 flight planning.

- h. The equations (6.31) in p. 121 and (6.33) in p.123 will be used in our test runs, since precisely matched parameters for DC10 are not available now.

(See lines 874-879 and 1305-1313 of the new program).

1. Initializing Input Parameters.

FLUR= sequence number.

TAXI= taxi fuel(kg).

GRW= zero fuel weight(kg).

RESERVE= reserve fuel(kg).

TOW= If -1, then computation starting in end point of flight.

MAXTOW= max. takeoff weight(kg).

MAXLW= max. landing weight(kg).

DATE= date/month/year.

IO= If -1, then east bound flight.

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TTT= time of departure.

ROUTE= route indicator.

ST= starting graph point number.

ST1= destination number.

Note: These input parameters are read from card images of the
PCF file in our testruns (element name = DC10F).

But these may be read directly from cards.

3. Output Values.

* See output listings.

NO.=graph point number.

HEAD= heading in flight (degree).

FL= flight level in 100 ft.

TMP= off standard temperature in centigrade degrees.

TAS= true air speed (n.m).

WIND=wind along the track (+ = tail, - = head).

DIST= distance of flight segment.

ACCD= accumulated distance flown(n.m).

TIME=time along the segment flown.

ACCT= accumulated time (hour, min).

BURN= fuel consumed in segment (kg).

WEIGHT= weight (kg).

TOC= top of climb.

TOD= top of descent.

a. Reviews on Test Runs.

Since Dr. DE Jong already proved that a solution in 3-space would reward as compared with a 2-space solution, we will not treat the factorized 2-space optimization case and the prescribed track case. Thus we will concentrate on test runs about pure 3-dimensional flight planning in free space.

While average CPU time for one flight plan with the modified program is approximately 120 seconds on UNIVAC 110B, the original program takes approximately 110 seconds or more for one flight plan on UNIVAC 110B.

However, for more than one flight plan it would require less than two minutes per one flight plan with the modified program, since they can share precalculated results for the weather information.

Note: In our test runs, two different sets of weather data and performance data will be used.

Weather data. (1) geopotential height and temperature,

(2) wind (speed, direction) and temperature.

Performance data:

(1) for DC8-D3:

standard cruise,

regularity 3 %

Mach 0.8034

taxi fuel 1500 kg

Zero fuel 75000 kg

reserves 10000 kg

max. takeoff wt. 142900 kg

max. landing wt. 93000 kg

(2) for DC10:

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standard cruise.

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regularity 3 %

Mach 0.82

taxi fuel 842 kg

zero fuel 177356 kg

reserves 3629 kg

max. takeoff wt. 259458 kg

max. landing wt. 190964 kg

a. Test runs of the original program (for DCB-D3).

(1). Test run #1.

(a). Input parameters.

start-destination: New York - Amsterdam (east bound)
 weather data: geopotential height and temperature
 performance data: DCB-D3
 flight level r1 r2
 31000 4.94 0.0000693
 35000 0.54 0.0001043
 39000 -0.65 0.000117
 extra burn: step up 100 kg/4000 ft
 step down -80 kg/4000 ft

(b) Output

* See Fig. 8.

criterion	trip fuel	cost	time	distance
min. cost	36398 kg	9914	6h 51m	3705 n.m
min. time	39931 kg	10359	6h 43m	3205 n.m

* routes taken: same route

115-113-108-103-97-91-87-77-66-52-37-21-11-6-2-0

(c). Remarks.

The original program written in Burrough ALGOL has been converted for use in UNIVAC 1108.

Test run results which come from the converted program are just identical to those obtained from the original program, assuming use of same input parameters.

(2). Test run #2.

(a). Input parameters.

start-destination:	New York - Amsterdam (east bound)
weather data:	zero wind and standard temperature
performance data:	DCB-D3
r1 and r2:	same as in test run #1
extra burn:	same as in test run #1

(b). Output.

* See Fig. 9.

criterion	trip fuel	cost	time	distance
min. fuel	38327 kg	10357	7h 05m	3193 n.m

* route taken:

115-113-108-103-97-91-87-76-64-50-36-21-11-6-2-0

(c). Remarks.

To run the program under zero wind and standard temperature is a kind of minimal check.

The optimal track should then consist of the 'optimal operational distance track' in the graph as a good approximation of the great circle track between the end points.

The results of test run #2 shows a slightly different route as compared with that obtained in the test run #1.

The results should be unaffected when the program is run for a flight in opposite direction between the same points (west bound versus east bound). See table 11, P. 128.

b. Test runs of the modified program.

(1). Test run #3.

(a). Input parameters.

start-destination: New York - Amsterdam (east bound)

weather data: zero wind and standard temperature

performance data: DCB-D3

flight level	r1	r2
31000	4.94	0.0000693
35000	0.54	0.0001043
39000	-0.65	0.000117

extra burn. step up 100 kg/4000 ft

step down -80 kg/4000 ft

(b). Output.

* See Fig. 10.

criterion	trip fuel	cost	time	distance
min. fuel	38225 kg	10335	7h 05m	3128 n.m

* route taken:

115-113-108-103-97-91-87-76-64-50-36-21-11-6-2-0

(c). Remarks.

Let us compare test run #3 with test run #2.

These test runs with same input parameters should show close results for the optimal operational distance track as shown

in Fig. 37. P.110.

Both test run #2 and #3 have same route between New York and Amsterdam.

program	criterion	fuel	cost	time	distance
original	min. fuel	38327	10357	7h 05m	3193 n.m
modified	min. fuel	38225	10335	7h 05m	3188 n.m

Differences in results may be attributed to the use of different formulas for computing segment distance and true course, and round of errors.

Thus we know that the modified program works correctly under this minimal check.

(2). Test run #4.

(a). Input parameters.

start-destination:	New York - Amsterdam (east bound)
weather data:	wind and temperature
performance data:	DC8-D3
r1 and r2:	same as in test run #3
extra burn:	same as in test run #3

(b). Output.

* See Fig. 11.

criterion	trip fuel	cost	time	distance
min. time	34273 kg	9015	5h 58m	3192 n.m

* route taken:

115-113-108-103-97-91-87-77-65-51-37-21-11-6-2-0

(c). Remarks.

Let us compare test run #4 with test run #1.

These test runs were executed under conditions having standard cruise, Mach=0.8034, New York - Amsterdam (east bound), DCB-D3 performance data, and min. time criterion.

test run	weather	fuel	cost	time	distance
testrun#1	geopotential	39931	10359	6h 43m	3205 n.m
testrun#4	wind	34327	9015	5h 58m	3192 n.m

Differences in results are attributed to the use of different weather data set.

The difference in flight time implies the test run #4 used weather data set with almost east bound wind along the track. It is reasonable to have faster flight in the test run #4 than in the test run #1 since as you see in Fig. 11, an aircraft to fly may experience only tail wind along the planned track.

(3). Test run #5.

(a). Input parameters.

start-destination:	New York - Amsterdam (east bound)
weather data:	wind and temperature
performance data:	DC10
r1 and r2:	same as in test run #3
extra burn:	same as in test run #3

(b). Output.

See Fig. 12.

criterion	trip fuel	cost	time	distance
min. time	48787 kg	11129	5h 52m	3192 n.m

* route taken:

115-113-108-103-97-91-87-77-65-51-37-21-11-6-2-0

(4). Test run #6.

(a). Input parameters.

start-destination: Amsterdam - New York (west bound)

weather data: wind and temperature

performance data: DC10

r1 and r2: same as in test run #3

extra burn: same as in test run #3

(b). Output.

* See fig. 13.

A strange symptom occurs: A negative segment flight time and a negative fuel burn between graph point number 0 and 1.

Thus we temporarily add one statement in line #884 to avoid this negative magnitude.

Let us make another test run with this added statement under same conditions (test run #7).

(5). Test run #7.

(a). Input parameters: same as in test run #6.

(b). Output.

* See Fig 14.

criterion	trip fuel	cost	time	distance
min. time	68447 kg	15383	7h 52m	3283 n.m

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* route taken:

0-1-4-8-17-30-44-60-75-87-92-98-104-109-113-115

(c). Remarks.

Let us compare test run #5 with test run #7.

These test runs are made under following conditions:

DC10 performance data, wind and temperature and same start-destination.

test run	bound	trip fuel	cost	time	distance
#5	east	48789 kg	11129	5h 52m	3192 n.m
#7	west	68447 kg	15383	7h 52m	3283 n.m

The west bound flight takes 2 hours more in flight time as compared with that obtained in east bound flight.

This is caused by the strong east-bound wind trend in weather data and longer flight distance in west bound route taken.

(7). Test run #8 and #9.

(a). Input parameters.

start-destination: New York - Amsterdam (east bound)

weather data: wind and temperature

performance data: DC10

flight level	r1	r2
31000 ft	2.366	0.0000722
35000 ft	0.35	0.0000792
39000 ft	-0.83	0.000089

extra burn: step up 700 kg/4000 ft

step down -28 kg/4000 ft

(b). Output.

* See Fig. 15 and 16.

criterion	trip fuel	cost	time	distance
min. fuel	49952 kg	11320	5h 53m	3192 n.m
min. time	51129 kg	11480	5h 52m	3192 n.m

* routes taken: same route

115-113-108-103-97-91-87-77-65-51-37-21-11-6-2-0

(c). Remarks.

These test runs show that the min. fuel flight plan gains 1177 kg of trip fuel and loses 1 minute of flight time as compared with the min. time flight plan.

The gains may look inconsiderable.

But this is the result of one test run only.

Here another comment is made for optimal step altitude profiles.

The fuel and cost profiles have both the normal appearance:

Approximation of a continuous cruise climb with one or two 4000 ft steps. However, the min. time flight is more irregular.

This is caused by the response of the aircraft's speed to the vertical temperature gradients: The level of highest temperatures is sought.

As you see temperature values in Fig. 3, some higher altitude levels have unexpectedly lower temperature values, for example, around graph point numbers 87, 77, 37, 21, 2 etc.

(2). Test run #10 and #11.

(a). Input parameters.

start-destination: New York - Amsterdam (east bound)

weather data: wind and temperature

performance data: DC10

flight level r1 r2

31000 ft 2.966 0.0000722

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35000 ft	0.85	0.0000792
39000 ft	-0.83	0.000029

extra burn: step up 700 kg/4000 ft
 step down -28 kg/4000 ft

(b). Output.

* See Fig. 17 and 18.

criterion	trip fuel	cost	time	distance
min. fuel	49948 kg	11319	5h 53m	3192 n.m
min. time	51118 kg	11479	5h 52m	3192 n.m

* route taken:

115-113-108-103-97-91-87-77-65-51-37-21-11-6-2-0

(c). Remarks.

We used slightly different r_1 , r_2 -parameter sets to see how they affect flight plannings in this test run.

When we see test runs, #8, #9, #10 and #11 we understand that there is no significant difference in results under slightly different r_1 , r_2 parameter sets.

(9). Test run #12.

(a). Input parameters.

start-destination:	Amsterdam - New York (west bound)
weather data:	wind and temperature
performance data:	DC10
r_1 and r_2 :	same as in test run #10
extra burn:	same as in test run #10

(b). Output.

*See fig. 19.

criterion	trip fuel	cost	time	distance
min. fuel	69928 kg	15667	7h 58m	3283 n.m

(c). Remarks.

In this test run we understand that there are significant differences in results mainly because of the east bound wind tendency in the weather data set used.

criterion	bound	fuel	cost	time	distance
min. fuel	east	49948	11319	5h 53m	3192
min. fuel	west	69928	15667	7h 58m	3283

(10). Test run #13.

- (a). Input parameters: same as in test run #12 except the following:
- 60 % of vector wind for mean climb vector,
 - 4 minutes for take-off and acceleration.

(b). Output.

* See Fig. 20.

criterion	trip fuel	cost	time	distance
min. fuel	70404 kg	15769	8h 01m	3283 n.m

*route taken:

0-1-4-8-17-30-44-60-75-87-92-98-104-109-113-115

(c). Remarks.

We made some modifications on climb distance computation to avoid the negative magnitude as described in the test run #6.

We took 60 % of vector wind instead of 75 % for the mean climb vector wind (See line #882-883 of the program listing).

The climb time is usually reduced by a few minutes to account for take-off and acceleration. We took four minutes for it in

this test run (two minutes taken in test run #12).

Then let us see how modifications affect the flight plannings.

test run	criterion	fuel	cost	time	distance
#12	min. fuel	69928	15667	7h 58m	3283 n.m
#13	min. fuel	70404	15770	8h 01m	3283 n.m

It shows that the test run #13 requires slightly more cost and time than the test run #12, but not significantly.

Graph point #1 has Dist=10, Time=1, and burn=200 in this test run instead of zeros.

EXTRA COMMENTS FOR THE MODIFIED PROGRAM.

** 54-334

Procedure WDATA scans weather data received from National Weather Service and obtains the required weather information for North Atlantic and North America area.

(see the weather data format in Operational Manual issued on 9/19/78 and Aviation Digital Forecasts Program issued in Aug. 1978, by National Weather Service).

The weather data received in packed decimal format is supplied in the form of grid point values of the vector wind and temperature.

* 72-35

Procedure CHOP cuts a piece of weather information from the whole weather data for a specified grid point.

* 89-116

Procedure STOR prepares a two dimensional array (120x34) for the weather information and stores the chopped weather data

in the array according to the standard pressure levels, i.e., 300 mbar, 250 mbar, 200 mbar etc.

* 119-133

Procedure AREA gets the header information of the weather data, i.e., area number, blockette number etc.

* 136-142

Procedure FINDNEXT checks the end of the weather data block.

* 145-213

Procedure GETDATA stores the weather data of each grid point in the prepared array according to GMT time, standard pressure level, area number, and blockette number.

* 216-225

Procedure SCAN activates the scanning procedures.

* 229-253

Procedure WINDCOMP decomposes a vector wind into x and y components.

* 257-262

Procedure INTP contains a formula for linear interpolation.

* 267-276

This routine prints out the weather data which are stored in the array space.

(One may delete this routine if not needed).

* 281-313

This routine converts the weather data in the standard pressure levels to the weather data in flight levels by using the interpolation formula.

* 315-332

This routine prints out the converted weather data above.

(only x component of vector wind and temperature).

One may delete this routine if not needed.

* 336-340

Initial values:

CG= conversion factor between degree and radian.

MACH= 0.82 for DC10.

P1,P2,P3= flight levels.

Q1,Q2,Q3= pressure altitudes for standard pressure levels.

* 350-353

The graph points are labelled by numbers running from 0 to 115 (note that the graph point numbers shown in Fig. 37, P. 110 runs from 1 to 116).

The graph is such that the point sets consist of subsets of points arranged along 'Meridians' whose indices run from 0 to 15.

Array A(index) contains the graph point number assigned to the most northerly point on each meridian.

Array A is used for the computation of zone index (See the procedure ZONEI).

* 358-372

Array V has values assigned for geographic coordinates for graph points and check points on continents: 4-digit latitude 4-digit longitude in degrees and hundredths.

(See Fig. 37, P. 110).

* 376-381

This routine fills Boolean array BK and BKQ with 'TRUE'.

* 382-395

This routine denotes blocking in continental airways.

(connectivity in the graph).

Boolean array entries of BK and BKG indicate which graph points are connected or blocked (TRUE=blocked, FALSE=connected).

Array BK is used for the zone index < 3 and array BKG is used for the zone index > 8 .

BK(a,b,c)=FALSE means point b on meridian a is connected with point c on meridian a+1.

Here point b denotes the b-th point from the bottom on the meridian. Example: BK(2,2,2)=FALSE means graph point number 3 on meridian 2 is connected with graph point 5 on meridian 3 as you see Fig. 37.

* 405-414

Procedure ZONEI determines the index of the zone associated with a graph point number.

Parameter Q=graph point number.

For example, a graph point number 49 gives ZONEI(49)=6.

* 416-424

Procedure DT dissects latitude and longitude from the compressed coordinates. LALAT and LALONG denote latitude and longitude respectively. Parameter K is an index of array V.

* 426-459

Procedure LIS determines actual latitude and longitude values for a graph point. (See procedure DT above).

The sign of longitude value is changed in the east of Greenwich.

Parameter U=graph point number.

* 461-480

Procedure CTG prepares a time instant array DD, zonally specified, to be used for the time interpolation later on.

A=0.4 denotes an estimated flight time of 24 minutes per continental zone.

The instant values run from index 0 to index 14.

*484-498

Procedure HH computes grid point values according to SELECT value

If SELECT=1 , HH gets x-component value of vector wind

If SELECT=2 , HH gets y-component value of vector wind.

If SELECT=3 , HH gets temperature value.

These values are computed under consideration of time factor for dynamic process.

Parameter V and W denote array index numbers for row and column respectively. Parameter F=index for flight levels (31000 ft=1, 35000 ft=2 and 39000 ft=3).

* 503-523

Procedure GEOP computes x and y component values of vector wind and temperature value for an arbitrary point by using procedure HH above. Bi-linear interpolation scheme is used in this computation. Parameter C=flight level index.

* 528-538

Procedure GEODIS computes a great circle distance between two arbitrary points P1(LAT1,LON1) and P2(LAT2,LON2).

* 543-550

Procedure GEOMGRID converts coordinates of two arbitrary points on sphere to their coordinates on the geometric grid. PP and GG denote two grid point numbers.

* 555-638

Procedure PART2GEO computes length of segment by summation of

contribution from subsegments (LENGTH(I)) and a true course angle of a flight segment.

E1 and E2 denote unit vectors for the true course.

Normalized coordinates (running from 0 to 1) are stored in array AB.

These values serve also as weighting factors later on.

Array LENGTH(I) contains lengths of subsegments on the sphere.

*640-658

These two procedures are summation formulas.

* 662-684

Procedure DRIFT computes a drift angle by using x,y components of vector wind.

** 687-741

Procedure METPROC processes meteorological data before optimization process later on.

Parameter S=flight level index.

* 695-705

This routine computes average weather parameters for each subsegment.

* 706-708

This routine computes average weather parameters for each segment in order to get single drift angle of the segment.

* 711-716

This routine computes flight time in each subsegment.

* 717-740

This routine computes temperature deviation, flight time, air distance, flight heading, x,y components of vector wind,

and x,y components of true air speed in each segment and flight level.

These computed values are all average values along a segment under consideration using previously calculated contributions.

TEM=temperature.

TDEV(S)=temperature deviation.

TIME(S)=flight time in flight level index S.

AIRDIST(S)=air distance.

LE=distance of flight segment.

WIX(S)=x component of vector wind.

TAX(S)=true air speed component.

* 745-785

Procedure TABLE and CLIMBCORT are table lookup procedures for picking up performance data for DC10.

* 787-830

Procedure READQ reads in performance data and procedure WRITEQ writes out those inputted data.

One may delete procedure WRITEQ and lines 813-830 if not needed.

* 833-862

This routine reads in input parameters for a flight planning. In case of prescribed track flight (ROUTE >= 1111 case), the routine reads in Q.

In another case, it reads in S1(starting point number) and S2(end point number) and decides Q value.

Q= # of graph points on the prescribed route or (# of zones between source and destination) - 1.

* 861-864

Procedure SQ and JQ are conversion formulas for indices used in subsegment algorithms by using array A(index) and array F(index) respectively.

* 866-889

Procedure DESCLIMB computes performance by using the table lookup procedure in climb(if MG=0) or descent(if MG not= 0). The calculation is somewhat complicated by the fact that the location of TOC is not fixed. The position where the flight levels off may vary due to the influence of the winds in the climb phase.

For mean climb vector wind we may take 60 or 75 % of the vector wind and the climb time is usually reduced by a few minutes to account for take-off and acceleration and thus we may take 2 minutes for it.

Array DECLTIME contains climb time or descent time.

Array DECLDIST contains climb distance or descent distance.

Array DECLFUEL contains climb fuel or descent fuel.

Array AIRDIST contains climb air distance or descent air distance.

It is noted that in the descent zone, the performance table is not used and thus specific expressions are chosen according to company's planning policy.

(See formula 6.31 in P. 120-121).

* 892-933

Procedure LINE prints out a flight plan.

** 935-1242

Procedure SPACEOPT is a key procedure for optimization.

In this procedure, crucial is that some parameters may not surpass upper bounds, for example, aircraft weight.

This requires the inclusion of several protective statements in order to ensure proper functioning of the operational scheme.

FBQ determines whether the flight plan computation will be performed backward (FBQ=FALSE) or forward (FBQ=TRUE).

FB determines whether cost (FB=1), fuel (FB=0) or flight time (FB=-1) will be optimized.

BI determines whether the navigation regime is free in the horizontal (BI=FALSE) or bounded by one position (BI=TRUE).

BG determines whether the cruising altitude is free (BG=FALSE) or bounded (BG=TRUE).

RR is take-off weight or landing weight.

* 953-961

Procedure PREP computes distance and flight time, and prints out a line of flight plan.

A1=segment distance.

B1=segment flight time.

AA=TRUE denotes a climb phase and AA=FALSE a descent phase.

* 963-1010

Procedure EDITING prints out proper heading lines for a flight plan.

** 1012-1084

Procedure WQ computes segment contribution, fuel, etc.

If D=-1, computation is for in-flight direction and if D=+1, then computation is for opposite flight direction.

* 1018-1038

Procedure CL computes the aircraft weight (GRWG) and total fuel.

flight time or costs at end point of a flown segment.

(the contribution of fuel in steps included).

Parameter M1 denotes segment fuel(kg) and M2 segment time(min).

In the climb phase no step contribution is taken into account as required(BCLIMB=TRUE).

GG denotes flight level index at the graph point when the computation starts. G denotes the flight level index to be investigated.

Step consumption: UP=700 kg/4000ft

DOWN=-28 kg/4000ft.

(surplus of segment fuel)

ITERATION becomes TRUE when (1) back-tracking (2) first zone is reached.

(3) TOW is unknown and Wb is known (see P.120).

In array ROW the aircraft weight is stored.

GRWG denotes aircraft weight at the end point of segment.

QUANT denotes cost, fuel or time at the end point of flown segment.

*1045-1052

computation in climb or descent by procedure CL.

If ED is TRUE then it prints out the results.

*1055-1057

safeguarding statements.

*1060-1068

computes segment contribution of changes in aircraft weight.

Note that fuel consumption is expressed as loss of aircraft weight.

The table for specific range (P.116) is used.

Formula 6.27 (P.115) requires an estimate of weight halfway a flight segment. For that purpose coefficients as shown in table 2, P.116 are required (r1, r2).

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*1069

jumping back to label JM1 is for safeguarding that the actually derived aircraft weight does not surpass the maximally allowed weight.

*1071-1078

computes the contribution for the last segment.
If ED is TRUE then it prints out the results.

*1081

GRWG and QUANT attain absurd values for safeguarding operational performance.

*1087

ED becomes TRUE when all degrees of freedom in the horizontal and vertical are lost, for example when a call of procedure SPACEOPT takes place in the final mode for flight plan computation along the (optimal) track found in previous calls.
(when navigation regimes is bounded by one point and cruising altitude is bounded).

*1088-1113

Initialization and preparation of all parameters needed for the algorithmic process of optimization.

FBQ=TRUE means flight plan computation will be performed forwards, while FBQ=FALSE backwards.

Array F is filled in line 1244-1248 (see procedure FF).

The process can be activated for arbitray begin- and end-points.

In order to reduce storage space a renumbering is made for all subset points. So array F is defined and functions completely analogous to array A for whole graph point set.

Array STOREI and STOREIQ contain the assigned numbers of labelled

end-points on meridians in the subgraph.

Zone cycle runs from line 1115 to 1220.

The zone cycle repeats as many times as the number of zones.

A cycle for graph points along meridian runs from line 1122 to 1216.

This cycle repeats as many times as the number of graph points in the current meridian.

A cycle for graph points along next meridian runs from line 1127 to 1214.

This cycle repeats as many times as the number of graph points in the next meridian.

A cycle for flight levels runs from line 1158 to 1212.

This cycle repeats as many times as the number of flight levels used.

* 1126

conversion for indices used in subsequent algorithms.

* 1131-1151

If the navigation is free (BI=FALSE) in the horizontal, it checks whether a segment (II, JJ) is blocked or not.

BK or BKQ = TRUE means airway is blocked.

If blocked, it skips computation for the segment.

* 1152-1156

conversion for indices (point G4).

determines geographic elements for a segment between points G3 and G4.

See procedures GEOMGRID and PART2GEOM.

* 1162-1191

In case of backtracking in a flight plan computation an iteration process is put into action in the climb zone

This is done in order to determine the (unknown) take-off weight by iteration in such a way that the climb parameters do match with the

parameters found during backtracking when arriving in the climb zone. The iteration starts with a take-off weight 20000 kg below the (known) maximum take-off weight.

Array ROW contains the (optimal) value of aircraft weight found during optimization, using a zone-cycle.

The iteration finishes when either the weight difference at the point of matching is less than 10 kg or the number of iteration steps exceeds 10 (poor convergence).

In each step take-off weight is adjusted, see line 1181-1191.

* 1195-1203

similar computations but not backtracking case or not take-off weight adjustment case.

* 1204-1210

These statements are crucial optimization criteria.

* 1225-1241

Preparation of elements which are required for a subsequent call for procedure SPACEDPT with lessened number of degrees of freedom including a final call for computation and presentation of flight plan data. In this final stage no degrees of freedom are left. Procedure SPACEDPT then merely operates along a predefined track (the solution of previous calls).

* 1244-1248

Procedure FF determines a zone index array F for a subset of graph points analogous to array A. (array F is a sub-zone array).

** 1250-1351

A call for procedure PROCES results in the production of a flight plan along whatever route is desired.

DETAILS

*1275-1289

Specification of limits in horizontal of graph points along meridians.

Array STOREI and array STOREIG store lower limits and upper limits respectively for the number of graph points on each meridian.

If route ≥ 1111 , then production of flight plan along a prescribed route.

In this case the procedure SPACEOPT works in a degenerate mode.

* 1291-1296

Specification of limits in the vertical.

Array STOREG and array STOREGG store lower limits and upper limits respectively for the number of flight levels on each meridian.

*1298-1303

Procedure EP indicates that the flight planning computation blows up.

* 1305-1316

See P. 123-124 for procedures SS, SSS and SSSS.

These procedures compute landing weights.

NN contains landing weight or take-off weight.

* 1318-1324

Procedure TW is for safeguarding against overloading.

* 1327-1351

activates process as follow:

If FACTORIZAION is TRUE, then the optimization takes place first in the horizontal and is followed by an optimization in the vertical.

The following steps occur:

a) optimization in the horizontal based on time.

(b) optimization in the vertical, using the track solution found in (a) and based on fuel, time or costs.

(c) computation of flight plan along solution found in (b).

If the optimization takes place in free space, the sequence of calls results in: (three procedure calls)

(i) optimization in space based on time, fuel or costs.

(ii) optimization in the vertical through horizontal track found in (i), based on time, fuel or costs.

(iii) compilation flight plan along track solution found in (ii).

Note: (ii) could be bypassed as the solution is found already in (i). But (ii) can be generated with a slightly different landing weight. The compilation of a flight plan along a prescribed route passes through all three procedure calls.

This means that in fact the computation is repeated threefold, however with properly tuned landing or take-off weights.

In order to protect against subsequent calls of procedure PROCES, ROUTE is assigned by 1000.

→ 1353-1364

Read statement in case that a flight plan compilation is desired along a prescribed track.

This track is specified by graph points indicated by their numbers.

→ 1365-1369

Computation of an estimate of flight time to be used for the estimation of other parameters.

The same with distance.

Procedure CIG makes time instant array DD for each zone(meridian).

Array E is for storing the number of graph points used on a meridian.

→ 1371-1389

performs a process for the production of a flight plan.

Actual parameters when calling procedure :

use landing weight (BB=TRUE).

cost optimization (FFBB=1).

FFBB=0 means fuel opt. FFBB=-1 means time opt.

regularity percentage (PR=0.03).

flight levels used between S1=1 for 31000 and S2=3 for 39000.

S3=1; the value is immaterial if FACTORIZATION is FALSE.

For required flight plans :

1. when a flight plan for the optimal cost track is needed,
call 'proces (1,3,1,0.03,1,TRUE,FALSE)'.
2. when a flight plan for the optimal fuel track is needed,
call 'proces (1,3,1,0.03,0,TRUE,FALSE)'.
3. when a flight plan for the least time track is needed,
call 'proces (1,3,1,0.03,-1,TRUE,FALSE)'.

For the flight plan 1, 2 or 3 above, FACTORIZATION=FALSE.

For other flight planning simulations, FACTORIZATION=TRUE.

Fig. 1-1.

* WEATHER DATA IN 3 STANDARD PRESSURE LEVELS *
 * 34X16 DATA OUT OF 34X20 GRIDPOINTS *
 * TEMPERATURE, DIRECTION, SPEED *

3127023	3327027	3426034	3526046	3525056	3624060	3723066	3822070	4022073	4222076	4321075	4421071	4520068	4621063	4821062	4822055
3231027	3330026	3430031	3529037	3627040	3626041	3725044	3824046	3924048	4123052	4223055	4322056	4422056	4522057	4623061	4724061
3433035	3333037	3432044	3532048	3632049	3732048	3831042	3930034	3928029	4026031	4224036	4224038	4324041	4424045	4525054	4625061
3432043	3532051	3632057	3832061	3932064	3934054	3934037	4035019	4029006	4124020	4125032	4225040	4326042	4426046	4427056	4527067
3329049	3630044	3930041	4130041	4230032	4234015	4206018	4107025	4008017	4031003	4127024	4227042	4227049	4328054	4428063	4528076
3426046	3626035	3926033	4226033	4325022	4319005	4209017	4107024	4005024	4001023	4133029	4133060	4331072	4431081	4531089	4630092
3423049	3624050	3825043	4025037	4224027	4324009	4205008	4203018	4101028	4136037	4134047	4233060	4331072	4431081	4531089	4630092
3324040	3525063	3726064	3926051	4126037	4230022	4334026	4433048	4434060	4435073	4535085	4534092	4634098	4733102	4832098	4933094
3325029	3525060	3726076	3926072	4128056	4330044	4333048	4434060	4435073	4535085	4534092	4634098	4733102	4832098	4933094	5032088
3225028	3326054	3526078	3827086	4228077	4429065	4430061	4532064	4633072	4634082	4635089	4634093	4734094	4833092	4933085	5033074
3027031	3227054	3426077	3727089	4127084	4327076	4527071	4628063	4729053	4730045	4732044	4733048	4833052	4833054	5033052	5133048
3029029	3227042	3426064	3726081	4225077	4525071	4625068	4825063	4924058	5024052	5024043	5125033	5127026	5229024	5330023	5430027
3230028	3330033	3428047	3627063	3825069	4125072	4324071	4624066	4823063	4923064	5123068	5223070	5323065	5324051	5424036	5525027
3231036	3331036	3530035	3527039	3625051	3924065	4223072	4523073	4822071	4922073	5022078	5223084	5223083	5224071	5324050	5524037
3330030	3531022	3531014	3528014	3625027	3723044	3923062	4222078	4421091	4521099	4722105	4922110	4923108	4923091	4924085	5223048
3426013	3522007	3617005	3621005	3622015	3622027	3722040	3822056	3921074	4021092	4222109	4322124	4423129	4423116	4523092	4822071
3332006	3430007	3631009	3731007	3825007	3823013	3722021	3722032	3722046	3722064	3822084	4022105	4123123	4123128	4223114	4423097
3434016	3634013	3833002	3915011	3917018	4018024	3920025	3822027	3723032	3723041	3723053	3723072	3823094	3923112	4023116	4223110
3605005	3812013	3913025	3914028	3815024	3817024	3820025	3822030	3824034	3724037	3624042	3625052	3725069	3725090	3925105	4024111
3711022	3712029	3712029	3611021	3610015	3611011	3721006	3725020	3726033	3726038	3726041	3726047	3726059	3726074	3826091	4026106
3808025	3808033	3708026	3506019	3503023	3602028	3736031	3734037	3732042	3731044	3730044	3729050	3729058	3728070	3828046	4027103
3803009	3805032	3706032	3603020	3601021	3701027	3736039	3834052	3834058	3833059	3833059	3732063	3731071	3833081	3933085	4129110
3728024	3703019	3704035	3702032	3701032	3736042	3735053	3734065	3834082	3834089	3833093	3833100	3932104	4131115	4331117	4331117
3626052	3729026	3736033	3736050	3735072	3735101	3735116	3835123	3835127	3835129	3935131	3934131	4034130	4133126	4433117	4632104
3526070	3627054	3730050	3932056	4133078	4134100	4135118	4235127	4335128	4335126	4335123	4235118	4335111	4534098	4734082	4933064
3326072	3526071	3727063	3928070	4328079	4529071	4631058	4833053	4834054	4835056	4835055	4836051	4836046	4935039	5035027	5232016
3326067	3426076	3726072	3926075	4225094	4625098	5025081	5225054	5324031	5323016	5224008	5224003	5109002	5212007	5316013	5318021
3425058	3525075	3625075	3924073	4224083	4524096	4824097	5023084	5222065	5421050	5420041	5319036	5318031	5317031	5316035	5318040
3524038	3625063	3625074	3724071	4024073	4324080	4523087	4723089	4922082	5121075	5220073	5219073	5319065	5318057	5217054	5218054
3726022	3726045	3725061	3724066	3924070	4124072	4324070	4523070	4722072	4821076	4920082	4920085	5019079	5019070	5018063	5019059
3729026	3728039	3627048	3727059	3826065	3926061	4125050	4224042	4422045	4521052	4621060	4721064	4821064	4820061	4820056	4921053
3531033	3530044	3530055	3630059	3729052	3828041	3926032	4125025	4224023	4424025	4524030	4624035	4723037	4822038	4822038	4924043
3632043	3631055	3631063	3731059	3831050	3930041	4030035	4130032	4331031	4431030	4531028	4730025	4828023	4928022	5028028	5028043
3732045	3831054	3930058	4031055	4032053	4132048	4232047	4332044	4533039	4733033	4833027	4933023	5032021	5131023	5230031	5229045

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Fig. 1-2.

* WEATHER DATA IN 3 STANDARD PRESSURE LEVELS *
 * 34X16 DATA OUT OF 34X20 GRIDPOINTS *
 * TEMPERATURE, DIRECTION, SPEED *

4227033	4327035	4426040	4426051	4425062	4424071	4523080	4623086	4822088	4922086	5022081	5121073	5121069	5221065	5221063	5122053
4331031	4330029	4429036	4528042	4527044	4526048	4626053	4725056	4824057	4923059	5023060	5122060	5221060	5322062	5322062	5223059
4434039	4433041	4432049	4532055	4532057	4632057	4731053	4830044	4929036	5026035	5125039	5224040	5324042	5324047	5325055	5225059
4531044	4532057	4632068	4732074	4833076	4734064	4834064	4935024	5030011	5025022	5125035	5225041	5226044	5326049	5327059	5327068
4229054	4529054	4830053	5030052	5031041	5034020	4906024	4907030	4907019	5030006	5127029	5127045	5227052	5328059	5428070	5429080
4326053	4525047	4826045	5026042	5125026	5216002	5108025	4907035	4905033	5001029	5132037	5230051	5229063	5329072	5429083	5429091
4324057	4428060	4725055	4924048	5124033	5224009	5206015	5004028	5002037	5136046	5234057	5331079	5431089	5530096	5530096	5530096
4324052	4525074	4625074	4825062	5026046	5229025	5235026	5236040	5235053	5335067	5334080	5333092	5433101	5432105	5432103	5431095
4425041	4525071	4625088	4726086	5127068	5330047	5333047	5334060	5334075	5435086	5434094	5434102	5433108	5433107	5332098	5332085
4225037	4326063	4426089	4727101	5027091	5229070	5330061	5232063	5233069	5234075	5234080	5234088	5233086	5233086	5233078	5233068
4027036	412061	4327086	4527101	4827096	5127084	5228073	5228083	5129053	5130044	5032041	5033043	5033046	5033048	5133048	5133044
4129032	4227047	4326074	4426093	4626094	4925088	5225080	5325071	5325063	5224055	5224048	5224039	5125029	5127024	5129023	5230024
4230023	4229033	4328055	4326077	4525087	4825087	5124082	5224074	5323067	5323066	5323067	5423066	5323059	5324047	5324034	5325027
4032037	4231042	4330044	4327047	4325059	4624074	5023081	5222081	5222077	5222078	5322082	5322085	5323081	5223069	5224052	5323039
4031040	4232036	4332028	4330023	4326029	4523046	4722067	4922084	5021099	5121109	5122116	5222117	5123111	4923094	5023071	5223055
4126023	4324014	4522005	4525005	4625015	4523027	4622042	4622060	4721081	4821103	4922123	4922137	4822137	4722122	4723099	4922079
4228013	4428015	4530015	4632012	4628010	4625012	4623020	4522032	4522048	4622068	4622091	4722113	4622129	4623130	4623116	4823101
4533030	4732026	4731014	4817004	4818016	4819023	4720024	4722025	4623031	4523041	4523055	4523076	4523097	4623112	4623116	4723114
4732010	4813006	4814024	4814031	4715030	4717030	4719030	4722031	4624032	4524035	4425042	4425055	4525073	4525092	4725108	4824119
4612018	4712030	4712031	4612023	4611015	4612010	4622009	4625021	4626031	4626035	4526039	4526048	4526062	4526078	4726098	4826119
4608019	4708032	4708027	4606019	4503024	4502029	4636031	4634037	4632042	4631044	4630044	4529050	4529060	4528075	4628097	4827122
4732006	4806028	4706032	4503020	4501020	4501024	4535035	4534050	4534060	4533061	4532060	4532063	4531074	4630049	4730110	4829131
4627032	4601014	4704033	4602031	4601028	4635035	4534049	4533065	4534076	4534085	4534091	4633096	4633104	4732115	4831127	4931133
4426060	4529032	4636035	4736057	4735082	4735105	4635117	4735125	4735133	4635138	4635138	4735137	4734134	4833130	4933124	5032112
4326079	4426064	4629046	4832061	4934092	4834113	4735125	4835135	4935138	4835135	4835129	4835121	4835113	4934101	5034087	5133069
4125080	4226084	4427073	4728072	4928077	4929073	4931063	4933057	5034058	5035059	5035057	4936054	4936049	5035042	5135032	5233021
4126072	4126088	4326087	4526083	4825094	5125096	5225079	5225053	5224030	5224014	5124005	5101002	5104004	5109004	5216008	5319017
4526060	4425080	4425088	4625088	4824096	5124106	5324103	5423088	5322068	5321051	5220040	5219032	5218027	5217027	5417032	5518038
4626043	4625065	4525077	4624082	4824087	5024092	5323097	5423096	5522086	5421076	5420071	5319068	5319061	5318054	5518054	5718056
4526033	4526049	4525062	4525071	4724080	4924082	5124078	5423075	5522075	5521079	5620084	5620086	5620079	5519070	5619066	5819064
4527028	4427040	4427052	4527063	4626068	4726063	4924054	5023050	5222053	5421059	5521065	5621068	5721067	5720064	5820060	5921058
4632032	4430046	4430062	4429066	4429058	4528051	4627043	4825037	5025034	5224033	5424036	5524040	5724043	5823042	5923041	6024046
4533056	4532067	4531076	4631073	4631063	4731053	4831044	4931040	5031040	5131041	5331039	5530035	5729032	5928030	6029034	6028046
4532056	4531064	4631069	4831067	4932065	5033059	5033056	5133052	5233047	5333040	5433032	5633025	5931027	5931035	5930047	

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Fig. 1-3.

- * WEATHER DATA IN 3 STANDARD PRESSURE LEVELS *
- * 34X16 DATA OUT OF 34X20 GRIDPOINTS *
- * TEMPERATURE, DIRECTION, SPEED *

5427050	5527051	5626048	5626052	5425070	5524085	5524098	5623104	5723102	5722093	5622080	5421066	5321058	5321054	5222052	5123046
5431039	5529040	5528043	5628042	5528044	5527055	5626066	5625071	5725071	5824070	5823065	5722060	5622056	5522054	5423053	5324051
5434043	5533046	5631054	5631058	5632060	5732063	5731060	5830051	5929043	6027040	6125041	6124041	5924042	5824044	5725049	5525052
5531049	5532063	5632075	5732078	5733077	5633065	5734074	5834029	5931018	6127024	6226036	6226042	6126043	6027047	5827054	5627059
5528065	5529067	5630063	5730054	5631037	5634019	5605022	5707026	5805016	6030011	6228033	6327048	6228054	6128059	5928066	5629069
5425064	5425065	5626058	5726047	5726026	5805001	5807023	5807035	5804034	6136035	6332046	6430059	6329068	6229073	5929077	5630078
5424063	5425073	5625072	5824061	6023040	6025011	6005015	5904031	6002042	6235056	6533069	6532079	6431084	6231087	5931086	5631082
5525059	5525079	5525083	5725075	6025057	6128030	6035023	6136038	6135055	6335071	6434085	6333094	6232097	5932094	5732089	5432081
5525052	5525079	5525096	5725097	5927078	6029050	6032042	6033054	6034069	6034080	6034085	5934090	5633092	5633089	5433082	5332074
5425044	5526071	5526098	5626112	5727096	5728069	5730057	5731058	5632062	5634067	5534069	5534070	5434071	5333069	5233065	5133060
5327040	5327063	5426092	5427109	5526098	5526079	5527067	5428058	5428049	5429040	5331036	5332036	5233039	5133041	5133042	5132042
5328031	5327049	5326080	5226103	5326099	5425089	5425084	5425070	5425062	5324054	5324045	5324035	5225026	5128022	5029023	5030025
5329018	5328035	5327063	5226089	5325099	5425094	5424087	5424079	5423073	5423070	5323068	5322064	5233056	5223044	5124033	5125027
5133039	5231048	5229051	5227052	5125063	5324074	5423078	5322080	5322081	5322083	5322085	5322085	5222081	5223070	5123055	5123042
5031049	5132051	5232044	5331036	5328035	5424046	5423064	5522080	5422093	5321103	5322109	5222110	5022106	5022095	5023077	5123061
5126039	5326028	5527013	5629010	5627016	5624026	5622043	5622063	5622084	5621104	5422119	5222126	5022124	4922115	5022101	5122085
5328033	5528031	5629022	5631016	5630014	5528011	5523017	5522031	5522050	5522073	5522095	5422111	5222118	5023120	5023115	5123105
5632049	5731041	5731024	5729006	5720013	5719021	5620022	5621023	5523028	5423041	5423059	5423079	5323095	5223108	5223115	5223116
5730025	5826005	5814020	5714033	5716038	5717040	5619035	5622031	5524028	5425032	5425043	5425060	5425077	5425092	5525107	5424118
5618014	5713025	5713020	5713025	5613018	5616014	5622014	5626020	5627025	5527029	5527037	5427051	5427066	5527082	5626103	5626121
5408004	5608022	5708023	5606016	5502017	5501021	5536026	5635034	5633041	5632041	5630043	5530049	5429063	5528083	5628110	5627129
5427014	5605016	5706026	5604019	5436019	5436021	5435031	5434047	5433059	5433062	5432060	5432063	5431076	5430099	5530124	5529137
5325039	5430011	5604022	5702028	5736029	5634033	5533046	5433065	5434077	5434085	5434093	5534099	5533108	5532122	5531135	5431133
5226063	5328040	5533030	5735056	5835088	5734099	5734110	5734121	5735130	5635135	5635141	5635141	5634136	5534129	5433121	5332107
5125085	5326073	5528055	5632064	5433092	5334104	5334114	5335123	5435126	5435127	5435127	5435121	5335110	5234097	5234083	5233066
5025088	5125098	5426084	5428073	5329075	5129075	5131067	5133059	5134058	5135059	5136059	5136056	5036050	5135044	5134034	5233024
5126073	5026099	5126102	5226088	5326081	5226084	5126073	5126051	5125029	5125011	5034002	5003007	5003008	5104005	5218003	5321011
5528064	5326082	5325099	5325103	5424096	5424095	5324091	5223080	5122066	5121051	5020038	5019029	5018024	5117024	5318026	5419030
5627054	5626065	5525081	5525097	5624102	5624098	5723095	5623090	5522081	5421070	5320062	5220057	5219051	5319047	5418044	5619044
5425030	5326046	5227062	5427069	5526067	5725064	5824061	6022060	6122063	6221065	6221065	6121063	6021060	6021057	6021053	6121049
5632033	5430053	5329072	5229073	5229065	5328062	5427057	5726052	6025047	6225043	6324041	6324042	6324044	6324043	6223041	6224042
5533067	5432078	5531087	5631088	5731080	5731068	5731055	5831047	5830045	5930043	5930039	6029036	6128032	6227031	6227032	6127039
5331068	5231074	5431080	5632076	5733068	5733058	5733052	5732048	5732044	5732037	5832029	5832023	5931021	6030022	6029028	6029037

Fig. 1-3

* WEATHER DATA IN 3 STANDARD PRESSURE LEVELS *
 * 34X16 DATA OUT OF 34X20 GRIDPOINTS *
 * TEMPERATURE, DIRECTION, SPEED *

3127023	3327026	3426039	3526065	3625086	4024080	4123067	4222059	4321057	4321056	4421057	4421058	4522060	4622055	4722047	4822044
3231027	3330026	3429035	3528048	3626059	3725060	3823056	4022055	4021058	4121061	4221064	4321068	4422071	4522067	4622058	4722050
3433035	3433038	3432044	3530043	3529038	3627034	3725029	3824030	3822036	3922042	4022049	4223055	4323062	4523063	4523060	4624055
3432043	3532052	3633057	3733052	3833037	3833037	3833037	3931014	3926016	3925020	4025036	4126044	4326050	4425054	4525057	4626057
3329049	3630045	3931044	4031043	4033033	4036021	4004018	4006011	4022003	4026020	4127035	4227044	4328053	4428050	4528054	4629064
3426046	3725036	4025033	4225029	4322017	4314010	4210019	4109018	4010003	4027017	4128039	4228052	4329061	4429069	4529073	4630083
3423049	3624049	3825040	4124030	4221023	4318013	4211012	4107010	4134010	4130027	4229048	4329061	4430074	4530081	4630083	4731086
3324040	3525062	3725059	3925039	4124025	4224013	4232006	4134015	4233028	4232044	4331059	4431074	4530083	4630083	4731086	4831086
3325029	3525058	3625069	3825055	4026036	4128026	4231027	4333039	4333052	4433064	4432073	4532078	4631083	4731088	4831087	4931079
3225028	3326052	3426067	3726068	3927056	4129048	4332053	4432064	4533073	4633080	4733088	4832089	4932086	4931078	5031065	5132050
3027031	3226051	3426066	3626078	3927079	4129068	4331065	4432069	4532072	4633074	4733075	4833074	4933072	5032068	5132060	5232050
3029029	3227039	3426060	3626084	3927093	4227081	4427068	4428056	4528046	4629040	4730037	4831033	4931031	5031031	5131031	5231029
3230028	3330033	3528051	3627078	3926090	4226081	4425073	4524070	4623066	4723061	4823055	4922049	5022044	5123041	5224036	5325030
3231036	3431038	3630042	3727052	3825065	4024068	4223070	4422076	4522082	4722085	4822084	4922079	5022076	5123072	5223064	5424051
3330030	3531021	3631014	3724032	3923046	4022059	4222071	4322081	4422087	4723088	4823084	5023083	5123085	5224080	5424064	5525070
3426013	3520004	3511006	3514002	3621009	3722022	3822037	3922053	4122069	4323042	4523089	4723090	4923091	5124094	5225089	5325070
3332006	3433005	3636006	3705007	3712006	3718010	3721020	3722033	3822049	4023067	4223085	4523099	4723107	4924112	4925105	5025077
3434016	3635011	3810006	3913020	3915026	3917028	3919028	3821032	3822039	3823051	3923071	4123094	4324115	4524128	4625118	4625085
3605005	3811016	3812029	3813030	3714026	3716025	3820027	3922034	3924037	3824040	3824052	3924075	4024103	4225125	4325125	4425094
3711022	3711031	3711030	3610024	3610020	3612013	3723012	3825029	3826036	3827037	3726041	3726055	3825081	4025108	4225118	4425101
3808025	3808034	3708025	3607019	3706023	3704022	3734020	3830030	3829038	3828039	3728040	3728047	3827065	3927090	4126107	4425099
3803009	3806032	3707027	3706010	3802011	3801028	3736039	3734041	3832042	3831043	3730044	3730049	3829062	3928060	4127095	4327094
3728024	3804018	3705026	3735009	3830022	3833029	3835038	3834048	3834056	3733058	3732060	3732064	3831072	3930083	4129091	4329090
3626052	3730023	3736030	3734043	3633054	3734060	3734070	3735081	3834086	3834089	3834090	3933090	3933091	4032094	4131096	4331092
3526070	3627052	3731045	3733068	3634091	3734102	3935113	4035120	4135119	4135115	4135109	4234103	4234097	4333091	4532082	4532082
3326072	3526071	3727065	3829068	3830070	4132068	4434067	4535070	4635077	4635081	4636080	4635077	4635075	4735069	4834060	4933048
3326067	3426078	3726079	3925083	4125085	4325070	4624050	4824033	5024017	5030008	5135012	5136017	5136021	5135021	5235017	5332008
3425058	3525079	3625084	3924084	4223093	4523095	4722069	4922082	5121073	5321059	5421042	5421026	5320017	5319015	5318016	5417020
3524038	3625066	3624081	3724079	3923079	4123083	4422086	4622091	4821096	5121095	5321081	5421060	5320047	5219045	5218044	5318041
3726022	3726045	3725063	3624070	3724070	3923068	4123071	4423078	4622085	4822091	5022090	5121081	5020072	5019070	5019067	5119059
3729026	3728036	3627044	3626054	3625060	3725062	3925062	4225060	4424058	4623061	4722068	4821074	4820075	4820074	4820072	4920066
3531033	3530041	3530046	3629048	3628051	3728057	3928057	4127047	4226036	4424033	4522039	4621046	4621051	4721053	4721055	4822058
3632043	3631054	3731059	3732056	3731051	3830047	3929041	4128032	4228024	4328018	4428016	4626017	4725019	4724023	4724032	4824044
3732045	3931050	3931049	4032045	3932044	4032042	4131042	4231040	4432034	4633030	4734026	4834023	4934018	4932015	4929018	4927033

Fig. 1-5

- WEATHER DATA IN 3 STANDARD PRESSURE LEVELS •
- 34x16 DATA OUT OF 34x20 GRIDPOINTS •
- TEMPERATURE, DIRECTION, SPEED •

4227033	4327035	4426047	4526074	4725095	4925083	5023068	5022062	5021060	5122058	5122057	5122056	5222060	5122055	5122048	5122046
4331031	4330029	4429040	4428055	4526065	4524064	4623063	4822066	4822066	4922067	5021069	5122071	5222067	5222068	5222060	5223053
4434039	4434042	4432049	4431049	4429042	4528037	4626033	4724034	4723039	4822046	4923052	4923059	5023065	5123067	5223064	5224058
4331044	4333058	4633069	4633069	4533059	4633054	4833030	4833019	4927020	4926030	5025039	5026047	5025054	5025059	5125062	5125059
4229054	4630055	4831057	4831056	4733042	4835027	4802022	4903013	4927007	5026026	5127041	5127049	5127053	5127057	5127062	5127063
4326053	4625048	4925046	5125037	5122021	5213011	5108025	4908023	4904003	5028025	5128049	5128060	5128063	5129065	5129070	5129070
4324057	4424060	4725054	5024045	5121033	5217015	5109018	5007019	5035012	5131035	5230058	5229071	5229075	5230080	5230082	5300080
4324052	4525073	4625069	4825050	5024032	5125013	5101008	5101016	5133029	5232049	5331066	5331076	5436084	5330090	5231090	5031083
4425041	4525069	4625080	4725068	4926046	5128029	5232027	5233039	5333055	5333069	5432077	5432082	5531088	5433109	5231086	5031076
4425037	4325060	4425078	4626084	4727072	5029054	5231054	5332065	5432075	5533084	5533089	5432088	5332083	5232074	5131063	
4027036	4126057	4326076	4526093	4727095	4928076	5130065	5131068	5232072	5332073	5333071	5232062	5132055	5132047		
4129032	4227044	4326069	4526096	4727104	4927087	5027070	5028057	5028046	5029040	5030036	5030033	5031031	5031031	5130031	5130030
4230023	4229034	4328061	4527093	4727099	4926084	5025074	5124070	5123064	5123059	5123053	5223046	5223039	5124036	5225033	5226030
4032037	4232046	4430054	4528067	4726078	4824076	5023077	5122082	5222088	5422090	5422087	5422079	5423072	5423066	5324059	5324047
4031040	4232034	4431025	4528028	4526043	4724053	4823063	5022075	5222087	5322096	5423096	5523091	5523086	5524084	5524078	5424062
4126023	4325009	4403001	4432004	4426011	4523022	4622038	4722056	4922073	5122088	5323096	5523097	5523096	5524097	5424088	5324070
4228013	4429012	4533010	4602009	4508003	4522005	4522019	4622035	4622053	4822074	5023093	5223108	5323114	5324114	5224104	5025079
4533030	4633023	4735004	4714017	4715027	4717028	4719026	4621030	4623039	4623054	4723076	4823101	4924121	5024129	4824117	4724089
4732010	4812010	4813029	4714034	4615031	4617029	4720029	4722032	4723034	4624040	4624054	4624079	4724107	4824124	4724122	4624098
4612018	4712032	4611032	4611025	4610019	4613012	4623012	4725026	4626032	4626034	4526041	4626059	4625086	4725111	4725119	4725104
4608019	4708034	4708027	4608019	4507019	4604018	4633019	4630029	4628035	4628037	4628039	4527088	4627069	4726096	4826113	4825105
4732006	4806027	4707027	4608009	4535006	4635026	4635039	4633041	4632041	4631041	4530044	4529051	4629065	4728087	4827104	4927102
4627032	4602012	4705022	4633010	4629029	4632032	4634037	4534045	4534051	4533054	4532058	4532065	4631076	4730091	4829101	4929099
4426060	4529028	4635029	4734045	4632056	4533058	4534068	4534076	4534079	4534083	4634087	4734092	4733099	4732105	4831105	4930099
4326079	4527061	4630052	4633076	4533094	4634104	4734118	4735124	4735120	4735118	4835117	4835116	4834113	4834106	4833097	4932086
4125080	4326083	4527073	4529073	4530076	4732071	4834071	4835074	4835079	4836083	4936085	4935084	4935081	4935073	5034064	5133052
4126072	4226090	4426091	4626088	4726088	4825073	4925051	5025031	5027015	5033013	5036020	5036024	5036025	5135025	5134020	5332012
4526060	4525083	4425095	4524099	4924106	5223104	5423095	5522084	5522071	5421054	5321035	5221021	5120014	5120012	5219013	5418017
4626043	4625067	4525083	4424094	4623103	4923105	5322105	5522105	5722106	5722100	5621082	5421059	5320047	5219044	5319043	5419041
4526033	4526049	4525064	4524077	4624087	4724089	4923092	5223098	5523103	5723103	5822095	5721082	5520074	5419071	5519068	5619061
4527028	4427038	4427050	4526063	4626073	4626077	4825077	5025074	5325071	5523070	5622073	5621076	5620077	5619076	5620074	5720069
4632032	4431044	4330057	4530062	4529061	4628067	4828064	4927054	5126043	5224040	5323044	5422049	5521052	5621054	5621058	5722062
4533056	4532066	4432071	4531068	4431061	4730056	4829050	4929040	5028033	5228027	5328024	5527022	5626022	5725026	5724035	5824049
4532056	4631058	4631056	4632054	4732054	4831053	4931051	5031046	5132039	5333034	5434030	5634026	5733021	5932018	5929021	5927037

Fig. 1-6

* WEATHER DATA IN 3 STANDARD PRESSURE LEVELS *

* 34X16 DATA OUT OF 34X20 GRIDPOINTS *

* TEMPERATURE, DIRECTION, SPEED *

5427050	5526052	5626060	5626084	5725101	5725080	5623061	5522054	5422050	5422048	5522043	5422050	5323044	5223045	5123041	5023041
5431039	5529039	5528048	5527061	5526072	5524069	5623071	5622074	5722071	5722069	5822070	5422070	5422070	5522065	5522059	5323047
5434043	5533047	5532053	5531051	5430042	5528038	5626037	5725040	5724044	5823050	5823058	5823058	5823064	5823067	5723066	5424060
5331049	5532065	5633078	5633079	5634070	5633053	5833037	5931026	6028026	6026035	6026044	5926052	5926059	5725062	5525060	5225053
5228065	5529065	5631063	5632055	5533042	5535029	5736023	5835016	6029017	6127034	6227049	6127055	6027056	5826057	5527057	5327053
5325064	5525065	5725056	5725037	5623017	5711008	5807022	5805020	5933011	6128038	6228062	6228062	6028069	5828060	5528060	5329058
5424063	5424072	5624070	5824058	5921039	5918014	5908016	5905019	6035018	6231045	6230069	6230077	6030074	5830071	5530069	5330068
5525059	5525079	5625079	5725063	5924040	6025016	6001009	6101019	6334034	6432056	6331072	6231076	5931078	5731077	5431076	5231073
5525052	5525076	5625089	5725082	5825062	5928037	6032028	6233039	6433057	6433071	6232076	6032076	5832076	5532077	5331075	5231070
5425044	5525069	5525089	5625099	5626091	5728063	5830051	6032059	6132069	6033074	5933076	5733075	5532073	5432070	5332066	5232060
5327040	5426059	5526082	5526103	5627104	5628082	5629064	5731062	5731063	5632061	5532058	5432056	5332055	5232052	5132049	5132045
5328031	5326047	5426076	5526106	5627113	5527093	5527072	5527058	5428047	5428039	5329035	5229032	5130030	5130031	5030033	5030033
5329018	5328038	5327071	5527106	5627107	5526084	5425070	5524066	5423060	5423054	5423049	5323042	5224035	5225033	5126032	5127031
5133039	5231054	5330065	5428081	5626088	5624079	5723078	5722081	5722084	5622084	5522079	5522071	5423063	5423056	5324050	5224043
5031049	5231048	5331040	5429042	5527058	5625063	5823068	5923078	5922089	5822095	5622093	5523088	5523082	5523078	5423071	5324058
5126039	5227023	5431013	5432014	5429020	5525026	5622039	5722059	5822077	5822091	5722097	5622096	5523095	5523094	5424086	5324071
5328033	5528026	5631015	5635012	5534010	5529010	5524020	5523038	5622059	5622081	5722097	5623106	5523108	5323107	5224099	5124081
5632049	5732036	5732011	5614013	5616027	5618026	5620023	5522027	5523040	5623059	5623081	5623099	5423111	5224115	5024108	5024090
5730025	5820003	5713026	5714038	5616037	5718033	5720028	5621026	5623029	5624040	5624057	5624080	5524103	5324114	5024112	4924097
5618014	5713027	5712032	5611025	5611017	5713008	5722009	5725017	5626023	5626031	5526043	5525064	5525088	5425106	5125109	4925100
5408004	5608024	5708025	5609018	5509015	5704009	5732015	5729025	5728030	5628033	5627039	5627052	5626073	5526092	5326102	5125098
5427014	5605014	5707021	5612007	5427009	5633026	5733039	5733041	5632040	5531039	5530044	5529054	5528069	5528086	5327096	5227094
5325039	5528009	5704007	5630016	5530034	5632035	5634036	5434041	5433050	5433050	5533058	5432068	5431081	5430092	5329095	5329091
5226063	5428037	5732028	5832046	5832055	5632055	5433061	5334067	5334070	5435076	5535082	5534088	5533096	5432100	5331096	5330087
5125085	5326069	5530059	5532079	5532092	5433096	5434109	5435118	5435117	5336111	5336107	5335105	5334103	5334096	5233086	5232075
5025088	5225095	5327081	5229076	5130079	5231073	5233073	5135077	5136081	5136083	5036084	5036083	5135078	5135069	5234059	5233048
5126073	5126100	5126101	5126090	5126083	5226071	5226050	5126030	5130017	5135021	5036030	5036033	5036031	5035028	5134022	5232016
5528064	5426083	5325098	5324103	5324101	5424099	5423078	5422062	5322044	5222028	5121017	5021011	5021010	5120011	5120011	5320015
5627054	5526064	5425081	5324105	5423118	5623113	5723108	5823103	5722096	5622084	5421069	5522054	5120043	5119039	5219037	5319035
5325045	5325056	5325071	5425091	5625113	5724116	5824111	5823104	5823099	5823092	5722081	5621070	5420063	5419059	5519056	5620052
5425030	5226046	5327067	5527085	5627095	5726096	5826093	5825085	5925075	5924070	6022069	6021068	5920066	5920065	5920063	5921061
5632033	5431053	5330075	5530081	5629076	5729074	5828071	5927061	6026050	6125047	6323050	6422051	6422050	6421051	6322055	6222058
5533067	5432074	5331080	5431079	5531072	5730067	5829060	5929051	6028044	6128039	6228034	6427029	6526027	6525030	6524039	6424049
5331068	5231064	5231063	5331064	5531068	5631066	5731061	5831053	5831044	5832037	5932031	6033025	6132020	6330019	6428026	6426039

Fig. 2-1

INTERPOLATED GRIDPOINT VALUES IN FLIGHT LEVELS
X-COMPONENTS OF WIND DATA

25	29	34	46	54	54	53	50	49	50	41	43	36	26	32	31	35	32	23	27	40
22	23	29	36	41	42	44	43	44	41	43	37	35	35	38	45	51	57	34	38	52
17	19	29	32	32	32	34	31	30	32	32	33	36	36	39	51	57	57	50	49	55
29	34	39	41	33	19	13	3	7	18	31	38	41	46	46	57	67	69	61	55	52
47	41	38	38	29	5	-17	-24	-17	3	25	43	50	54	54	64	75	76	72	61	44
47	36	35	34	22	1	-19	-25	-20	-4	17	39	54	54	63	72	81	77	70	52	42
41	45	43	37	24	8	-8	-11	-7	0	17	33	56	63	63	72	81	75	59	47	35
37	62	65	52	38	20	8	5	8	10	25	42	46	46	63	64	72	64	52	39	26
30	59	77	74	58	39	24	21	16	15	31	34	52	52	52	63	57	47	37	29	18
28	55	80	90	80	62	53	41	36	28	18	31	32	32	45	42	36	31	31	19	16
32	56	78	92	87	78	71	62	50	39	28	24	25	26	26	26	24	26	22	17	8
28	43	65	83	83	75	70	65	59	50	44	36	30	30	26	23	20	20	19	16	7
23	29	48	66	69	71	63	59	49	49	52	53	49	49	43	31	25	24	23	19	9
27	29	32	41	50	58	57	55	47	48	51	62	64	64	59	43	32	29	29	23	11
27	18	13	15	26	34	46	51	47	51	69	72	83	83	70	56	38	35	33	28	15
15	6	0	3	11	18	26	37	38	47	72	82	96	96	86	71	47	41	44	34	17
6	8	8	6	8	10	13	21	30	42	55	68	91	91	86	87	75	67	57	42	21
7	7	3	-5	-2	1	9	17	25	31	41	56	72	72	86	89	85	80	80	58	29
-2	-10	-18	-18	-13	-4	8	19	29	32	37	50	66	66	85	99	98	102	95	68	30
-20	-25	-25	-20	-15	-10	4	19	32	36	40	46	59	59	74	92	107	114	104	71	30
-24	-32	-26	-16	-12	-10	0	13	27	34	38	47	55	55	70	88	108	117	104	67	24
-3	-27	-28	-10	-4	-5	1	18	20	30	32	40	55	55	72	85	108	111	90	56	15
26	-8	-22	-11	-6	1	11	25	26	28	30	47	50	50	70	90	93	94	70	35	4
53	25	0	0	13	18	20	21	22	22	23	40	44	44	63	60	68	64	42	18	-5
71	56	37	37	37	35	20	22	22	22	21	20	19	19	34	28	33	29	21	7	-8
72	73	65	69	78	67	45	27	18	10	10	0	0	0	7	5	10	14	14	7	-5
67	78	75	76	88	92	76	51	27	12	6	2	-2	-2	-6	-4	1	10	16	13	1
56	71	73	68	75	85	85	65	42	25	14	6	6	0	-5	-11	0	15	22	24	11
35	59	70	63	66	72	69	69	53	38	25	13	11	11	0	-7	0	18	35	34	20
24	45	57	59	63	64	63	55	46	38	28	29	17	17	12	3	10	30	47	46	28
25	38	49	60	65	60	47	36	30	27	31	32	32	32	21	19	27	45	61	54	34
24	38	49	54	50	42	35	26	23	24	27	31	30	30	26	26	38	56	69	61	37
28	42	50	48	40	37	31	29	26	25	23	24	25	25	24	29	43	61	72	62	39
31	43	51	44	36	31	30	28	21	18	14	12	14	14	19	27	42	60	67	60	48

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Fig. 2-2.

INTERPOLATED GRIDPOINT VALUES IN FLIGHT LEVELS
 X-COMPONENTS OF WIND DATA

37	38	41	50	60	64	66	69	62	56	52	36	34	32	32	30	23	26	46
25	28	36	41	44	49	55	56	53	48	47	39	31	39	40	39	32	36	52
13	21	33	37	37	38	42	39	35	35	37	35	36	40	51	53	47	46	52
35	38	45	48	38	24	15	5	11	22	33	39	43	48	58	65	58	52	52
54	54	48	45	30	7	-20	-27	-17	6	30	46	52	58	68	73	67	59	48
54	48	47	42	24	-1	-24	-33	-24	-4	25	46	60	68	77	82	74	52	45
50	56	55	44	29	8	-13	-18	-13	2	22	46	62	68	79	79	66	46	34
47	71	72	61	47	25	5	0	9	12	27	46	53	65	64	68	60	35	29
41	69	85	86	70	42	25	22	26	18	31	34	52	52	58	53	45	31	21
36	64	90	103	92	66	52	41	36	25	26	28	29	41	38	33	30	21	17
37	61	87	103	96	83	71	61	50	38	26	22	22	23	23	26	22	15	10
30	47	74	94	94	83	75	67	59	48	41	33	26	24	22	21	20	15	8
19	32	56	79	84	83	72	65	52	52	51	49	45	39	29	25	23	17	8
23	33	40	48	56	64	62	52	50	51	53	55	60	53	44	30	27	20	10
33	25	20	22	30	36	44	53	52	54	74	74	81	70	55	43	37	25	14
26	15	5	6	14	21	27	39	44	52	78	86	86	77	74	52	44	33	20
17	18	15	9	10	11	15	21	31	45	59	73	81	98	89	78	69	44	24
18	20	13	1	4	4	8	15	23	31	43	59	74	85	89	87	83	60	33
9	-3	-15	-20	-15	-5	5	20	27	30	39	53	70	86	101	103	115	73	40
-13	-24	-26	-20	-14	-8	7	20	30	33	38	48	62	78	98	117	127	79	41
-16	-30	-26	-16	-11	-9	0	11	26	32	38	46	57	76	99	124	133	76	36
6	-21	-27	-10	-2	-3	6	17	23	31	39	40	57	79	98	124	124	65	28
33	1	-19	-11	-4	7	18	33	26	29	31	45	52	75	98	102	102	44	16
60	32	3	2	14	21	24	26	23	24	24	24	46	60	62	71	65	26	6
78	65	45	39	34	38	26	23	24	23	22	21	20	35	30	35	31	22	0
77	85	75	71	75	69	49	29	20	10	8	0	0	7	7	11	14	10	1
71	89	89	83	86	88	74	50	26	12	3	-1	-3	-4	-2	4	8	13	4
60	76	85	86	83	90	87	66	44	26	14	6	0	-5	-5	1	13	19	12
65	62	73	75	78	81	74	73	54	37	23	14	11	2	0	2	18	30	19
34	49	60	70	73	73	68	58	48	39	28	28	26	12	11	12	30	43	26
28	41	54	64	67	62	48	38	35	31	33	34	33	24	22	28	45	49	32
21	41	57	64	56	52	46	38	35	31	32	35	37	32	31	39	55	64	35
29	45	60	58	51	43	36	32	33	32	31	31	30	30	32	44	57	65	36
39	51	55	51	40	30	28	27	25	21	17	14	16	21	27	40	53	59	37

Fig. 2-3.

INTERPOLATED GRIDPOINT VALUES IN FLIGHT LEVELS
X-COMPONENTS OF WIND DATA

51	52	48	51	67	75	87	81	80	60	51	33	29	27	33	35	28	23	27	43
30	39	43	41	43	56	66	68	68	62	50	39	36	35	41	44	36	32	35	48
15	23	42	45	39	40	46	44	40	40	39	36	36	38	46	49	48	44	44	49
38	40	48	50	39	34	16	10	14	24	35	41	42	47	54	58	57	53	49	55
65	64	56	47	28	6	-17	-24	-14	10	32	48	53	58	65	64	63	56	56	49
61	62	58	46	26	-1	-22	-33	-22	0	30	52	64	69	72	67	64	53	51	47
55	70	69	54	31	10	-11	-20	-14	11	36	52	64	67	65	62	58	54	41	37
56	74	79	71	55	31	4	0	10	12	29	47	63	59	56	50	47	41	37	33
50	75	91	91	79	47	27	27	24	28	29	31	45	44	39	47	42	37	33	23
41	71	98	111	96	68	49	44	40	23	24	24	24	34	33	30	35	31	22	19
40	63	91	110	97	78	67	57	48	38	28	23	20	21	21	27	26	24	17	14
31	49	79	102	97	84	75	66	58	47	39	30	24	22	22	22	23	18	16	8
17	34	64	89	94	88	75	68	56	54	52	40	43	33	29	25	23	20	15	8
20	37	49	52	59	64	60	51	52	53	55	55	51	54	42	32	27	23	18	11
39	34	29	29	34	40	49	51	61	52	70	71	67	60	59	47	33	29	23	16
39	29	14	9	16	23	28	40	55	52	76	80	79	74	64	55	46	39	31	22
33	32	22	12	12	11	13	20	32	47	61	71	75	91	88	80	70	59	46	27
32	32	19	7	4	4	8	12	21	31	45	61	73	83	88	89	82	79	61	39
23	6	-13	-21	-13	-7	6	20	24	30	40	56	72	86	101	102	110	96	73	46
1	-18	-23	-19	-14	-5	9	20	25	29	37	51	66	82	101	119	122	105	80	49
-3	-21	-23	-14	-6	-4	0	5	21	25	37	42	59	83	109	130	128	107	78	46
15	-11	-23	-12	0	0	5	16	31	31	39	40	58	87	108	129	118	95	67	38
37	11	-13	-10	0	11	23	33	26	29	32	33	54	78	103	102	98	73	52	27
62	40	16	11	15	35	39	42	23	23	24	24	47	42	61	69	53	46	30	16
80	73	55	41	47	36	40	21	22	22	22	21	19	33	28	33	31	25	20	9
84	93	84	72	70	70	51	30	20	10	-1	0	0	8	12	12	15	16	12	6
72	98	101	87	79	82	72	50	27	10	1	-4	-4	-3	0	6	10	15	15	8
63	81	94	98	83	81	78	61	42	26	13	5	0	-4	0	5	11	17	19	13
55	64	76	92	89	85	73	69	52	35	21	20	9	9	0	9	14	19	21	17
43	51	67	82	88	82	67	60	47	37	25	24	23	10	10	17	23	33	33	25
28	45	63	69	66	60	53	39	40	33	33	32	30	30	27	25	37	41	39	30
21	46	69	70	61	62	58	52	45	41	36	36	38	33	31	36	44	50	44	33
34	51	68	68	62	53	43	36	40	37	34	34	32	31	32	39	47	52	45	34
53	58	62	49	33	29	26	31	28	24	19	15	16	19	26	35	44	49	43	33

Fig. 2-4.

INTERPOLATED GRIDPOINT VALUES IN FLIGHT LEVELS
X-COMPONENTS OF WIND DATA

25	28	40	66	83	71	51	38	29	30	31	31	39	35	30	28	26	19	18	24
22	23	34	49	59	56	44	37	32	34	33	37	46	43	37	34	33	25	21	29
17	18	29	37	34	28	27	25	28	28	33	43	48	49	47	48	40	29	26	37
29	32	30	30	26	20	13	12	17	26	35	44	49	52	55	56	49	40	37	43
47	41	36	35	18	1	-11	-9	3	21	36	45	50	53	60	63	57	49	47	46
47	37	34	29	11	-6	-20	-19	-3	19	40	53	57	58	65	68	60	51	49	41
41	44	41	29	13	-1	-13	-11	3	24	46	59	65	65	70	71	59	44	41	37
37	61	57	39	23	11	3	3	14	29	46	53	61	73	75	66	58	49	35	23
30	57	67	55	37	27	20	20	26	33	47	51	65	67	67	60	50	39	28	18
28	52	68	71	60	46	36	41	40	40	43	44	57	55	57	50	39	30	21	14
32	51	67	81	83	67	51	46	46	39	38	37	36	43	38	32	26	25	21	14
28	40	61	86	96	82	68	55	45	38	32	26	24	24	25	23	23	22	20	13
23	30	52	82	91	81	69	61	51	47	42	32	28	31	31	28	25	24	21	14
27	29	39	55	65	61	55	50	54	56	54	51	50	54	49	43	33	29	23	14
27	17	13	20	31	38	40	46	53	57	69	65	64	67	69	55	40	31	23	14
15	3	-5	0	6	15	24	34	45	62	69	70	71	82	82	65	45	31	25	18
6	5	1	-5	-4	1	10	21	32	50	66	78	83	97	97	72	44	26	22	17
7	4	-4	-14	-13	-5	5	16	26	39	55	73	101	111	109	79	45	24	20	21
-2	-14	-24	-23	-17	-8	9	22	31	35	45	66	90	115	114	87	51	30	23	26
-20	-29	-28	-24	-20	-11	9	26	34	36	40	55	77	102	111	96	63	36	31	32
-24	-33	-25	-18	-20	-14	8	26	36	38	39	46	66	91	106	94	74	52	43	38
-3	-27	-25	-9	-3	-3	2	16	27	33	38	43	59	81	97	96	79	64	52	39
26	-10	-19	3	21	16	8	16	19	29	39	41	56	74	88	87	82	68	54	33
53	21	1	15	29	23	24	17	29	30	31	42	47	62	75	74	72	59	45	23
71	54	37	35	35	35	25	21	21	21	20	19	36	34	47	53	53	42	28	13
72	73	67	65	62	44	23	12	13	11	0	13	13	12	21	24	28	23	16	6
67	80	81	80	82	67	44	29	15	7	2	0	0	4	4	6	8	11	15	10
56	75	81	76	76	75	61	53	39	29	20	13	6	3	0	-2	1	7	16	19
35	62	72	71	65	58	58	60	53	52	41	30	16	8	2	2	2	9	24	29
24	45	59	62	64	58	58	64	61	63	59	41	25	12	12	10	11	18	31	38
25	36	45	55	60	62	61	59	54	49	45	37	26	22	25	23	29	33	44	49
24	36	42	47	52	58	58	49	37	30	27	25	26	27	28	38	38	48	55	53
28	41	45	40	41	43	41	33	26	20	18	18	19	21	28	39	48	59	66	57
31	39	39	30	30	30	34	32	23	15	9	8	7	10	18	34	54	70	74	58

Fig. 2-5

INTERPOLATED GRIDPOINT VALUES IN FLIGHT LEVELS
X-COMPONENTS OF WIND DATA

37	38	49	75	90	77	51	39	30	36	36	36	39	35	31	30	28	23	20	23
25	28	40	56	66	56	49	43	44	43	37	46	45	43	39	40	33	26	22	28
13	16	32	38	38	36	33	31	32	32	41	46	50	51	50	49	40	29	26	37
35	32	36	36	29	23	16	16	21	31	38	47	52	56	58	54	47	37	35	46
54	51	45	41	21	5	-6	-5	9	28	43	50	54	57	61	61	53	45	44	43
54	48	45	35	13	-8	-24	-21	0	28	51	61	62	61	64	64	55	52	46	40
50	54	53	41	18	-2	-18	-17	2	29	52	67	69	67	69	67	56	51	40	37
47	70	67	50	30	13	-1	-3	14	32	52	58	70	74	67	62	55	47	36	25
41	66	77	67	48	31	17	20	28	35	49	52	63	65	64	57	48	35	30	21
36	58	75	85	76	53	42	41	47	41	43	43	55	51	47	46	39	28	24	16
37	56	76	94	97	76	57	51	46	45	37	36	34	38	34	30	27	26	19	13
30	44	70	97	106	88	70	56	45	38	31	29	24	25	27	27	25	23	21	15
19	33	62	96	101	83	69	60	48	44	40	34	30	31	31	30	27	25	21	14
23	32	49	69	79	66	59	53	56	57	55	50	53	49	49	40	35	28	23	14
33	25	22	30	45	49	49	51	56	62	71	69	65	70	65	53	40	31	23	15
26	11	1	4	13	19	24	36	47	57	71	71	74	81	76	61	44	33	26	19
17	14	6	-2	-1	4	13	24	35	49	69	83	86	95	89	73	48	32	24	19
18	14	2	-10	-13	-4	6	15	30	42	59	77	101	109	99	77	54	36	27	26
9	-7	-22	-22	-15	-4	10	19	25	35	47	68	92	105	104	85	61	41	32	29
-13	-26	-30	-23	-18	-8	8	22	30	33	40	58	81	103	110	97	69	48	41	34
-16	-31	-27	-19	-17	-11	10	25	33	35	38	49	70	94	109	97	79	59	50	42
6	-20	-24	-8	3	7	10	21	26	31	38	49	63	86	102	100	84	69	57	43
33	-1	-14	7	27	21	13	15	17	27	35	42	59	79	94	91	86	72	59	39
60	28	8	18	36	30	25	25	26	25	27	31	50	66	79	84	73	66	48	30
78	63	46	41	50	39	39	22	21	16	16	20	38	35	48	53	54	47	34	20
77	84	75	69	66	48	27	13	11	0	0	12	14	13	22	26	30	26	20	12
71	91	92	87	86	69	48	29	15	6	0	0	0	4	7	8	11	14	15	14
60	79	90	87	91	81	72	55	45	27	18	11	5	4	2	1	5	13	20	20
45	63	78	83	81	82	70	70	67	62	40	27	16	8	7	7	8	16	24	27
34	49	62	71	82	82	76	76	78	77	59	40	24	12	12	13	18	24	31	36
28	40	54	67	77	80	76	72	68	56	46	37	25	15	24	26	30	34	40	47
21	36	52	57	60	67	65	56	44	37	35	31	27	27	30	39	41	46	54	52
29	43	49	54	49	50	49	40	34	29	26	24	23	25	31	42	51	61	65	57
39	45	44	38	39	43	41	36	27	19	12	10	11	13	21	37	57	71	73	58

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Fig. 2-6

• INTERPOLATED GRIDPOINT VALUES IN FLIGHT LEVELS •
• X-COMPONENTS OF WIND DATA •

51	52	60	84	95	75	47	35	32	31	31	31	32	37	34	31	31	29	21	17	21
30	38	48	62	72	60	54	48	46	44	46	41	42	42	38	41	36	31	25	23	32
15	25	34	39	36	37	36	39	39	39	44	51	49	51	51	52	46	37	30	27	32
38	43	39	40	24	27	19	20	26	34	43	55	51	55	58	56	50	42	35	34	40
65	62	48	34	21	5	1	4	17	35	50	56	55	56	56	57	52	46	41	41	41
61	62	54	35	13	-8	-21	-14	7	38	62	63	69	63	59	58	54	47	44	44	39
55	63	62	51	20	0	-16	-15	3	35	61	67	64	64	60	59	54	57	49	39	34
56	74	75	60	36	15	-2	-3	12	36	55	58	59	59	58	57	55	53	40	37	27
50	71	85	78	59	37	18	20	29	36	49	49	49	48	48	56	54	40	37	32	23
41	66	85	94	81	63	44	38	44	37	37	37	37	46	44	42	38	34	30	26	18
40	58	81	102	105	81	60	47	48	38	37	36	36	35	32	31	29	31	24	21	15
31	46	76	105	114	93	72	58	46	38	33	29	26	26	27	29	28	27	25	20	13
17	37	72	107	108	83	66	57	46	41	38	32	30	30	31	32	31	29	26	21	13
20	42	57	81	88	68	60	52	54	54	51	46	47	47	42	42	37	33	27	22	14
39	38	32	40	59	60	52	61	57	61	59	67	63	63	59	53	50	39	31	23	15
39	24	11	9	20	25	25	38	49	58	61	61	61	73	71	74	61	47	32	27	20
33	27	11	2	3	9	17	30	38	52	61	81	81	83	81	86	70	54	36	25	23
32	24	7	-8	-9	0	8	17	31	45	62	76	84	84	99	93	78	62	42	29	26
23	2	-20	-24	-13	0	10	12	22	35	49	69	89	89	98	96	84	69	48	39	34
1	-20	-28	-23	-16	-6	6	15	22	31	42	60	83	83	100	101	94	73	60	49	35
-3	-23	-25	-18	-15	-6	10	23	30	32	39	52	72	72	91	99	91	81	68	56	44
15	-10	-20	-6	10	14	21	21	26	30	38	51	69	69	85	95	93	84	71	58	45
37	10	-3	15	29	22	12	14	15	25	28	44	62	62	80	89	85	81	70	57	42
62	37	19	31	35	35	32	23	24	12	13	30	48	48	64	74	74	67	62	49	34
80	69	51	52	60	49	37	20	20	-1	-1	18	35	35	33	43	47	49	45	37	27
84	90	82	71	68	57	38	13	-1	0	0	-1	14	14	12	20	24	29	28	24	18
72	99	100	89	82	70	49	30	15	4	0	0	0	0	5	8	10	13	16	19	17
63	82	92	89	87	86	69	60	40	28	18	9	6	6	5	4	5	7	15	18	22
55	63	76	92	91	88	84	80	62	53	35	17	15	15	7	6	6	12	19	26	25
43	53	68	87	108	102	98	80	76	69	51	35	35	22	10	10	19	16	22	28	32
28	46	68	87	97	96	93	81	70	62	44	34	34	23	23	22	32	28	31	35	37
21	42	66	71	72	70	71	62	50	45	38	33	33	32	26	35	37	44	45	45	44
34	48	62	62	56	59	57	40	44	39	34	30	30	27	28	34	42	48	52	52	44
53	49	48	50	53	52	48	41	35	25	21	13	13	13	16	26	34	51	59	59	50

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Fig. 3-2.

• TEMPERATURES OF GRID POINTS IN FLIGHT LEVELS •

45	46	47	47	46	46	47	47	48	50	51	51	52	52	51	52	51	50	50	50
45	46	46	47	47	47	47	48	49	50	51	52	53	53	52	53	51	50	50	50
46	46	47	47	47	47	48	49	50	51	52	53	54	54	53	54	51	50	50	49
45	47	48	49	50	50	51	50	51	52	53	54	55	55	54	55	52	50	49	49
44	47	50	52	51	51	51	51	51	51	52	53	54	55	54	55	52	50	49	49
45	47	50	52	52	51	52	53	51	51	52	54	55	55	55	55	53	50	49	49
45	46	49	51	53	51	52	54	52	52	53	55	55	56	55	55	53	51	50	50
46	47	48	50	52	54	54	54	54	54	55	55	55	55	54	55	52	51	51	51
46	47	48	49	53	53	55	55	55	55	55	55	55	54	53	53	52	52	52	52
45	46	46	46	49	52	53	54	53	53	53	53	53	52	52	52	52	52	53	53
43	44	45	47	50	52	53	53	52	52	52	51	51	50	51	52	51	52	53	53
44	44	45	46	48	50	52	52	53	53	52	52	51	51	51	51	52	53	53	54
44	44	45	45	47	49	52	52	52	53	53	53	53	53	53	53	53	53	53	54
42	44	45	45	45	45	48	51	52	52	52	53	53	52	52	52	53	54	54	55
43	45	47	47	48	47	47	49	50	51	51	51	52	49	50	52	52	54	54	55
44	46	47	48	48	48	48	48	47	47	50	50	50	49	47	48	49	51	52	54
47	49	49	50	50	50	50	49	49	48	47	47	47	47	47	47	48	50	51	54
49	50	50	50	49	49	49	49	49	48	47	46	46	46	47	47	49	50	51	55
48	49	49	48	48	47	47	48	48	48	48	48	47	47	47	48	50	51	52	56
49	50	49	47	47	47	47	47	47	47	47	47	47	48	49	50	50	51	53	57
48	48	49	48	48	48	48	47	47	47	47	47	48	49	50	50	51	52	53	56
46	47	48	49	49	49	49	48	49	49	48	48	49	49	50	50	51	52	54	56
45	46	48	50	50	50	49	48	49	50	49	49	49	50	50	51	52	54	54	56
43	44	46	49	49	50	49	49	49	50	50	49	49	50	51	52	53	54	54	56
43	43	45	47	49	49	51	52	52	52	52	51	51	51	52	53	54	55	55	55
47	46	46	48	49	49	52	53	54	53	53	52	52	52	54	55	56	55	55	55
48	48	47	47	49	51	53	54	55	56	56	56	56	55	57	57	57	56	55	55
47	47	47	47	47	47	53	53	53	55	56	56	56	55	58	58	58	57	55	54
47	46	46	47	48	49	51	52	52	54	56	57	57	58	58	58	59	57	55	53
48	46	46	46	46	46	47	48	50	52	54	56	57	58	59	60	60	59	54	53
47	47	47	48	48	48	49	50	51	52	53	54	55	56	57	60	60	59	56	53
47	47	48	50	51	52	52	52	52	53	54	55	56	58	59	59	59	58	56	53

Fig. 3-3.

• TEMPERATURES OF GRID POINTS IN FLIGHT LEVELS •

55	56	57	57	55	56	56	56	57	57	58	58	58	56	53	53	53	52	52	51	51	50	50	50
55	56	56	57	56	56	56	56	57	57	58	58	58	59	57	55	55	54	54	53	52	51	51	50
55	56	57	57	57	58	58	58	58	59	60	60	61	62	60	58	58	57	57	55	53	52	51	50
54	56	57	58	58	58	57	58	58	59	60	60	62	63	62	61	61	58	58	56	54	52	51	50
53	56	57	58	56	56	57	57	58	58	59	59	61	63	63	62	62	59	59	56	54	52	50	49
54	55	57	58	57	58	59	58	59	59	62	64	65	64	65	64	59	59	56	53	51	50	49	
55	55	57	59	61	61	61	61	60	60	61	63	66	66	65	63	59	59	56	53	50	49	48	
56	56	56	58	61	62	61	62	61	62	62	64	65	64	64	63	59	57	54	52	50	50	50	
56	56	56	58	60	61	61	61	61	61	61	60	60	60	59	57	56	54	53	51	50	50	50	
55	56	56	57	58	57	57	57	57	57	56	56	55	55	55	54	53	52	51	51	51	51	51	
54	54	55	55	56	55	55	55	54	54	54	54	53	53	53	52	51	51	51	51	51	51	51	
54	54	54	53	54	54	54	54	54	54	54	53	53	53	53	52	51	50	50	51	51	51	51	
54	54	54	53	54	54	54	54	54	54	54	54	53	53	53	53	52	51	51	51	51	51	51	
52	53	53	53	52	54	54	54	54	53	53	53	53	53	52	52	52	51	51	51	52	52	52	
51	52	53	54	54	55	55	55	55	55	54	53	53	53	52	50	50	50	51	52	52	53	53	
52	54	56	57	57	57	57	57	57	57	57	57	54	54	52	50	49	50	51	51	52	53	53	
54	56	57	57	57	57	56	56	56	56	56	56	56	56	55	52	50	50	51	51	52	52	53	
57	58	58	58	58	58	58	58	57	57	56	55	55	55	54	52	52	52	52	52	52	53	54	
58	59	59	58	58	58	58	58	57	57	56	55	55	55	55	55	55	56	54	54	53	53	54	
57	58	58	58	57	57	57	57	57	57	57	56	56	56	55	56	57	57	57	55	53	53	55	
55	57	58	57	56	56	56	56	56	56	57	57	57	57	56	55	56	57	57	55	54	54	55	
55	57	58	57	55	55	55	55	55	55	55	55	55	55	55	55	55	56	56	54	53	54	55	
54	55	57	58	58	58	57	58	58	58	58	58	58	58	58	56	56	56	56	54	53	52	53	
53	54	56	58	59	58	58	58	58	58	58	57	57	57	57	57	56	54	53	52	52	53	56	
52	54	56	57	54	53	53	53	53	53	54	54	54	54	53	52	52	52	52	52	52	54	56	
51	52	55	55	53	53	51	51	51	51	51	51	51	51	50	51	51	51	52	53	53	54	56	
52	51	52	53	53	53	52	52	51	51	51	51	50	50	50	51	51	52	53	54	55	55	56	
56	54	54	54	54	54	54	54	53	52	51	51	50	50	50	50	51	53	53	55	55	55	55	
57	57	56	56	57	57	56	57	56	56	55	54	53	53	52	52	53	54	56	56	56	56	55	
54	54	55	56	57	57	59	59	61	60	59	59	58	58	56	56	56	57	58	58	57	55	55	
55	54	53	55	56	58	58	59	59	61	62	63	63	63	61	60	60	60	61	60	58	56	54	
57	55	54	53	53	53	54	54	55	58	61	63	64	64	63	62	62	62	62	61	58	55	54	
56	55	56	56	58	58	58	58	58	59	59	60	59	60	61	62	62	62	61	60	57	54	54	
54	53	55	55	57	58	58	58	58	57	57	57	57	57	58	59	60	60	60	58	56	54	52	

Fig. 3-5

* TEMPERATURES OF GRID POINTS IN FLIGHT LEVELS *

45	46	47	47	49	51	51	51	52	52	52	52	51	51	51	51	50	49	40
45	46	46	46	47	47	48	50	51	52	53	53	53	52	52	51	51	50	50
46	46	46	46	46	47	48	49	49	50	51	51	52	52	52	51	51	50	50
45	47	48	48	47	48	50	50	51	51	52	52	53	52	52	51	50	50	50
44	48	50	50	49	50	50	51	51	52	53	53	53	52	52	51	50	49	49
45	48	51	52	52	53	53	51	51	52	53	53	53	52	52	51	50	49	49
45	46	49	52	53	54	53	52	52	53	54	54	53	53	53	51	49	48	40
46	47	48	50	52	53	53	53	54	55	55	55	54	52	50	50	49	49	50
46	47	48	49	51	53	54	54	55	56	56	55	54	52	50	50	50	50	51
45	46	46	46	48	52	53	55	56	56	55	55	54	52	51	51	51	52	52
43	44	46	47	49	51	52	52	53	53	53	53	52	52	51	51	52	52	53
44	44	45	47	49	50	51	51	51	51	50	50	50	50	51	52	53	53	53
44	44	45	47	49	50	51	52	52	52	52	52	51	52	52	52	53	53	54
42	44	46	47	49	50	52	52	54	54	54	54	54	53	53	54	54	54	54
42	44	46	47	47	49	50	52	54	54	54	55	55	55	54	54	54	55	55
43	45	46	46	46	47	48	49	51	53	54	55	55	55	54	53	53	55	56
44	46	47	48	47	47	47	48	48	50	52	53	53	52	50	51	53	55	56
47	48	49	49	49	49	49	48	48	48	49	50	50	48	48	48	49	52	56
49	50	50	49	48	48	49	49	49	48	48	48	49	49	48	47	48	51	56
48	49	49	48	48	48	48	48	48	48	47	48	49	49	48	47	48	51	57
48	49	49	48	47	48	48	48	48	48	47	47	48	49	49	49	50	52	56
49	50	49	48	47	48	48	48	48	48	47	47	48	49	49	50	50	52	55
48	48	49	48	48	48	48	47	47	47	47	47	48	49	49	50	51	53	54
46	47	48	49	49	47	47	47	47	47	48	49	49	49	49	50	51	52	54
45	47	48	48	47	48	49	49	49	49	49	49	49	49	50	50	51	52	54
43	45	47	47	46	48	49	49	49	49	49	49	49	50	51	52	52	54	55
43	44	46	47	48	49	50	50	50	50	50	50	51	51	53	54	55	55	56
47	47	46	47	50	52	54	55	57	57	56	54	52	52	54	56	57	58	57
48	48	47	46	48	51	54	56	57	57	56	54	52	53	54	56	57	58	59
47	47	47	47	48	49	51	53	56	57	58	57	55	55	55	56	57	58	59
47	46	46	47	48	48	50	52	54	56	57	57	57	57	57	57	58	59	59
48	46	45	47	47	48	50	51	53	54	55	56	57	58	58	59	60	59	58
47	47	46	47	48	49	50	51	52	54	55	57	58	59	59	60	60	59	57
47	47	47	48	49	50	51	52	53	54	55	57	58	60	60	60	60	59	56

Fig. 3-6.

• TEMPERATURES OF GRID POINTS IN FLIGHT LEVELS •

55	56	57	57	58	58	56	57	55	54	55	54	53	52	51	50	49	48	46
55	56	56	56	56	56	57	57	58	58	59	59	59	57	55	53	51	50	50
55	56	56	56	55	55	56	57	58	58	59	59	59	57	57	54	52	51	50
54	56	57	57	57	57	59	59	60	61	61	60	60	58	58	55	52	51	50
53	56	57	57	56	56	58	58	59	61	62	63	62	61	59	55	53	51	50
54	56	58	57	56	57	59	59	59	60	62	63	63	61	59	55	53	51	50
55	55	57	59	60	60	60	60	60	61	63	63	63	61	58	55	53	51	50
56	56	57	58	60	61	61	61	62	64	65	64	63	59	57	54	52	51	50
56	56	57	58	59	60	61	63	63	65	65	65	60	58	55	53	52	51	50
55	56	56	57	57	58	58	58	61	62	60	59	57	55	54	53	52	51	50
54	55	56	56	57	57	56	57	57	56	56	55	54	53	52	51	51	51	51
54	54	55	56	57	55	55	55	55	54	54	53	52	51	51	50	50	51	51
54	54	54	56	57	55	54	54	55	54	54	54	53	52	51	51	51	51	52
52	53	54	55	57	57	57	58	57	56	56	55	55	54	54	53	52	52	52
51	53	54	55	56	57	59	59	60	60	58	56	55	55	55	54	53	52	53
52	53	55	55	56	57	57	57	58	59	59	57	56	55	55	54	53	52	53
54	56	57	57	56	56	56	56	56	57	57	56	55	55	53	52	51	52	54
57	58	57	57	57	57	57	57	56	56	57	57	54	54	52	50	50	52	55
58	59	58	58	57	58	58	58	57	57	57	57	56	56	53	50	49	51	55
57	58	58	57	57	58	58	58	58	57	57	56	56	56	55	51	49	50	56
55	57	58	57	56	58	58	58	58	58	57	57	57	57	56	53	51	52	54
55	57	58	57	55	57	58	58	58	57	56	56	56	56	56	53	52	53	55
54	56	58	57	56	57	57	57	55	55	55	56	55	55	55	53	53	54	55
53	55	58	59	59	57	55	55	54	54	55	56	56	56	55	53	53	54	55
52	54	56	56	56	55	55	55	55	55	55	53	53	53	53	53	53	53	54
51	53	54	53	51	52	52	52	51	51	51	50	50	51	51	52	52	53	54
52	52	52	51	51	52	52	52	51	51	51	50	50	50	50	51	52	53	55
56	55	54	54	53	54	54	54	54	53	53	52	51	50	50	51	53	54	55
57	56	55	54	55	57	57	57	58	57	56	54	52	51	51	52	53	57	57
54	54	54	55	57	58	58	59	58	58	58	57	56	54	55	57	58	58	54
55	53	54	56	57	58	59	59	59	59	59	60	60	59	59	59	59	59	54
57	55	54	56	57	58	59	59	60	61	62	64	65	65	65	64	62	61	59
56	55	54	55	56	58	58	59	60	61	62	63	65	66	66	64	63	61	54
54	52	52	54	56	57	58	59	59	59	58	58	60	61	63	64	63	61	57

Fig. 4.

• PERFORMANCE DATA FOR DC10 •

• SPECIFIC RANGE •

757	748	740	731	722	713	704	694	684	674	664	654	643	633	623	612
856	842	828	814	799	784	769	754	739	722	706	690	674	657	640	623
897	880	862	844	825	807	787	764	748	728	708	688	668	648	627	606
601	590	579	568	557	545	534	522	511	499	488	476	465	453	440	428
697	590	573	556	538	520	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1
584	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1	-1

• MAX. WEIGHT •

269437270344271251272158*00000*00000*00000
 227705228613229520230427231334232242233149
 188596189150189604190057190511189964191418

Fig. 5-1.

* CLIMB TIME *

160	162	163	165	167	167	168	182	198
178	180	182	183	185	187	188	202	222
205	207	208	210	212	213	215	228	250
165	167	168	170	172	172	173	187	205
185	187	188	190	192	193	195	208	230
212	213	215	217	220	222	223	238	260
170	172	173	175	177	178	180	193	212
190	192	193	195	197	198	202	215	238
220	222	223	225	228	230	232	247	270
175	177	178	180	182	183	185	200	220
197	198	200	202	203	205	208	223	247
228	230	232	233	237	238	240	257	282
180	182	183	185	187	188	190	207	227
203	205	207	208	210	212	215	230	255
237	238	240	243	245	247	250	267	293
187	188	190	192	192	193	197	212	235
210	212	213	215	217	218	222	238	265
245	247	250	252	255	257	260	277	305
192	193	195	197	198	200	202	218	242
217	218	220	222	225	227	228	247	273
255	257	260	262	263	267	270	288	318
197	198	200	202	203	205	208	227	250
223	225	228	230	232	233	237	255	283
265	267	270	272	275	277	280	298	332

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Fig. 5-2.

[illegible]

Fig. 5-3.

265	268	270	273	275	278	282	312	355
315	317	320	323	327	330	333	365	420
-1	-1	-1	-1	-1	-1	-1	-1	-1
273	277	278	282	285	287	290	322	368
327	330	333	337	340	343	347	380	440
-1	-1	-1	-1	-1	-1	-1	-1	-1
282	285	288	290	293	297	300	333	383
340	343	347	350	353	357	362	397	462
-1	-1	-1	-1	-1	-1	-1	-1	-1
292	295	297	300	303	305	310	345	398
355	358	362	365	368	372	377	415	487
-1	-1	-1	-1	-1	-1	-1	-1	-1
300	303	307	310	312	315	320	358	415
372	375	378	382	385	390	393	435	513
-1	-1	-1	-1	-1	-1	-1	-1	-1
310	313	317	320	322	325	330	370	432
390	393	397	402	405	408	413	457	545
-1	-1	-1	-1	-1	-1	-1	-1	-1
320	323	327	330	333	337	340	385	450
-1	-1	-1	-1	-1	-1	-1	-1	-1
-1	-1	-1	-1	-1	-1	-1	-1	-1
332	335	338	342	345	348	352	400	472
-1	-1	-1	-1	-1	-1	-1	-1	-1
-1	-1	-1	-1	-1	-1	-1	-1	-1
343	347	350	353	357	360	365	415	493
-1	-1	-1	-1	-1	-1	-1	-1	-1
-1	-1	-1	-1	-1	-1	-1	-1	-1

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Fig. 5-4.

355	358	362	367	370	373	378	433	520
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-1	-1	-1	-1	-1	-1	-1	-1	-1
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-1	-1	-1	-1	-1	-1	-1	-1	-1
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368	373	377	380	383	387	392	453	548
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-1	-1	-1	-1	-1	-1	-1	-1	-1
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-1	-1	-1	-1	-1	-1	-1	-1	-1
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383	387	392	395	398	403	408	473	582
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-1	-1	-1	-1	-1	-1	-1	-1	-1
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-1	-1	-1	-1	-1	-1	-1	-1	-1
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400	403	408	412	415	420	425	498	620
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-1	-1	-1	-1	-1	-1	-1	-1	-1
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-1	-1	-1	-1	-1	-1	-1	-1	-1
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418	422	427	430	435	438	445	525	667
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-1	-1	-1	-1	-1	-1	-1	-1	-1
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-1	-1	-1	-1	-1	-1	-1	-1	-1
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438	443	447	452	455	460	467	557	725
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-1	-1	-1	-1	-1	-1	-1	-1	-1
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-1	-1	-1	-1	-1	-1	-1	-1	-1
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462	467	472	477	480	485	492	595	-1
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-1	-1	-1	-1	-1	-1	-1	-1	-1
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-1	-1	-1	-1	-1	-1	-1	-1	-1
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Fig. 6-1.

* CLIMB DISTANCE *

52	53	54	55	56	57	58	64	72
60	61	62	64	65	66	67	74	83
72	73	74	76	77	79	80	87	97
54	55	56	57	58	59	60	66	74
62	64	65	66	67	69	70	77	86
75	76	78	79	81	82	84	91	102
56	57	58	59	60	61	62	69	77
65	66	67	69	70	71	73	80	90
78	79	81	83	84	86	88	95	106
58	59	60	61	62	63	64	71	80
67	69	70	71	73	74	76	83	94
81	83	84	86	88	90	91	99	111
60	61	62	63	64	65	67	74	84
70	71	73	74	75	77	78	86	98
85	86	88	90	92	93	95	103	116
62	63	64	65	66	68	69	77	87
72	74	75	77	78	80	81	89	102
88	90	92	94	96	98	100	108	122
64	65	66	68	69	70	72	80	90
75	77	78	80	81	83	85	93	106
92	94	96	98	100	102	104	113	127
66	67	69	70	71	72	74	82	94
78	80	81	83	84	86	88	97	110
96	98	100	102	104	106	109	118	133

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Fig. 6-2.

68	70	71	72	74	75	77	85	97
81	82	84	86	87	89	91	100	115
118	121	124	126	129	131	134	144	162
71	72	73	75	76	78	79	88	101
84	86	87	89	91	93	95	104	120
106	108	110	112	115	117	119	130	147
73	74	76	77	79	80	82	92	105
87	89	91	92	94	96	98	108	125
111	113	116	118	120	123	125	136	155
75	77	78	80	82	83	85	95	109
90	92	94	96	98	100	102	113	130
117	119	122	124	127	129	132	143	164
78	80	81	83	84	86	88	98	113
94	96	98	100	102	104	106	117	136
123	126	129	131	134	136	139	151	173
81	82	84	86	87	89	91	102	118
98	100	102	104	106	108	110	122	142
131	134	137	139	142	145	148	161	185
83	85	87	89	90	92	94	106	123
101	104	106	108	110	112	115	127	148
-1	-1	-1	-1	-1	-1	-1	-1	199
86	88	90	92	93	95	97	110	128
106	108	110	112	114	117	119	133	155
-1	-1	-1	-1	-1	-1	-1	-1	-1
89	91	93	95	97	99	101	114	133
110	112	115	117	119	122	124	139	163
-1	-1	-1	-1	-1	-1	-1	-1	-1

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Fig. 6-4.

130	133	135	138	141	144	147	173	213
-1	-1	-1	-1	-1	-1	-1	-1	-1
-1	-1	-1	-1	-1	-1	-1	-1	-1
136	139	141	144	147	150	154	182	227
-1	-1	-1	-1	-1	-1	-1	-1	-1
-1	-1	-1	-1	-1	-1	-1	-1	-1
142	145	148	151	154	157	161	192	242
-1	-1	-1	-1	-1	-1	-1	-1	-1
-1	-1	-1	-1	-1	-1	-1	-1	-1
149	152	155	159	162	165	169	203	260
-1	-1	-1	-1	-1	-1	-1	-1	-1
-1	-1	-1	-1	-1	-1	-1	-1	-1
157	160	164	167	170	173	178	215	283
-1	-1	-1	-1	-1	-1	-1	-1	-1
-1	-1	-1	-1	-1	-1	-1	-1	-1
166	169	173	176	180	183	188	230	310
-1	-1	-1	-1	-1	-1	-1	-1	-1
-1	-1	-1	-1	-1	-1	-1	-1	-1
176	180	184	187	191	195	199	248	-1
-1	-1	-1	-1	-1	-1	-1	-1	-1
-1	-1	-1	-1	-1	-1	-1	-1	-1

Fig. 7-1.

* CLIMB FUEL *

2893	2938	2983	3028	3073	3118	3167	3279	3424
3080	3139	3190	3240	3290	3341	3395	3515	3677
3317	3373	3430	3486	3543	3600	3660	3786	3961
2970	3017	3064	3110	3157	3205	3255	3375	3528
3177	3229	3281	3333	3386	3439	3495	3622	3795
3419	3478	3537	3596	3656	3715	3778	3912	4098
3049	3097	3146	3195	3244	3293	3346	3472	3634
3266	3320	3375	3430	3484	3540	3598	3733	3916
3524	3586	3647	3709	3772	3834	3900	4041	4240
3129	3179	3230	3281	3332	3383	3438	3572	3743
3357	3414	3471	3528	3586	3643	3704	3847	4042
3633	3698	3763	3827	3892	3957	4026	4176	4387
3211	3263	3316	3369	3422	3475	3533	3674	3856
3452	3511	3570	3630	3690	3750	3813	3964	4171
3747	3814	3882	3949	4017	4086	4157	4315	4541
3295	3349	3404	3460	3515	3570	3630	3779	3972
3549	3611	3672	3734	3797	3859	3926	4085	4305
3866	3935	4006	4077	4148	4219	4294	4462	4702
3381	3438	3495	3552	3610	3668	3729	3887	4092
3649	3713	3778	3842	3907	3972	4042	4210	4445
3989	4062	4136	4210	4284	4359	4437	4614	4872
3470	3529	3588	3648	3708	3768	3832	3999	4216
3753	3819	3886	3954	4021	4089	4161	4339	4590
4119	4196	4273	4350	4428	4506	4588	4775	5051

Fig. 7-3

4532 4618 4704 4790 4877 4964 5059 5360 5777

5057 5157 5257 5357 5457 5558 5667 5992 6509

-1 -1 -1 -1 -1 -1 -1 -1 -1

4662 4750 4840 4930 5019 5110 5209 5530 5978

5230 5334 5438 5542 5647 5752 5865 6213 6778

-1 -1 -1 -1 -1 -1 -1 -1 -1

4797 4890 4982 5076 5169 5263 5365 5709 6192

5417 5525 5634 5742 5852 5962 6079 6452 7073

-1 -1 -1 -1 -1 -1 -1 -1 -1

4938 5034 5130 5226 5323 5421 5527 5895 6417

5617 5731 5844 5958 6072 6187 6310 6710 7398

-1 -1 -1 -1 -1 -1 -1 -1 -1

5076 5175 5275 5376 5476 5577 5687 6084 6650

5830 5948 6067 6186 6305 6424 6553 6984 7754

-1 -1 -1 -1 -1 -1 -1 -1 -1

5222 5325 5429 5532 5636 5741 5856 6283 6899

6070 6194 6318 6442 6567 6692 6827 7291 8166

-1 -1 -1 -1 -1 -1 -1 -1 -1

5376 5483 5590 5698 5806 5914 6034 6496 7078

-1 -1 -1 -1 -1 -1 -1 -1 8661

-1 -1 -1 -1 -1 -1 -1 -1 -1

5539 5650 5762 5874 5986 6098 6222 6724 7463

-1 -1 -1 -1 -1 -1 -1 -1 -1

-1 -1 -1 -1 -1 -1 -1 -1 -1

5713 5828 5943 6060 6176 6293 6428 6969 7785

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Fig. 7-4.

5899 6019 6130 6260 6381 6502 6638 7231 8143

-1 -1 -1 -1 -1 -1 -1 -1 -1

-1 -1 -1 -1 -1 -1 -1 -1 -1

6100 6225 6350 6475 6602 6728 6870 7526 8545

-1 -1 -1 -1 -1 -1 -1 -1 -1

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6318 6448 6578 6710 6841 6972 7121 7846 9002

-1 -1 -1 -1 -1 -1 -1 -1 -1

-1 -1 -1 -1 -1 -1 -1 -1 -1

6557 6693 6829 6965 7102 7239 7396 8202 9530

-1 -1 -1 -1 -1 -1 -1 -1 -1

-1 -1 -1 -1 -1 -1 -1 -1 -1

6821 6963 7105 7247 7390 7534 7698 8603 10159

-1 -1 -1 -1 -1 -1 -1 -1 -1

-1 -1 -1 -1 -1 -1 -1 -1 -1

7116 7264 7414 7563 7712 7862 8036 9062 10932

-1 -1 -1 -1 -1 -1 -1 -1 -1

-1 -1 -1 -1 -1 -1 -1 -1 -1

7453 7609 7765 7792 8078 8235 8419 9602 -1

-1 -1 -1 -1 -1 -1 -1 -1 -1

-1 -1 -1 -1 -1 -1 -1 -1 -1

*** INPUT PARAMETERS ***

2 862 177356 3629 -1 259458 190964 190581 1 0

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ORIGINAL PAGE IS
OF POOR QUALITY

24 4130/00 0.00

מחלקת המחקר והפיתוח
מחלקת המכשירים והציוד

000 242 15 501 000

Fig. 9.

*** DETAILED FLIGHT PLAN ***

MIN. TRACK IN SPACE
FUEL

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CH 1160768 0.00

NO.	HEAD	FL	TOP	WAS	VIND	DIST	ACCD	TIME	ACCT	SURF	ELEV
											124524
100	51	350			0		151	27	27	4752	116776
113	51	350	0	464	0	12"	163	2"	26	157	116619
102	56	350	0	464	0	233"	396	30	58	2944	116673
103	62	350	0	464	0	150"	546	19	113	1650	114623
97	61	350	0	464	0	142"	688	16	136	1723	113106
91	59	350	0	464	0	99	767	13	149	1191	111939
87	51	350	0	464	0	160	967	23	212	2128	109781
75	59	350	0	464	0	136	1156	25"	237	2193	107543
64	64	350	0	464	0	415"	1571	54	331	4685	102696
50	71	390	0	463	0	373"	1944	46	419	4150	96744
36	80	390	0	463	0	345	2229	45	504	3570	95174
21	90	390	0	463	0	336"	2625	43	567	3340	91838
11	99	390	0	463	0	185	2810	24	611	1796	90042
0	108	390	0	463	0	93	2903	12	623	894	89148
2	124	390	0	463	0	147	3050	19	642	1392	87756
100	124	390	0	463	0	30	3060	4	646	284	87672
0					0		3193"	19	705"	1271	86201

TRIP FUEL 35327
COST 10357.21

*** END OF RUN ***

Fig. 10.

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*** DETAILED FLIGHT PLAN ***

INIT. TRACK 11 51702
FUEL

ON 1100768 0.00

NO.	HEAD	FL	TRF	TAS	WIND	DIST	ACCD	TIME	ACCT	CUM	WEIGHT
											124477
100	50	350			0		150	26	26	4720	119717
110	50	350	0	400	0	12	162	2	28	158	119550
100	60	350	0	400	0	232	394	30	58	2932	116627
100	61	350	0	400	0	180	544	19	117	1643	114784
97	60	350	0	400	0	142	686	16	136	1719	113065
97	50	350	0	400	0	99	785	13	169	1126	111879
87	40	350	0	400	0	130	905	23	212	2120	109759
70	30	350	0	400	0	130	1134	24	236	2154	107870
57	00	350	0	400	0	414	1308	54	330	4671	102000
50	07	390	0	400	0	372	1540	40	415	4143	98751
30	70	390	0	400	0	345	2205	45	503	3568	95183
21	60	390	0	400	0	330	2520	44	547	3338	91845
14	47	390	0	400	0	165	2603	24	611	1798	90040
0	107	390	0	400	0	92	2493	12	623	892	80154
0	122	390	0	400	0	147	3045	19	642	1361	87767
100	123	390	0	400	0	30	3075	4	646	264	87432
0					0		3108	19	705	1271	80212

INIT. FUEL 33240
COST 10335.78

*** END OF LOG ***

Fig. 11.

212

TEL. 444-1170
 CASH 15.10

2000 1000 500 0

Fig. 12.

*** DETAILED FLIGHT PLAN ***

MIN TRACK IN SPACE
FLTIME

CH 1190581 0.00

NO.	HEAD	FL	TMP	TAS	WIND	DIST	ACCD	TIME	ACCT	BURN	WEIGHT
											231393
TOC	46	310			29	120		20	20	5756	225637
113	46	310	-2	479	39	42	162	5	25	708	224929
108	66	310	-3	478	54	232	394	26	51	3741	221188
103	63	310	-4	477	65	150	544	17	107	2335	218853
97	62	310	-5	477	71	142	686	15	123	2167	216686
91	61	310	-5	476	81	99	785	11	134	1472	215214
87	51	350	2	475	100	180	965	19	152	2689	212525
77	54	310	-1	480	112	216	1181	22	214	2914	209611
65	62	310	3	484	116	407	1588	41	255	5525	204086
51	66	310	4	486	106	364	1952	37	332	4898	199188
37	72	350	5	478	104	336	2288	35	406	4445	194743
21	90	350	4	478	93	336	2624	35	441	4297	190446
11	89	310	0	482	55	185	2809	21	502	2521	187925
6	101	310	-1	480	44	93	2902	11	513	1330	186595
2	118	350	4	477	41	147	3049	17	530	2105	184490
TOD	121	310	-4	477	15	51	3100	6	536	683	183807
0					12		3192	16	552	1203	182604

TRIP FUEL 48789
COST 11129.51

*** END OF RUN ***

Fig. 13.

*** DETAILED FLIGHT PLAN ***

MIN TRACK IN SPACE
FLTIME

CH 1190581 0.00

NO.	HEAD	FL	TMP	TAS	WIND	DIST-	ACCD	TIME	ACCT	BURN	WEIGHT
											251697
✓ TOC	262	310			3		136	23	23	6611	245086
1	262	310	-4	477	3	0	136	-100	23	-2	245088
4	282	310	-1	480	-22	242	378	32	55	5065	240023
8	279	310	2	484	-36	115	493	16	111	2475	237548
17	292	310	3	485	-73	57	550	8	120	1313	236235
30	268	310	6	487	-39	397	947	54	214	8260	227975
44	268	310	7	489	-55	394	1341	55	308	8026	219949
60	270	310	7	488	-64	394	1735	56	404	7912	212037
75	265	310	2	484	-75	394	2129	59	503	7972	204065
87	261	310	-2	480	-78	179	2308	27	530	3588	200477
92	257	310	-4	477	-74	161	2469	24	554	3119	197338
98	238	310	-5	476	-80	66	2535	10	604	1283	196075
104	239	310	-4	477	-68	217	2752	32	636	4054	192021
109	246	310	-3	478	-50	189	2941	27	702	3330	188691
113	219	310	-2	479	-26	180	3121	24	726	2974	185717
TOD	237	310	-1	480	-22	77	3198	10	736	1262	184455
✓ 115					-17		3283	16	752	1203	183252

TRIP FUEL 68445
COST15383.19

*** DETAILED FLIGHT PLAN ***

CH 1190581 0.00

NO.	HEAD	FL	TMP	TAS	WIND	DIST	ACCD	TIME	ACCT	BURN	WEIGHT
											251699
2.3280,+01 0.0000,+00											
TOC	262	310.			3		136	23	23	6611	245088
2.3280,+01 0.0000,+00											
1	262	310	-4	477	3	0	136	0	23	0	245088
2.3280,+01 1.9204,+04											
4	282	310	-1	480	-22	242	378	32	55	5065	240023
2.3280,+01 9.4894,+03											
8	279	310	2	484	-36	115	493	16	111	2475	237548
2.3280,+01 5.0680,+03											
17	292	310	3	485	-73	57	550	8	120	1313	236235
2.3280,+01 3.2515,+04											
30	268	310	6	487	-39	397	947	54	214	8260	227975
2.3280,+01 3.2738,+04											
44	268	310	7	489	-55	394	1341	55	308	8026	219949
2.3280,+01 3.3479,+04											
60	270	310	7	488	-64	394	1735	56	404	7912	212037
2.3280,+01 3.5169,+04											
75	265	310	2	484	-75	394	2129	59	503	7972	204065
2.3280,+01 1.6322,+04											
87	261	310	-2	480	-78	179	2308	27	530	3588	200477
2.3280,+01 1.4450,+04											
92	257	310	-4	477	-74	161	2469	24	554	3119	197358
2.3280,+01 6.0011,+03											
98	238	310	-5	476	-80	66	2535	10	604	1283	196075
2.3280,+01 1.9166,+04											
104	239	310	-4	477	-68	217	2752	32	636	4054	192021
2.3280,+01 1.5906,+04											

Fig. 14-2.

109	246	310	-3	478	-50	189	2941	27	702	3330	188691
2.3280,+01			1.4323,+04								
113	219	310	-2	479	-26	180	3121	24	726	2974	185717
1.5810,+01			6.1052,+03								
TOD	237	310	-1	480	-22	77	3198	10	737	1262	184455
1.5810,+01			6.1052,+03								
115					-17		3283	16	752	1203	183252

TRIP FUEL 68447
COST15383.64

*** END OF RUN ***

PROGRAM COMPLETED IN 130.1426 CRU.

END OF RUN:	137 CRU	ACCOUNT:	510055.1	CARDS:	4 IN	0 OUT	P
BASE CRU:	137.035	SEQ. NO.	122425	CPU TIME:	130.79 SEC.		E
CORE FACTOR:	1.000	DATE:	22 MAY 81	TIME:	19:59:28		T
TOTAL:	5852 CRU	LIMIT:	7500				

Fig. 15.

*** DETAILED FLIGHT PLAN ***

MIN TRACK IN SPACE
FUEL

CH 1190581 0.00

NO.	HEAD	FL	TMP	TAS	WIND	DIST	ACCD	TIME	ACCT	BURN	WEIGHT
											232421
TOC	46	310			29	-	121	20	20	5796	226625
113	46	310	-2	479	39	41	162	5	25	694	225931
108	66	350	2	475	55	232	394	26	51	4622	221309
103	63	350	1	474	66	150	544	17	108	2407	218902
97	62	350	1	474	74	142	686	16	123	2210	216692
91	62	350	1	474	85	99	785	11	134	1496	215196
87	51	350	2	475	102	180	965	19	153	2598	212598
77	55	350	4	477	114	216	1181	22	215	3002	209596
65	62	350	6	479	116	407	1588	41	256	5493	204103
51	66	350	6	479	110	364	1952	37	333	4814	199289
37	72	350	5	478	106	336	2288	35	407	4368	194921
21	90	350	4	478	99	336	2624	35	443	4317	190604
11	89	350	5	478	65	185	2809	21	503	2491	188113
6	101	390	3	476	47	93	2902	11	514	1989	186124
2	118	390	4	476	41	147	3049	17	531	2023	184101
TOD	121	390	4	477	22	26	3075	3	534	361	183740
0					17		3192	19	553	1271	182469

TRIP FUEL 49952
COST 11320.37

Fig. 16.

*** DETAILED FLIGHT PLAN ***

MIN TRACK IN SPACE
FLTIME

CH 1190581 0.00

NO.	HEAD	FL	TMP	TAS	WIND	DIST	ACCD	TIME	ACCT	BURN	WEIGHT
											233624
TOC	46	310			29		122	20	20	5843	227781
113	46	310	-2	479	39	40	162	5	25	678	227103
108	66	310	-4	478	56	232	394	26	51	3787	223316
103	63	310	-4	477	66	150	544	17	108	2360	220956
97	62	310	-5	476	73	142	686	15	123	2185	218771
91	61	310	-5	477	84	99	785	11	134	1488	217283
87	51	(350)	2	(475)	102	180	965	19	152	3331	213952
77	54	310	-1	480	112	216	1181	22	214	2986	210966
65	62	310	2	483	116	407	1588	41	255	5554	205412
51	66	310	4	486	109	364	1952	37	332	4930	200482
37	72	(350)	5	(478)	106	336	2288	35	406	5096	195386
21	90	(350)	4	(478)	99	336	2624	35	442	4331	191055
11	89	310	1	482	62	185	2809	21	502	2580	188475
6	101	310	-1	481	49	93	2902	11	513	1333	187142
2	118	350	4	477	42	147	3049	17	530	2717	184425
TOD	121	310	-4	477	19	51	3100	6	536	727	183698
0					14		3192	16	552	1203	182495

TRIP FUEL 51129
COST11480.87

*** END OF RUN ***

Fig. 17.

*** DETAILED FLIGHT PLAN ***

MIN TRACK IN SPACE
FUEL

CH 1190581 0.00

NO.	HEAD	FL	TMP	TAS	WIND	DIST	ACCD	TIME	ACCT	BURN	WEIGHT
232450											
TOC	46	310			29		121	20	20	5797	226653
113	46	310	-2	479	39	41	162	5	25	694	225959
108	66	350	2	475	55	232	394	26	51	4622	221337
103	63	350	1	474	66	150	544	17	108	2407	218930
97	62	350	1	474	74	142	686	16	123	2210	216720
91	62	350	1	474	85	99	785	11	134	1496	215224
87	51	350	2	475	102	180	965	19	153	2598	212626
77	55	350	4	477	114	216	1181	22	215	3002	209624
65	62	350	6	479	116	407	1588	41	256	5493	204131
51	66	350	6	479	110	364	1952	37	333	4814	199317
37	72	350	5	478	106	336	2288	35	407	4361	194956
21	90	350	4	478	99	336	2624	35	443	4317	190639
11	89	350	5	478	65	185	2809	21	503	2491	188148
6	101	390	3	476	47	93	2902	11	514	1991	186157
2	118	390	4	476	41	147	3049	17	531	2023	184134
TOD	121	390	4	477	22	26	3075	3	534	361	183773
0					17		3192	19	553	1271	182502

TRIP FUEL 49948
COST 11319.77

Fig. 18.

*** DETAILED FLIGHT PLAN ***

MIN TRACK IN SPACE
FLTIME

CH 1190581 0.00

NO.	HEAD	FL	TMP	TAS	WIND	DIST	ACCD	TIME	ACCT	BURN	WEIGHT
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233643

TOC	46	310			29		122	20	20	5844	227799
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113	46	310	-2	479	39	40	162	5	25	678	227121
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108	66	310	-4	478	56	232	394	26	51	3787	223334
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103	63	310	-4	477	66	150	544	17	108	2360	220974
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97	62	310	-5	476	73	142	686	15	123	2185	218789
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91	61	310	-5	477	84	99	785	11	134	1488	217301
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87	51	350	2	475	102	180	965	19	152	3331	213970
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77	54	310	-1	480	112	216	1181	22	214	2986	210984
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65	62	310	2	483	116	407	1588	41	255	5545	205439
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51	66	310	4	486	109	364	1952	37	332	4930	200509
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37	72	350	5	478	106	336	2288	35	406	5096	195413
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21	90	350	4	478	99	336	2624	35	442	4331	191082
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11	89	310	1	482	62	185	2809	21	502	2580	188502
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6	101	310	-1	481	49	93	2902	11	513	1333	187169
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2	118	350	4	477	42	147	3049	17	530	2714	184455
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TOD	121	310	-4	477	19	51	3100	6	536	727	183728
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0					14		3192	16	552	1203	182525
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TRIP FUEL 51118

COST11479.22

*** END OF RUN ***

Fig. 19.

*** DETAILED FLIGHT PLAN ***

MIN TRACK IN SPACE
FUEL

CH 2190581 0.00

NO.	HEAD	FL	TMP	TAS	WIND	DIST	ACCD	TIME	ACCT	BURN	WEIGHT
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252998

TOC	262	310			3		136	24	24	6678	246320
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1	262	310	-4	477	3	0	136	0	24	0	246320
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4	282	310	-1	480	-22	242	378	32	56	5105	241215
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8	279	310	2	484	-36	115	493	16	111	2490	238725
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17	292	310	3	485	-73	57	550	8	120	1320	237405
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30	268	310	6	487	-39	397	947	54	214	8306	229099
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44	268	350	7	480	-57	394	1341	56	310	9187	219912
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60	270	350	7	480	-66	394	1735	57	407	8142	211770
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75	264	350	5	478	-74	394	2129	60	507	7979	203791
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87	260	350	2	475	-78	179	2308	28	534	3549	200242
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92	257	350	1	474	-74	161	2469	24	559	3063	197179
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98	238	350	1	474	-78	66	2535	10	609	1250	195929
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104	239	350	1	474	-66	217	2752	32	641	3926	192003
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109	246	350	2	475	-48	189	2941	27	707	3197	188806
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113	219	390	2	474	-28	180	3121	24	731	3590	185216
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TOD	236	390	0	473	-27	55	3176	7	739	875	184341
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115					-20		3283	19	758	1271	183070
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TRIP FUEL 69928

COST 15666.98

026704

*** DETAILED FLIGHT PLAN ***

Fig. 20.

*** DETAILED FLIGHT PLAN ***

MIN TRACK IN SPACE
FUEL

CH 2190581 0.00

NO.	HEAD	FL	TMP	TAS	WIND	DIST	ACCD	TIME	ACCT	BURN	WEIGHT
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253489

TOC	262	310			3		126	24	24	6704	246785
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1	262	310	-4	477	3	10	136	1	25	200	246585
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4	282	310	-1	480	-22	242	378	32	57	5105	241480
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8	279	310	2	484	-36	115	493	16	113	2490	238990
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17	292	310	3	485	-73	57	550	8	121	1323	237667
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30	268	310	6	487	-39	397	947	54	215	8322	229345
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44	268	350	7	480	-57	394	1341	56	311	9203	220142
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60	270	350	7	480	-66	394	1735	57	409	8142	212000
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75	264	350	5	478	-74	394	2129	60	508	7993	204007
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87	260	350	2	475	-78	179	2308	28	536	3555	200452
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92	257	350	1	474	-74	161	2469	24	560	3068	197384
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98	238	350	1	474	-78	66	2535	10	610	1250	196134
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104	239	350	1	474	-66	217	2752	32	642	3926	192208
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109	246	350	2	475	-48	189	2941	27	709	3202	189006
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113	219	390	2	474	-28	180	3121	24	733	3594	185412
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TOO	236	390	0	473	-27	67	3188	9	742	1056	184356
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115					-20		3283	19	801	1271	183085
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TRIP FUEL 70404

COST 15769.97

Program Listing (DC10).

Δ ELT DC10,1,810528,065609

COMMENT KNMI/KLM 020169 SPG NAV 20 JNG,
NAVIGATION-FLIGHTPLANNING-MODULE FOR THE PRODUCTION OF
FLIGHTPLANS OVER THE NORTH ATLANTIC.
THE MAIN FEATURES

ARE:

1. INCLUSION OF 6 METEOROLOGICAL PARAMETER FIELDS,
TEMPERATURE AND WIND DATA FOR 300,250 AND 200MB
VALID FOR TWO STANDARD TIMES 12 HOURS APART.
2. WEATHER INFO. COMES FROM NATIONAL WEATHER SERVICE.
3. INCLUSION OF A DYNAMIC PROCESS BASED ON INTERPOLATION OF
TWO PARAMETER FIELDS.
4. OPTIMALISATION OF FUEL, COSTS OR FLIGHT TIME IN SPACE AS
WELL AS IN THE HORIZONTAL AS IN THE VERTICAL.
5. IN - AND OUTBOUND TRAFFIC (IO= 1 OUTBOUND IO= -1 INBOUND).
6. FLIGHTPLAN PRODUCTION FOR OPTIMUM TRACKS, SPECIFIC ROUTES
ETC. E.G. ALTERNATIVE ATC MINIMUM ROUTES.
7. BLOCKING E.G. SECTOR BLOCKING OVER THE NORTH ATLANTIC
BLOCKING IN AIRWAYS AND ATC RESTRICTED AREAS.
8. STANDARD CRUISE AND USE OF PERFORMANCE TABLES

CONSTANT KQ= 14 , W= 35

INTEGER P1,P2,P3,Q1,Q2,Q3,S,TTT,

G1,G2,G3,G4,B1,B2,B3,MQ,G1Q,G2Q,Q,

RES1,RES2,RES3,I,J,N1,N2,N3,M,G,

M0,M1,M2,M3,M4,M5,M6,K,IO,

A1,A2,A3,A4,A5,T1,T2,T3,KOUNT,

K1,K2,L1,L2,K1Q,K2Q,L1Q,L2Q,KK1,KK2,LL1,LL2,

FLUR,TAXI,TOW,GRW,RESERVE,MAXTOW,MAXLW,

DATE,ST,ST1,ROUTE,DISTANCE,FLTIME,BURN,

GRWQ,TOWQ,LW,COST,LE,TEL\$

REAL C0,CG,P,C1,X1,X2,Y1,Y2,X,Y,E1,E2,E3,

GG1,GG2,D,ANGLE,LALAT,LALONG,TT,LA1,LO1,LA2,LO2,

XX1,XX2,YY1,YY2,AID1,AID2,AID3,AID4,XSTER,YSTER,

MINTIME,TC,TASM,WX,WY,TAS,ENDU,TEM\$

INTEGER ARRAY A(-1..KQ+1), V(0..41),

TEMPTIME,TEMPDIST,TEMPFUEL(1..99, 1..9), MW(1..3, 1..7),

RANGE(1..3, 1..33)\$

ARRAY DD(0..KQ)\$

ARRAY WCX,WCY,TPC(1..120, 1..34)\$

BOOLEAN ED\$

BOOLEAN ARRAY BK(0..2,1..6,1..6), BKQ(9..KQ,1..6,1..6)\$

FORMAT F01(E2, S10, D7.0, A5),

PEJT (E2, ' ', A1),

FOT(X5, *I6, A2),

FOD(*I6, A1),

F02(X5, *I7, A2)\$

LOCAL LABEL ERR,EOP\$

COMMENT PROCEDURE 'WDATA' SCANS WEATHER DATA AND OBTAINS
THE REQUIRED WEATHER INFO. FOR NORTH AMERICA AND
NORTH ATLANTIC AREA \$

ΔK* >WK[DA[AGA Δ

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```

PROCEDURE WDATA$
BEGIN INTEGER I,X,Y1,Y2,Y3,R,T,U,V$
STRING ARRAY WD(7..1..120,1..34)$
STRING S(81)$
STRING TW(AG(2), SP(3), TP(2))$
  STRING BA(BD(1),BL(3),AR(2),TM(1),B(3)),
    GW(UG(2),W1(7),WWW(W2(7),W3(7),W4(7)),HH(2),G(4)),
    SW (WT(2),DR(2),WS(3))$
LOCAL LABEL FINIS
FORMAT F(A,S80)$
FORMAT F1(*S8, A1),
  F2('BLOCKETTE H=',S3,' AREA = NORTH AMERICA' , A1),
  F4('BLOCKETTE H=',S3,' AREA = NORTH ATLANTIC', A1),
  F5(3(X3,S7), A1),
  FW(*I6,A1),
  PJ(E2,' ',A1)$

```

```

PROCEDURE CHOPS$
BEGIN INTEGER K,L$
IF I LEQ 45 THEN
  BEGIN GW(1,36)=S(I,36)$ I=I+36$
    IF I GTR 80 THEN
      BEGIN READ(PCF('NWS'),F,S,FINI)$ I=1$ ENDS
    END
  ELSE BEGIN K=81-I$ GW(1,K)=S(I,K)$ READ(PCF('NWS'),F,S,FINI)$
    L=36-K$ GW(K+1, L)=S(1,L)$ I=L+1$
  ENDS
  IF S(I) EQL '\ ' THEN
    BEGIN READ(PCF('NWS'),F,S,FINI)$ I=1$
  ENDS
END$ COMMENT CHOPS$

```

```

PROCEDURE STOR$
BEGIN INTEGER J$
LOCAL LABEL L3$
STRING ARRAY SA(36..1..8)$
FOR J=1 STEP 1 UNTIL 8 DO
  BEGIN CHOPS$ SA(1,36..J)=GW$ ENDS
FOR J=1 STEP 1 UNTIL 4 DO
  BEGIN GW=SA(1,36..J)$
    IF ALPHABETIC(WWW) THEN
      BEGIN WRITE('W-ERROR')$ WRITE(WWW)$ GOTO L3$
    ENDS
    WD(1,7..Y1,X)=W2$
    WD(1,7..Y2,X)=W3$
    WD(1,7..Y3,X)=W4$
    Y1=Y1-1$ Y2=Y2-1$ Y3=Y3-1$
  ENDS
  X=X-1$ Y1=Y1+4$ Y2=Y2+4$ Y3=Y3+4$
FOR J=5 STEP 1 UNTIL 8 DO
  BEGIN GW=SA(1,36..J)$

```

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        IF ALPHABETIC(WWW) THEN
            BEGIN WRITE('W-ERROR')$ WRITE(WWW)$ GOTO L3$
            END$
        WD(1,7..Y1,X)=W2$
        WD(1,7..Y2,X)=W3$
        WD(1,7..Y3,X)=W4$
        Y1=Y1-1$ Y2=Y2-1$ Y3=Y3-1$
    END$
L3.. END$ COMMENT STORS

```

```

PROCEDURE AREAS$
BEGIN INTEGER K,L$
IF I LEQ 71 THEN
    BEGIN BA(1,10)=S(I,10)$ I=I+10$
        IF I GTR 80 THEN
            BEGIN READ(PCF('NWS'),F,S,FINI)$ I=1$ END$
        END
    ELSE BEGIN K=81-I$ BA(1,K)=S(I,K)$
        READ(PCF('NWS'),F,S,FINI)$ L=10-K$
        BA(K+1,L)=S(1,L)$ I=L+1$
    END$
IF S(I) EQL '\ ' THEN
    BEGIN READ(PCF('NWS'),F,S,FINI)$ I=1$
    END$
END$ COMMENT AREAS$

```

```

PROCEDURE FINDNEXT$
BEGIN
IF S(I) EQL ' ' THEN
    FOR I=I WHILE S(I) NEQ '*' DO
        BEGIN READ(PCF('NWS'),F,S,FINI)$ I=1$
        END$
    END$
END$

```

```

PROCEDURE GETDATA$
BEGIN INTEGER GMT,A,B,C,D,E,F,J,S,T$
LOCAL LABEL L5, NAM, NAT$
A=20$ B=40$ C=60$ D=80$ E=100$ F=120$
AREAS$
IF AR EQL '21' THEN
    BEGIN IF TM EQL '1' THEN
        BEGIN GMT=0$ X=14$ Y1=A$ Y2=B$ Y3=C$
            WRITE('GMT = 0000')$
        END
    ELSE IF TM EQL '3' THEN
        BEGIN GMT=12$ X=14$ Y1=D$ Y2=E$ Y3=F$
            WRITE('GMT = 1200')$
        END
    ELSE BEGIN WRITE('W-ERROR')$ GOTO L5$ END$
GOTO NAM$
END

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ELSE IF AR EQL '22' THEN
  BEGIN IF TM EQL '1' THEN
    BEGIN GMT=0$ X=34$ Y1=A$ Y2=B$ Y3=C$
      WRITE('GMT = 0000')$
    END
    ELSE IF TM EQL '3' THEN
      BEGIN GMT=12$ X=34$ Y1=D$ Y2=E$ Y3=F$
        WRITE('GMT = 1200')$
      END
      ELSE BEGIN WRITE('W-ERROR')$ GOTO L5$ ENDS
    GOTO NAT$
  ENDS$
  WRITE('W-ERROR')$
  GOTO L5$
NAM.. FOR S=1 STEP 1 UNTIL 7 DO
  BEGIN FOR T=1 STEP 1 UNTIL 5 DO
    BEGIN
      WRITE(F2,BL)$
      STOR$ X=X+1$ AREA$
      IF NUMERIC(BL) THEN
        IF INTEGER(BL) GEQ 259 THEN
          FOR J=1 STEP 1 UNTIL 3 DO CHOP
            ELSE J=1
          ELSE BEGIN WRITE('W-ERROR')$ GOTO L5$
            ENDS$
        ENDS$
        X=X-2$
        IF GMT EQL 0 THEN
          BEGIN Y1=A$ Y2=B$ Y3=C$ END
        ELSE BEGIN Y1=D$ Y2=E$ Y3=F$ ENDS$
        IF S LSS 7 THEN AREA$
      ENDS$
      GOTO L5$
    NAT.. FOR S=1 STEP 1 UNTIL 10 DO
      BEGIN FOR T=1 STEP 1 UNTIL 5 DO
        BEGIN
          WRITE(F4,BL)$
          STOR$ X=X+1$ AREA$
          IF NUMERIC(BL) THEN
            IF INTEGER(BL) GEQ 253 THEN
              FOR J=1 STEP 1 UNTIL 3 DO CHOP
                ELSE J=1
              ELSE BEGIN WRITE('W-ERROR')$ GOTO L5$
                ENDS$
            ENDS$
            X=X-2$
            IF GMT EQL 0 THEN
              BEGIN Y1=A$ Y2=B$ Y3=C$ END
            ELSE BEGIN Y1=D$ Y2=E$ Y3=F$ ENDS$
            IF S LSS 10 THEN AREA$
          ENDS$
        L5.. ENDS$ COMMENT GETDATA$

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PROCEDURE SCANS$
BEGIN
LOCAL LABEL BEGN,LO$
BEGN.. READ(PCF('NWS'),F,S,FINI)$
I=1$
LO.. IF S(I,2) EQL '**' THEN
BEGIN I=I+38$ GETDATA$ FINDNEXT$ GOTO LO$
END
ELSE GOTO BEGN$
END$ COMMENT SCANS$

COMMENT COMPUTATION OF X,Y COMPONENTS OF WIND VECTORS$

PROCEDURE WINDCOMP(X,Y)$
VALUE X,Y$
INTEGER X,Y$
BEGIN REAL A$
IF X GTR 36 THEN WRITE('WIND ANGLE ERROR')$
IF X LEQ 9 THEN
BEGIN A=(90-X*10)*CG$
WX=-Y*COS(A)$
WY=-Y*SIN(A)$

END
ELSE IF X LEQ 18 THEN
BEGIN A=(X*10-90)*CG$
WX=-Y*COS(A)$
WY=Y*SIN(A)$

END
ELSE IF X LEQ 27 THEN
BEGIN A=(270-X*10)*CG$
WX=Y*COS(A)$
WY=Y*SIN(A)$

END
ELSE BEGIN A=(X*10-270)*CG$
WX=Y*COS(A)$
WY=-Y*SIN(A)$

END$
END$ COMMENT WINDCOMP$

COMMENT LINEAR INTERPOLATIONS$

INTEGER PROCEDURE INTP(F,F1,F2,F1Q,F2Q)$
INTEGER F,F1,F2,F1Q,F2Q$
INTP=((F-F1)*F2Q + (F2-F)*F1Q) / (F2-F1)$
COMMENT INTP$

SCANS$
FINI..
FOR R=0 STEP 1 UNTIL 5 DO
BEGIN T=R*20$ WRITE(PJ)$
WRITE('* WEATHER DATA IN 3 STANDARD PRESSURE LEVELS *')$

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WRITE('* 34X16 DATA OUT OF 34X20 GRIDPOINTS *')$
WRITE('* TEMPERATURE, DIRECTION, SPEED *')$
WRITE(' ')$ WRITE(' ')$
FOR U=1 STEP 1 UNTIL 34 DO
    WRITE( F1, 20, FOR V=T+20 STEP -1
        UNTIL T+5 DO WD(1,7..V,U))$
END$

COMMENT CONVERSION OF WEATHER INFO. IN STANDARD PRESSURE LEVELS
BY INTERPOLATION SCHEME TO WEATHER INFO. IN FLIGHT LEVELS$

FOR I=1 STEP 1 UNTIL 20, 61 STEP 1 UNTIL 80 DO
    FOR J=1 STEP 1 UNTIL 34 DO
        BEGIN
            SW=WD(1,7..I,J)$
            M1=INTEGER(DR)$
            M2=INTEGER(WS)$
            T1=INTEGER(WT)$
            IF M1 GEQ 50 THEN BEGIN M1=M1-50$ T1=-T1$ ENDS$
            WINDCOMP(M1,M2)$
            M1=WX$ M2=WY$
            SW=WD(1,7..I+20,J)$
            M3=INTEGER(DR)$
            M4=INTEGER(WS)$
            T2=INTEGER(WT)$
            IF M3 GEQ 50 THEN BEGIN M3=M3-50$ T2=-T2$ ENDS$
            WINDCOMP(M3,M4)$
            M3=WX$ M4=WY$
            SW=WD(1,7..I+40,J)$
            M5=INTEGER(DR)$ M6=INTEGER(WS)$
            T3=INTEGER(WT)$
            IF M5 GEQ 50 THEN BEGIN M5=M5-50$ T3=-T3$ ENDS$
            WINDCOMP(M5,M6)$
            M5=WX$ M6=WY$
            WCX(I,J)=INTP(P1,Q1,Q2,M1,M3)$
            WCY(I,J)=INTP(P1,Q1,Q2,M2,M4)$
            TPC(I,J)=INTP(P1,Q1,Q2,T1,T2)$
            WCX(I+20,J)=INTP(P2,Q2,Q3,M3,M5)$
            WCY(I+20,J)=INTP(P2,Q2,Q3,M4,M6)$
            TPC(I+20,J)=INTP(P2,Q2,Q3,T2,T3)$
            WCX(I+40,J)=INTP(P3,Q2,Q3,M3,M5)$
            WCY(I+40,J)=INTP(P3,Q2,Q3,M4,M6)$
            TPC(I+40,J)=INTP(P3,Q2,Q3,T2,T3)$
        ENDS$

        FOR A1=0 STEP 1 UNTIL 5 DO
            BEGIN A2= A1*20$ WRITE(PEJT)$
            WRITE('*INTERPOLATED GRIDPOINT VALUES IN FLIGHT LEVELS*')$
            WRITE('*X-COMPONENTS OF WIND DATA*')$
            WRITE(' ')$ WRITE(' ')$
            FOR A4=1 STEP 1 UNTIL 34 DO
                WRITE(FW, 20, FOR A5=A2 + 20 STEP -1
                    UNTIL A2+1 DO WCX(A5, A4))$
            ENDS$

```


END\$ COMMENT END OF WEATHER DATA COLLECTION\$

P1=31000\$ P2=35000\$ P3=39000\$
Q1=30065\$ Q2=33999\$ Q3=38662\$
TEL=0\$
CG=0.0174532925\$
TASM=0.82*38.9826\$

WRITE('* SCANNING WEATHER DATA IN NORTH AMERICA AND-')\$
WRITE(' NORTH ATLANTIC AREA *')\$

WDATAS

COMMENT RELATIONSHIP BETWEEN GRAPH POINT NUMBERS AND ZONE INDICES\$
A(-1)= -1\$ A(0)= 0\$ A(1)= 2\$ A(2)= 6\$ A(3)= 11\$ A(4)= 26\$
A(5)= 41\$ A(6)= 56\$ A(7)= 71\$ A(8)= 86\$ A(9)= 90\$ A(10)= 96\$
A(11)= 102\$ A(12)= 107\$ A(13)= 111\$ A(14)= 114\$ A(15)= 115\$

COMMENT COORDINATES OF CHECK POINTS\$

V(0)= 52290477\$
V(1)= 51850115\$ V(2)= 53640150\$
V(3)= 51000200\$ V(4)= 51990539\$ V(5)= 53580300\$
V(6)= 55000200\$ V(7)= 49980632\$ V(8)= 51840849\$
V(9)= 52700892\$ V(10)= 53500630\$ V(11)= 55490459\$
V(12)= 54271005\$ V(13)= 48905454\$ V(14)= 51375560\$
V(15)= 53735697\$ V(16)= 58476263\$ V(17)= 47005800\$
V(18)= 48545856\$ V(19)= 55506000\$ V(20)= 57006000\$
V(21)= 53286035\$ V(22)= 54836683\$ V(23)= 46156006\$
V(24)= 48006000\$ V(25)= 49846439\$ V(26)= 50506500\$
V(27)= 51006750\$ V(28)= 52006900\$ V(29)= 45006300\$
V(30)= 46176459\$ V(31)= 47506600\$ V(32)= 48576826\$
V(33)= 50007050\$ V(34)= 43836608\$ V(35)= 44846867\$
V(36)= 45327179\$ V(37)= 45467385\$ V(38)= 41287003\$
V(39)= 42367099\$ V(40)= 43007250\$ V(41)= 40647378\$

COMMENT DETERMINATION OF CONNECTIVITY AMONG GRAPH POINTS.
FALSE=CONNECTED, TRUE=BLOCKED \$

FOR I= 1 STEP 1 UNTIL 6 DO

FOR J= 1 STEP 1 UNTIL 6 DO

BEGIN

FOR MQ= 0,1,2 DO BK(MQ,I,J) = TRUE\$

FOR MQ= 9 STEP 1 UNTIL KQ DO BKQ(MQ,I,J) = TRUE

END\$

BK(1,1,1)= BK(2,1,1)= BK(1,2,2)= BK(2,2,2)=

BKQ(9,1,1)= BKQ(10,1,1)= BKQ(11,1,1)= BKQ(12,1,1)=

BKQ(13,1,1)= BKQ(14,1,1)= BKQ(9,2,2)= BKQ(10,2,2)=

BKQ(11,2,2)= BKQ(12,2,2)= BKQ(13,2,2)= BKQ(10,3,3)=

BKQ(11,3,3)= BKQ(13,3,3)= BKQ(11,4,4)= BK(2,3,4)= BK(2,4,5)=

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BKQ(12,4,4) = BKQ(10,6,6) = BK(1,1,2) =
BK(1,2,3) = BK(1,2,4) = BK(2,2,3) =
BKQ(9,1,2) = BKQ(9,2,3) = FALSE$
BKQ(9,2,5) = BKQ(9,3,4) = BKQ(9,3,5) = BKQ(9,4,6) = BKQ(10,2,1) =
BKQ(10,4,3) = BKQ(10,5,3) = BKQ(10,5,4) = BKQ(10,6,5) =
BKQ(11,1,2) = BKQ(11,3,4) = BKQ(11,5,4) = FALSE$
BKQ(11,6,5) = BKQ(12,2,1) = BKQ(12,3,2) = BKQ(12,4,3) =
BKQ(12,5,4) = BKQ(13,1,2) = BKQ(14,2,1) = BKQ(14,3,1) = BK(0,1,1) =
BK(0,1,2) = FALSE$

```

```

BEGIN

```

```

REAL ARRAY AB(0..10), LENGTH(1..10),
HEADING(1..W),
TIME,AIRDIST,TDEV,WIX,WIY,TAX,TAY(1..W)$
REAL COSA,COSD$
LOCAL LABEL DONE$

```

```

INTEGER PROCEDURE ZONEI(Q)$ INTEGER Q$
COMMENT THIS SUBROUTINE DETERMINES THE INDEX OF THE
ZONE ASSOCIATED WITH A STATIONSNUMBER$

```

```

BEGIN

```

```

LOCAL LABEL AGAIN$ INTEGER I$
I = -1$

```

```

AGAIN..

```

```

I = I+1$ IF A(I)-Q LSS 0 THEN GOTO AGAIN$
ZONEI = I

```

```

END$ COMMENT ZONEI$

```

```

PROCEDURE DT(K)$ INTEGER K$
COMMENT THIS SUBROUTINE DISSECTS LATITUDE AND
LONGITUDE FROM THE COMPRESSED COORDINATES$
BEGIN

```

```

INTEGER K0$
K0 = ENTIER(V(K)/10000)$
LALAT = K0/100$
LALONG = (V(K)-10000*K0)/100

```

```

END$ COMMENT DISSECTS$

```

```

PROCEDURE LIS(U)$ INTEGER U$
COMMENT DETERMINATION OF LATITUDE AND LONGITUDE FOR
GRAPH POINTS$
COMMENT THE SIGN OF LONGITUDE IS CHANGED FOR
EAST OF GREENWHICH$

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```

BEGIN

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```

IF U EQL 19 THEN DT(12)
ELSE IF U LEQ 11 THEN
BEGIN
DT(U)$ IF U EQL 0 OR U EQL 1 OR
U EQL 2 THEN LALONG = -LALONG

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END

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ELSE IF U LEQ 26 THEN
BEGIN

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LALAT = 35+U$ LALONG = 10

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END	****432
ELSE IF U LEQ 41 THEN	****433
BEGIN	****434
LALAT= 20+U\$ LALONG= 20	****435
END	****436
ELSE IF U LEQ 56 THEN	****437
BEGIN	****438
LALAT= 5+U\$ LALONG= 30	****439
END	****440
ELSE IF U LEQ 71 THEN	****441
BEGIN	****442
LALAT= U-11\$ LALONG= 40	****443
END	****444
ELSE IF U LEQ 86 THEN	****445
BEGIN	****446
LALAT= U-26\$ LALONG= 50	****447
END	****448
ELSE DT(U-74)	****449
END\$ COMMENT LISS	****450
PROCEDURE CTQ\$	****451
COMMENT THIS SUBROUTINE PREPARES THE TIME INSTANTS AT WHICH	****452
IN EACH ZONE THE METEOROLOGICAL PARAMATER WILL BE	****453
DERIVED FROM BOTH PARAMETER FIELDS, COMPOSITE CHARTS	****454
IN TIME ARE SIMULATED\$	****455
BEGIN	****456
INTEGER JO,M0\$	****457
REAL A,SUM,RES\$	****458
A= 0.4\$	****459
JO = IF IO EQL 1 THEN KQ ELSE 0\$ SUM= 0\$	****460
FOR I= KQ-JO STEP IO UNTIL JO DO	****461
BEGIN	****462
SUM= SUM+(IF I GTR 3 AND I LSS 8 THEN 2*A ELSE A)\$	****463
DD(I)= SUM	****464
END\$	****465
M0 = ZONEI(ST)\$ RES= IF IO EQL 1 THEN DD(M0) ELSE	****466
DD(M0-1)\$	****467
FOR I= 0 STEP 1 UNTIL KQ DO DD(I)= IF TT GTR 12	****468
THEN TT-12 ELSE TT+A/2+DD(I)-RES\$	****469
END\$ COMMENT CTQ\$	****470
COMMENT COMPUTATION OF GRID POINT VALUES FOR DYNAMIC PROCESS\$	****471
REAL PROCEDURE HH(V,W,F,SELECT)\$	****472
VALUE F,V,W,SELECT\$	****473
INTEGER F,V,W,SELECT\$	****474
BEGIN	****475
M5= (F-1)*20\$	****476
M6= (F+2)*20\$	****477
IF SELECT EQL 1 THEN	****478
BEGIN M1=WCX(V+M5,W)\$ M2=WCX(V+M6,W)\$	****479
HH=((12-DD(M))*M1 + DD(M)*M2) /12\$ END	****480
ELSE IF SELECT EQL 2 THEN	****481
BEGIN M3=WCY(V+M5,W)\$ M4=WCY(V+M6,W)\$	****482
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      HH=((12-DD(M))*M3 + DD(M)*M4) /12$ END
    ELSE BEGIN T1=TPC(V+M5, W)$ T2=TPC(V+M6, W)$
      HH=((12-DD(M))*T1 + DD(M)*T2) /12$ ENDS
    ENDS COMMENT HH$

```

COMMENT COMPUTATION OF GRID POINT VALUE BY BI-LINEAR INTERPOLATION
FOR AN ARBITRARY POINT (TEMP., DIRECTION AND SPEED)\$

```

REAL PROCEDURE GEOP(V,W,C,SELECT)$
VALUE C,SELECT,V,W$
INTEGER C,SELECT$ REAL V,W$
BEGIN
  INTEGER V1,W1$ REAL A,B,B1,B2,B3,B4$
  V1= ENTIER(V)$ W1= ENTIER(W)$
  B1=IF SELECT EQL 1 THEN HH(V1,W1,C,1)
    ELSE IF SELECT EQL 2 THEN HH(V1,W1,C,2)
      ELSE HH(V1,W1,C,3)$
  B2=IF SELECT EQL 1 THEN HH(V1+1,W1,C,1)
    ELSE IF SELECT EQL 2 THEN HH(V1+1,W1,C,2)
      ELSE HH(V1+1,W1,C,3)$
  B3=IF SELECT EQL 1 THEN HH(V1+1,W1+1,C,1)
    ELSE IF SELECT EQL 2 THEN HH(V1+1,W1+1,C,2)
      ELSE HH(V1+1,W1+1,C,3)$
  B4=IF SELECT EQL 1 THEN HH(V1,W1+1,C,1)
    ELSE IF SELECT EQL 2 THEN HH(V1,W1+1,C,2)
      ELSE HH(V1,W1+1,C,3)$
  A= V1+1-V$ B= W1+1-W$
  GEOP= A*B*B1+(1-A)*B*B2+(1-A)*(1-B)*B3+A*(1-B)*B4$
  ENDS COMMENT GEOP$

```

COMMENT COMPUTATION OF GREAT CIRCLE DISTANCE BETWEEN TWO
POINTS BY USING THE GONIOMETRIC RELATIONS\$

```

REAL PROCEDURE GEODIST(LAT1,LON1,LAT2,LON2)$
VALUE LAT1,LAT2,LON1,LON2$
REAL LAT1,LAT2,LON1,LON2$
BEGIN
  LOCAL LABEL SKP$
  IF LAT1 EQL LAT2 AND LON1 EQL LON2 THEN
    BEGIN GEODIST=0$ GOTO SKP$ ENDS
  GEODIST=60*ARCCOS(SIN(LAT1*CG)*SIN(LAT2*CG)
    +COS(LAT1*CG)*COS(LAT2*CG)*COS((LON2-LON1)*CG))/CG$

```

SKP..

```

  ENDS COMMENT GEODIST$

```

COMMENT COMPUTATION OF COORDINATES OF TWO GEOGRAPHICAL POINTS
ON THE GRID PLANES\$

```

PROCEDURE GEOMGRID(PP,GG)$ INTEGER PP,GG$
COMMENT X1,X2=ROW INDICES AND Y1,Y2=COL. INDICES $
BEGIN
  LIS(PP)$ LA1= LALAT$ LO1= LALONG$
  LIS(GG)$ LA2= LALAT$ LO2= LALONG$
  X1=(70-LA1)/2.5$ Y1=(130-LO1)/5$

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X2=(70-LA2)/2.5$ Y2=(130-L02)/5$
END$ COMMENT GEOMGRIDS$

```

```

COMMENT COMPUTATION OF GREAT CIRCLE DISTANCE AND TRUE COURSE
OF A SEGMENT FLOWNS$

```

```

PROCEDURE PART2GEOM$

```

```

BEGIN

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REAL AS

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```

INTEGER NS

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REAL TOTL,LA11,LA22,L011,L022,XX1,XX2,YY1,YY2$

```

```

K1= ENTIER(X1)$ K2= K1+1$ L1= ENTIER(Y1)$

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L2= L1+1$ K1Q= ENTIER(X2)$ K2Q= K1Q+1$

```

```

L1Q= ENTIER(Y2)$ L2Q= L1Q+1$

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```

N1= ABS(K1Q-K1)$

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N2= ABS(L1Q-L1)$

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N3 = IF K1Q EQL K1 AND L1Q EQL L1 THEN 0

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```

ELSE IF N1 LEQ N2 THEN N2 ELSE N1$

```

```

BEGIN

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```

INTEGER I,J$

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```

LOCAL LABEL LAB1$

```

```

AB(0)= 0$ AB(N3+1)= 1$

```

```

IF N3 EQL 0 THEN GOTO LAB1$ IF N3 EQL N1 THEN

```

```

BEGIN

```

```

IF K1 GTR K1Q THEN

```

```

BEGIN

```

```

RES1= K1$

```

```

RES2= K2Q$ RES3= -1

```

```

END

```

```

ELSE

```

```

BEGIN

```

```

RES1= K2$ RES2= K1Q$

```

```

RES3= 1

```

```

END$

```

```

FOR I= RES1 STEP RES3 UNTIL RES2 DO

```

```

BEGIN

```

```

J= RES3*(I-RES1)+1$ AB(J)= (I-X1)/
(X2-X1)

```

```

END

```

```

END

```

```

ELSE

```

```

BEGIN

```

```

IF L1 GTR L1Q THEN

```

```

BEGIN

```

```

RES1= L1$

```

```

RES2= L2Q$ RES3= -1

```

```

END

```

```

ELSE

```

```

BEGIN

```

```

RES1= L2$ RES2= L1Q$

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```

RES3= 1

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```

END$

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```

FOR I= RES1 STEP RES3 UNTIL RES2 DO

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BEGIN

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J= RES3*(I-RES1)+1$ AB(J)= (I-Y1)/
(Y2-Y1)
END
END$
LAB1..
TOTAL=0$
LA11=LA1$ L011=L01$
N=N3+1$
FOR I=1 STEP 1 UNTIL N DO
BEGIN
XX2=AB(I)*X2 + (1-AB(I))*X1$
YY2=AB(I)*Y2 + (1-AB(I))*Y1$
LA22=70-(XX2*2.5)$
L022=130-(YY2*5.0)$
LENGTH(I)=GEODIST(LA11,L011,LA22,L022)$
LA11=LA22$ L011=L022$
TOTAL=LENGTH(I)+TOTAL$
END$
D=TOTL$
TC=ARCCOS((SIN(LA2*CG) - SIN(LA1*CG)*COS(D/60*CG)) /
(SIN(D/60*CG)*COS(LA1*CG)))$
TC=TC/CG$
IF SIN((L02-L01)*CG) GTR 0 THEN TC=360 - TC$
IF TC LEQ 90 THEN
BEGIN A=(90-TC)*CG$
E1=COS(A)$ E2=SIN(A)$ END
ELSE IF TC LEQ 180 THEN
BEGIN A=(TC-90)*CG$
E1=COS(A)$ E2=-SIN(A)$ END
ELSE IF TC LEQ 270 THEN
BEGIN A=(270-TC)*CG$
E1=-COS(A)$ E2=-SIN(A)$ END
ELSE BEGIN A=(TC-270)*CG$
E1=-COS(A)$ E2=SIN(A)$ END$
END
END$ COMMENT PART2GEOM$

REAL PROCEDURE SUM1(A, B, ARR)$
VALUE A, B$
INTEGER A, B$ ARRAY ARR$
BEGIN INTEGER I$ REAL S$
S= 0$
FOR I= A STEP 1 UNTIL B DO
S= S + ARR(I)$
SUM1 = S$
END$ COMMENT SUM1$

REAL PROCEDURE SUM2(A, B, ARR1, ARR2)$
VALUE A, B$
INTEGER A, B$ ARRAY ARR1, ARR2$
BEGIN INTEGER I$ REAL S$
S= 0$
FOR I= A STEP 1 UNTIL B DO
S = S + ARR1(I)*ARR2(I)$

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SUM2 = S$
END$ COMMENT SUM2$
```

COMMENT COMPUTATION OF A DRIFT ANGLE FOR THE SEGMENTS

```
REAL PROCEDURE DRIFT(X,Y)$
VALUE X,Y$
REAL X,Y$
BEGIN
REAL SPD,ANG,DEG,W$
LOCAL LABEL BR$
IF X EQL 0 AND Y EQL 0 THEN
BEGIN SPD=DEG=0$ GOTO BR$ END$
SPD=SQRT(X**2 + Y**2)$
W=ABS(X)$
IF SPD EQL 0 THEN GOTO BR$
ANG=ARCCOS(W/SPD) /CG$
IF X GEQ 0 AND Y LEQ 0 THEN ANG=270+ANG
ELSE IF X GEQ 0 AND Y GEQ 0 THEN
ANG=270-ANG
ELSE IF X LEQ 0 AND Y GEQ 0 THEN ANG=90+ANG
ELSE IF X LEQ 0 AND Y LEQ 0 THEN ANG=90-ANG
ELSE WRITE('WIND DIRECTION ERROR')$
DEG=ANG-TC$
```

BR..

```
DRIFT=ANG=SPD*SIN(DEG*CG) /TAS$
COSA=COS(ARCSIN(ANG))$
END$ COMMENT DRIFT$
```

```
PROCEDURE METPROC(S)$ VALUE S$ INTEGER S$
COMMENT PROCESSING METEOROLOGICAL PARAMETERS$
BEGIN
```

```
INTEGER I,N$
REAL HD,GS,TASS$
ARRAY TEMP,WNDX,WNDY,ENDUR(1..N3+1)$
XX1=X1$ YY1=Y1$
N=N3+1$
FOR I=1 STEP 1 UNTIL N DO
BEGIN
XX2= AB(I)*X2+(1-AB(I))*X1$
YY2= AB(I)*Y2+(1-AB(I))*Y1$
XSTER= (XX1+XX2)/2$
YSTER= (YY1+YY2)/2$
TEMP(I)= -GEOP(XSTER,YSTER,S,3)$
WNDX(I)=GEOP(XSTER,YSTER,S,1)$
WNDY(I)=GEOP(XSTER,YSTER,S,2)$
XX1=XX2$ YY1=YY2$
```

```
END$
WX=SUM1(1,N,WNDX) /N$
WY=SUM1(1,N,WNDY) /N$
TEM=SUM1(1,N,TEMP) /N$
TAS=TASM*SQRT(273.16+TEM)$
ANGLE=DRIFT(WX,WY)$
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FOR I=1 STEP 1 UNTIL N DO
  BEGIN
    TASS=TASM*SQRT(273.16 + TEMP(I))$
    GS=TASS*COSA + (WNDX(I)*E1 + WNDY(I)*E2)$
    ENDUR(I)=36000*LENGTH(I) / GS$
  ENDS$
ENDU=SUM1(1,N,ENDUR)$
RES1= 31+(S-1)*4$
WIX(S)=SUM2(1,N,ENDUR,WNDX)/ENDU$
WIY(S)=SUM2(1,N,ENDUR,WNDY)/ENDU$
TEM=SUM2(1,N,ENDUR,TEMP)/ENDU$
TAS=TASM*SQRT(273.16+TEM)$
TDEV(S)= IF RES1 LEQ 35.332 THEN TEM +1.98*RES1-15 ELSE
55+TEM$
TIME(S)= ENDU$
AIRDIST(S)= ENDU *TAS/36000$ LE= DS
HEADING(S)=TC+ARCSIN(ANGLE)/CG$
HD=HEADING(S)$
IF HD LEQ 90 THEN
  BEGIN HD=(90-HD)*CG$
    TAX(S)=TAS*COS(HD)$ TAY(S)=TAS*SIN(HD)$ END
ELSE IF HD LEQ 180 THEN
  BEGIN HD=(HD-90)*CG$
    TAX(S)=TAS*COS(HD)$ TAY(S)=-TAS*SIN(HD)$ END
ELSE IF HD LEQ 270 THEN
  BEGIN HD=(270-HD)*CG$
    TAX(S)=-TAS*COS(HD)$ TAY(S)=-TAS*SIN(HD)$ END
ELSE BEGIN HD=(HD-270)*CG$
  TAX(S)=-TAS*COS(HD)$
  TAY(S)=TAS*SIN(HD)$ ENDS$
ENDS$ COMMENT METPROC$

COMMENT 'TABLE' AND 'CLIMBCORT' ARE TABLE LOOK-UP PROCEDURES$

INTEGER PROCEDURE TABLE(P,R,MA)$
VALUE P,R$ INTEGER P,R$ INTEGER ARRAY MAS$
BEGIN
  INTEGER G,B,D$ REAL R0,C$
  LOCAL LABEL LAB20$
  B=IF P EQL 0 THEN 4536 ELSE 5$
  C=IF P EQL 0 THEN GRWG ELSE TDEV(R)$
  D=IF P EQL 0 THEN 127006 ELSE -15$
  R0=(C - D)/B$
  G=ENTIER(R0)$
  R0=R0 - G$
  IF MA(R,G+1) EQL -1 THEN
    BEGIN TABLE=-1$ GOTO LAB20$
  ENDS$
  TABLE=R0*MA(R,G+1) + (1-R0)*MA(R,G)$
-AB20..
ENDS$ COMMENT TABLE$

INTEGER PROCEDURE CLIMBCORT(L,MA)$
VALUE L$ INTEGER L$ INTEGER ARRAY MAS$

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```

BEGIN
INTEGER R,C,E1,E2,E3,E4$
REAL G,R0,R1$
LOCAL LABEL LAB21$
G=(GRWQ - 127006)/4536$
R=ENTIER(G)$
R0=G-R$
R=R*3 + L$
G=(TDEV(L) + 25)/5$
C=ENTIER(G)$
R1=G-C$
E1=MA(R,C)$
E2=MA(R+3,C)$
E3=MA(R,C+1)$
E4=MA(R+3,C+1)$
IF E1 EQL -1 OR E2 EQL -1 OR E3 EQL -1 OR E4 EQL -1 THEN
    BEGIN CLIMBCORT=-1$ GOTO LAB21$ ENDS
CLIMBCORT=R0*R1*E4 + (1-R0)*(1-R1)*E1
    + (1-R0)*R1*E3 + R0*(1-R1)*E2$
-AB21..
END$ COMMENT CLIMBCORT$

PROCEDURE READQ(Y0,Y1,Y2,Y3,ARR)$
VALUE Y0,Y1,Y2,Y3$ INTEGER Y0,Y1,Y2,Y3$
INTEGER ARRAY ARR$
BEGIN
    FOR I=Y0 STEP 1 UNTIL Y1 DO
        READ(PCF('DC10F'), FOR J=Y2 STEP 1 UNTIL Y3
            DO ARR(I,J), ERR,ERR)$
    ENDS COMMENT READ$

PROCEDURE WRITEQ(Y0,Y1,Y2,Y3,ARR)$
VALUE Y0,Y1,Y2,Y3$
INTEGER Y0,Y1,Y2,Y3$
INTEGER ARRAY ARR$
BEGIN
    FOR I=Y0 STEP 1 UNTIL Y1 DO
        WRITE(FOT,Y3, FOR J=Y2 STEP 1 UNTIL Y3 DO
            ARR(I,J), ERR)$
    ENDS COMMENT WRITEQ$

READQ(1,3,1,16,RANGE)$
READQ(1,3,17,33,RANGE)$
READQ(1,99,1,9,TEMPTIME)$
READQ(1,99,1,9,TEMPDIST)$
READQ(1,99,1,9,TEMPFUEL)$
READQ(1,3,1,7,Mw)$

WRITE(PEJT)$
WRITE('* PERFORMANCE DATA FOR DC10 *')$ WRITE(' ')$
WRITE(' ')$ WRITE(' ')$
WRITE('* SPECIFIC RANGE *')$ WRITE(' ')$
WRITEQ(1,3,1,16,RANGE)$
WRITEQ(1,3,17,33,RANGE)$

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WRITE(' ')$ WRITE(' ')$ WRITE(' ')$ WRITE(' ')$
WRITE('* MAX. WEIGHT *')$ WRITE(' ')$
WRITEQ(1,3,1,7,MW)$
WRITE(PEJT)$
WRITE('* CLIMB TIME *')$ WRITE(' ')$
WRITEQ(1,99,1,9,TEMPTIME)$
WRITE(PEJT)$
WRITE('* CLIMB DISTANCE *')$ WRITE(' ')$
WRITEQ(1,99,1,9,TEMPDIST)$
WRITE(PEJT)$
WRITE('* CLIMB FUEL *')$ WRITE(' ')$
WRITEQ(1,99,1,9,TEMPFUEL)$

```

RUN..

```

READ(PCF('DC10F'), FLUR, TAXI, GRW, RESERVE, TOW,
MAXTOW,MAXLW,DATE,IO,TTT,ROUTE,DONE, ERR)$
WRITE(' ')$ WRITE(' ')$ WRITE(' ')$
WRITE(' *** INPUT PARAMETERS ***')$
WRITE(F02, 11, FLUR,TAXI,GRW,RESERVE,TOW,
MAXTOW,MAXLW,DATE,IO,TTT,ROUTE)$
IF ROUTE GEQ 1111 THEN
BEGIN
READ(PCF('DC10F'), Q, DONE, ERR)$
WRITE(F02, 1, Q)$
Q=Q-1$
END
ELSE
BEGIN
READ(PCF('DC10F'), ST,ST1, DONE, ERR)$
WRITE(F02, 2, ST, ST1)$
G1Q= ZONEI(ST)$ G2Q= ZONEI(ST1)$ Q= ABS(G2Q-G1Q)
END$
TT = TTT$

BEGIN
INTEGER ARRAY STOREI,STOREIO,STOREG,STOREGQ,E(0..Q),
F(-1..Q)$
FORMAT F04(X63, I6, A2),
F05('TRIP FUEL', I6, A1),
F06('COST', D8.2, A1)$
REAL ARRAY DECLTIME,DECLFUEL,DECLDIST(1..W)$
INTEGER PROCEDURE SQ(H1,H2)$ INTEGER H1,H2$
SQ= A(G1Q+IO*H1-1)+H2$
INTEGER PROCEDURE JQ(H1,H2)$ INTEGER H1,H2$
JQ= F(H1-1)+H2-STOREI(H1)+1$

PROCEDURE DESCLIMB(S)$ VALUE S$ INTEGER S$
COMMENT COMPUTATION OF PERFORMANCE IN CLIMB OR DESCENTS
BEGIN
INTEGER ALTS
LOCAL LABEL JUMS
REAL TASQRTS
TASQRT=SQRT(TAX(S)**2 + TAY(S)**2)$

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```

ALT= 31+(S-1)*4$
DECLTIME(S)=IF MQ EQL 0 THEN 60*CLIMBCORT(S,TEMPTIME)
/1000 ELSE 3.1+0.41*ALT$
DECLDIST(S)=IF MQ EQL 0 THEN CLIMBCORT(S,TEMPDIST)
ELSE 9+3*ALT$
DECLFUEL(S)=IF MQ EQL 0 THEN CLIMBCORT(S,TEMPFUEL)
ELSE 940+8.5*ALT$ IF DECLTIME(S) LSS 0 THEN GOTO JUM$

```

```

AID4=DECLDIST(S)*60/(DECLTIME(S)*TASQRT)$
DECLDIST(S)= SQRT((0.75*WIX(S)+TAX(S)*AID4)**2+
(0.75*WIY(S)+TAY(S)*AID4)**2)*(DECLTIME(S)-2)/60$
IF DECLDIST(S) GTR LE THEN DECLDIST(S)=LE$
AIRDIST(S)= (1-DECLDIST(S)/LE)*AIRDIST(S)$
TIME(S)=AIRDIST(S)/TASQRT*36000$
LE=LE-DECLDIST(S)$

```

JUM..

END\$ COMMENT DECLIMBS

```

PROCEDURE LINE(N1,N2)$ BOOLEAN N1,N2$
COMMENT PRINT-OUT PROCEDURE$
BEGIN

```

```

    INTEGER I,J,K,L,M,N,P,Q,R,S,T    $
    FORMAT P1('TOC', 2I5, X12, I4, X10, I4, 3I6, I8, A2),
           P2(I3, X22, I4, X10, I4, 3I6, I8, A2),
           P3('TOD', 4I5, I6, I8, I6, 3I6, I8, A2),
           P4(I3, 4I5, I6, I8, 4I6, I8, A2)$

```

LOCAL LABEL LAB30,LAB31,LAB32\$

IF N1 THEN GOTO LAB30\$

IF N2 THEN GOTO LAB31\$

I=G3\$ S=M0\$ T=B3\$

GEOMGRID(G4, G3)\$

J=HEADING(G)\$

K= 310 + (G-1)*40\$

IF NOT N1 AND NOT N2 THEN BEGIN

L= TDEV(G)\$

M= SQRT(TAX(G)**2 + TAY(G)**2)\$

END\$

LAB30..

LAB31..

N= (IF N1 OR N2 THEN .75 ELSE 1)*
(WIX(G)*E1 + WIY(G)*E2)\$

M3= IF N1 OR N2 THEN

DECLTIME(G)*600 ELSE TIME(G)\$

P= 100*ENTIER(M3/36000) + MOD(M3, 36000)/600\$

G= 100*ENTIER(FLTIME/36000) + MOD(FLTIME, 36000)/600\$

R= BURN - GRWQ\$

IF N1 THEN

BEGIN

WRITE(P1,J,K,N,DISTANCE,P,Q,R,GRWQ)\$

GOTO LAB32

END\$

IF N2 THEN

BEGIN

WRITE(P2,ST1,N,DISTANCE,P,Q,R,GRWQ)\$

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C-2

```

      GOTO LAB32
END$
      IF S EQL T THEN
        WRITE(P3,J,K,L,M,N,LE,DISTANCE,P,Q,R,GRWQ)
      ELSE
        TE(P4,I,J,K,L,M,N,LE,DISTANCE,P,Q,R,GRWQ)$

```

LAB32..

END\$ COMMENT LINES

```

PROCEDURE SPACEOPT(FBQ,FB,BI,BG,RR)$ INTEGER FB,RR$
BOOLEAN FBQ,BI,BG$
COMMENT FBQ DETERMINES WETHER THE FLIGHTPLAN
COMPUTATION WILL BE PERFORMED BACKWARDS(FALSE) OR FOR
WARDS(TRUE).
FB DETERMINES WETHER COSTS(+1) OR FUEL(0) OR FLIGHT
TIME(-1) WILL BE OPTIMIZED. RR IS TAKE OFF WEIGHT OR
LANDINGWEIGHT.
BI DEFINES WETHER THE NAVIGATION REGIME IS FREE IN THE
HORIZONTAL(FALSE) OR BOUNDED BY ONE POINT(TRUE).
BG DEFINES WETHER THE CRUISING ALTITUDE IS FREE(FALSE)
OR BOUNDED(TRUE)$
BEGIN

```

```

  LOCAL LABEL ITER, ENDG, CI, REPEAT, EIND$
  INTEGER AA,QUANT,II,JJ,GG,GRWP, DDG, DTG, TMG$
  BOOLEAN ITERATION, BCLIMB,BNQ,BN$
  INTEGER ARRAY ROW,ROWQ,QUANTQ(0..F(Q))$

```

```

PROCEDURE PREP(A1,B1,AA,BB)$ INTEGER A1,B1$
COMMENT COMPUTATION OF DISTANCE AND FLIGHT TIME, AND
PRINT-OUT OF THE FLIGHT PLAN$
BOOLEAN AA,BB$
COMMENT AA REFERS TO CLIMB, BB TO DESCENT$
BEGIN
  DISTANCE= DISTANCE+A1$ FLTIME= FLTIME+B1$
  LINE(AA,BB)$ BURN= GRWQ
END$ COMMENT PREP$

```

```

PROCEDURE EDITING$
BEGIN LOCAL LABEL ENDED$
  FORMAT F03(X44, 'CH', I4, I6, D6.2, A2)$

```

```

PROCEDURE QP$
BEGIN
  IF FB EQL 1 THEN
    WRITE('COST')
  ELSE IF FB EQL 0 THEN
    WRITE('FUEL')
  ELSE IF FB EQL -1 THEN
    WRITE('FLTIME')$
  GOTO ENDED$
END$ COMMENT QP$

```

WRITE(PEJT)\$

WRITE('

*** DETAILED FLIGHT PLAN ***'\$

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WRITE(' ')$ WRITE(' ')$
IF ROUTE EQL 1111 THEN
BEGIN
  WRITE('NON SPECIAL MIN TRACK')$
  QP
END$
IF ROUTE EQL 4444 THEN
BEGIN
  WRITE('ATC I')$ QP$
END$
IF ROUTE EQL 5555 THEN
BEGIN
  WRITE('ATC II')$ QP$
END$
IF ROUTE EQL 7777 THEN
BEGIN
  WRITE('GRC')$ QP$
END$
IF ROUTE EQL 9999 THEN
BEGIN
  WRITE('SPECIAL TRACK')$ QP$
END$
WRITE('MIN TRACK IN SPACE')$ QP$
WRITE(F03, FLUR, DATE, TT)$
WRITE(' ')$

```

ENDED..

WRITE(
'NO. HEAD
)\$

FL TMP TAS WIND DIST ACCD TIME ACCT BURN WEIGHT

END\$ COMMENT EDITINGS

PROCEDURE QQ(0)\$ INTEGER 0\$
COMMENT COMPUTATION OF SEGMENT CONTRIBUTION. COST,
TIME, FUEL, WEIGHT ETC.\$

BEGIN
LOCAL LABEL JM1, JM2, JM3, JM, ENDQ\$

PROCEDURE CL(M1, M2)\$ REAL M1, M2\$
COMMENT M1 DENOTES SEGMENT FUEL, M2 SEGMENT TIMES
BEGIN

LOCAL LABEL JUS REAL MMS
IF BCLIMB THEN
BEGIN

MM= 0\$ GOTO JU

END\$
IF ITERATION THEN
BEGIN

MM= IF G GEQ GG THEN -28
ELSE -700\$ GOTO JU

END\$
MM= IF (0 EQL -1 AND G GEQ GG) OR (0 EQL 1 AND
G LSS GG) THEN 700 ELSE 28\$

JU..

MM= M1+ 0*(GG-G)* (IF MQ NEQ B1 THEN MM ELSE 0)\$

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GRWQ= GRWQ + 0*MM\$
 QUANT= QUANT+(IF FB EQL 1 THEN 1083.3*M2+15*MM
 ELSE IF FB EQL 0 THEN MM ELSE 600*M2)\$
 ENDS COMMENT CL\$

QUANT = QUANTQ(I)\$
 ITERATION= IF NOT FBQ AND MQ EQL 0 AND 0 EQL -1
 THEN TRUE
 ELSE FALSE\$ IF ROW(I) EQL 0 THEN GOTO JMS
 GRWQ= IF ITERATION THEN ROW(0) ELSE ROW(I)\$
 IF MQ EQL B1 OR ITERATION THEN
 BEGIN
 IF DECLFUEL(G) LSS 0 THEN GOTO JMS
 BCLIMB= TRUES CL(DECLFUEL(G), DECLTIME(G))\$
 BCLIMB= FALSE\$
 DDG= DECLDIST(G)\$ DTG= DECLTIME(G)*600 \$
 IF ED THEN PREP(DDG, DTG, TRUE, FALSE)\$
 ENDS
 IF NOT FBQ THEN GOTO JM2\$

JM1..

AID4= IF TDEV(G) LSS -10 THEN 64.08+6
 ELSE TABLE(1,G,MW)\$
 IF GRWQ GEQ AID4 THEN GOTO JMS
 IF NOT FBQ THEN GOTO JM3\$

JM2..

GRWP= GRWQ\$ GRWQ= GRWQ + 0* AIRDIST(G)/ 2*
 (IF G EQL 1 THEN 2.366+0.0000722* GRWQ ELSE
 IF G EQL 2 THEN 0.35 + 0.0000792* GRWQ
 ELSE -0.83+ 0.000089* GRWQ)\$
 AA= TABLE(0,G,RANGE)\$ GRWP= GRWP\$
 IF AA LSS 0 THEN GOTO JMS
 CL(AIRDIST(G)*10**4/AA*TIME(G)/600)\$
 TMG= TIME(G)\$
 IF ED THEN PREP(LE, TMG, FALSE, FALSE)\$
 IF NOT FBQ THEN GOTO JM1\$

JM3..

IF MQ EQL B3 AND NOT ITERATION THEN
 BEGIN
 BCLIMB=
 TRUES CL(DECLFUEL(G),DECLTIME (G))\$
 BCLIMB= FALSE\$
 DDG= DECLDIST(G)\$ DTG= DECLTIME(G)*600 \$
 IF ED THEN PREP(DDG, DTG, FALSE, TRUE)\$
 ENDS
 GOTO ENDQ\$

JM..

ENDQ..

GRWQ= 0\$ QUANT= 64.08+6\$

ENDS
 COMMENT QG\$

ED= IF B1 AND B8 THEN TRUE ELSE FALSE\$
 FOR AA= 0 STEP 1 UNTIL F(Q) DO

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BEGIN	****1080
ROW(AA)= ROWQ(AA)= 0\$ QUANTQ(AA)= 64.08+6	****1081
END\$	****1082
QUANT= 0\$ BCLIMB= FALSE\$	****1083
IF FBQ THEN	****1084
BEGIN	****1085
ROW(0)= RRS QUANTQ(0)= 0	****1086
END	****1087
ELSE	****1088
BEGIN	****1089
ROW(F(Q))= RRS QUANTQ(F(Q))= 0	****1090
END\$	****1091
IF ED THEN	****1092
BEGIN	****1093
DISTANCE= FLTIME= 0\$ BURN= ROW(0)\$	****1094
EDITINGS WRITE(F04, RR)\$	****1095
END\$	****1096
IF FBQ THEN	****1097
BEGIN	****1098
B1= 0\$ B2= 1\$ B3= Q-1	****1099
END	****1100
ELSE	****1101
BEGIN	****1102
B1= Q-1\$ B2= -1\$ B3= 0	****1103
END\$	****1104
COMMENT ZONE CYCLE BEGINS\$	****1105
FOR MQ= B1 STEP B2 UNTIL B3 DO	****1106
BEGIN	****1107
G1= IF FBQ THEN MQ+1 ELSE MQ\$	****1108
G2= IF FBQ THEN MQ ELSE MQ+1\$	****1109
M= IO*MQ+G1Q+(IF IO EQL -1 THEN -1 ELSE 0)\$	****1110
	****1111
COMMENT A CYCLE FOR GRAPH POINTS ALONG MERIDIAN	****1112
BEGINS\$	****1113
FOR JJ= STOREI(G1) STEP 1 UNTIL STOREIQ(G1) DO	****1114
BEGIN	****1115
G3= SQ(G1,JJ)\$ J= JQ(G1,JJ)\$	****1116
COMMENT A CYCLE FOR GRAPH POINTS	****1117
ALONG NEXT MERIDIAN BEGINS\$	****1118
FOR II= STOREI(G2) STEP 1 UNTIL STOREIQ(G2) DO	****1119
BEGIN	****1120
IF NOT B1 THEN	****1121
BEGIN	****1122
IF(M GEQ 3 AND M LEQ 8) AND ABS	****1123
(II-JJ) GEQ 10 THEN GOTO C1\$	****1124
BNQ= (FBQ AND IO EQL -1) OR (NOT FBQ AND	****1125
IO EQL 1)\$	****1126
BN= (FBQ AND IO EQL 1) OR (NOT FBQ AND	****1127
IO EQL -1)\$	****1128
IF M LSS 3 THEN	****1129
BEGIN	****1130
IF(BNQ AND BK	****1131
(M,JJ,II)) OR (BN AND BK(M,II,	****1132
	****1133

```

      JJ)) THEN GOTO CI
    ENDS
    IF M GTR 8 THEN
    BEGIN
      IF (BNQ AND
        BKQ(M,JJ,II)) OR (BN AND BKQ
          (M,II,JJ)) THEN GOTO CI
    END
    ENDS
    G4= SQ(G2,II)$ I= JQ(G2,II)$
    IF FBQ THEN GEOMGRID(G4,G3)ELSE
    GEOMGRID(G3,G4)$
    PART2GEOMS
    IF MQ NEQ B1 THEN GG=STOREG(MQ - B2)$

    COMMENT A CYCLE FOR FLIGHT LEVELS BEGINS$
    FOR G= STOREG(MQ) STEP 1 UNTIL
    STOREGQ(MQ) DO
    BEGIN
      IF NOT FBQ AND MQ EQL 0 THEN
      BEGIN
        TEL = 0$ IF G NEQ GG THEN
        GOTO ENDG$
        N1= ROW(0)$ ROW(0)= GRWQ=
        MAXTOW-20000$

        TEL = TEL +1$ IF G LSS 1
        THEN
        BEGIN
          G= GG$ GRWQ= 0$
          GOTO ENDG
        ENDS
        METPROC(G)$ DESCLIMB(G)$
        IF DECLFUEL(G) LSS 0 THEN
        BEGIN
          TEL= 0$ G= G-1$ GOTO REPEAT
        ENDS
        QQ(-1)$ IF GRWQ EQL 0 THEN GOTO ENDG$
        N2= ROW(I) - GRWQ$ IF N2 GTR 10
        AND ROW(0) EQL MAXTOW THEN GOTO
        ENDG$
        ROW(0)= ROW(0) + (IF TEL GTR 10
        THEN N2/2 ELSE N2)$
        GRWQ= ROW(0)$ IF ABS(N2) LSS 10
        OR TEL GTR 10 THEN
        BEGIN
          ROW(0)= N1$ GOTO ITER
        END
        ELSE GOTO REPEAT$
      END
    ELSE
    BEGIN
      METPROC(G)$

```

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```

REPEAT..

ITER..

IF MQ EQL 0 OR MQ EQL Q-1 THEN	****1188
BEGIN	****1189
GRWQ= RRS DESCLIMB(G)	****1190
ENDS	****1191
IF FBQ THEN QQ(-1) ELSE QQ(1)\$	****1192
IF GRWQ EQL 0 THEN GOTO ENDG	****1193
ENDS	****1194
IF QUANT LEQ QUANTQ(J) THEN	****1195
BEGIN	****1196
ROW(J)= GRWQS QUANTQ(J)= QUANTS	****1197
ROWQ(J)= 1\$ IF BI AND NOT BG	****1198
THEN STOREG(MQ)= G\$	****1199
IF ITERATION THEN G= GG	****1200
ENDS	****1201
ENDG..	****1202
ENDS COMMENT FLIGHT-LEVEL CYCLES	****1203
I..	****1204
ENDS COMMENT ALONG-NEXT-MERIDIAN CYCLES	****1205
ENDS COMMENT ALONG-CURRENT-MERIDIAN CYCLES	****1206
IF BI AND NOT BG THEN	****1207
STOREGQ(MQ) = STOREG(MQ)	****1208
ENDS COMMENT ZONE CYCLES	****1209
IF ROW(0) EQL 0 THEN GOTO EINDS	****1210
IF BI THEN GOTO EINDS J=IF FBQ THEN F(Q) ELSE F(0)\$	****1211
FOR MQ= B3 STEP -B2 UNTIL B1 DO	****1212
BEGIN	****1213
K= IF FBQ THEN MQ ELSE MQ+1\$ I= ROWQ(J)\$	****1214
STOREIQ(MQ +(IF B3 EQL 0 THEN 1 ELSE 0))= I-F(K-1)+	****1215
STOREI(K)-1\$ J= 1\$	****1216
ENDS	****1217
FOR MQ= 0 STEP 1 UNTIL Q DO STOREI(MQ)= STOREIQ(MQ)\$	****1218
EIND..	****1219
TOWQ= ROW(0)\$ M1= IF FBQ THEN QUANTQ(F(Q)) ELSE	****1220
QUANTQ(0)\$	****1221
LW= ROW(F(Q))\$ IF ED THEN	****1222
BEGIN	****1223
WRITE(' ')\$	****1224
WRITE(F05, TOWQ-LW)\$	****1225
WRITE(F06, IF FB EQL 1 THEN M1/100 ELSE	****1226
((TOWQ-LW)*15+1083.3*FLTIME/600)/100)\$	****1227
ENDS	****1228
ENDS COMMENT SPACEOPTS	****1229
PROCEDURE FF(UU,VV)\$ INTEGER ARRAY UU,VV\$	****1230
BEGIN	****1231
F(-1)= -1\$ FOR K= 0 STEP 1 UNTIL Q DO	****1232
F(K)= F(K-1)+VV(K)-UU(K)+1	****1233
ENDS COMMENT FF\$	****1234
PROCEDURE PROCES(S1,S2,S3,PR,FFBB,BB,FACTORISATION)\$	****1235
	****1236
	****1237
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```

INTEGER S1,S2,S3,FFBB$ REAL PR$
BOOLEAN BB,FACTORISATIONS
COMMENT S1 AND S2 DETERMINE THE LIMITS OF FLIGHT
LEVELS.
S3 IS A DUMMY,EXCEPT WHEN
FACTORISATION IS TRUE,
THEN S3 IS A DATUM FOR THE FLIGHT
LEVEL
IN WHICH THE M,F,P, IS COMPUTED,
PR IS PERCENTAGE TRIP FUEL
FFBB DETERMINES WETHER COSTS(+1),
FUEL(0) OR TIME(-1) IS OPTIMIZED,
BB,USE LANDING WEIGHT(TRUE),USE
TAKE OFF WEIGHT(FALSE)
FACTORISATION(TRUE) INITIALISES
PROCES IN THE HORIZONTAL ON THE
BASIS OF FLIGHT TIME,
FOLLOWED BY COMPILATION OF FLIGHT
PLAN IN THE VERTICAL ON THE BASIS
OF COSTS,FUEL OR TIMES
BEGIN
    INTEGER NN$
    LOCAL LABEL ENDPR,INGS

    PROCEDURE AA$
    COMMENT SPECIFICATION OF LIMITS IN HORIZONTAL OF
        GRAPH POINTS ALONG MERIDIANS$
    BEGIN
        LOCAL LABEL UTRECHTS$
        STOREI(0)=STOREIQ(0)=ST - A(G1Q-1)$
        STOREI(Q)= STOREIQ(Q)= ST1-A(G2Q-1)$
        IF ROUTE GEQ 1111 THEN GOTO UTRECHTS$
        FOR K= 1 STEP 1 UNTIL Q-1 DO
            BEGIN
                STOREI(K)= 1$ STOREIQ(K)= E(K)
            ENDS$
        END$
        FF(STOREI,STOREIQ)
    ENDS$ COMMENT AA$

    PROCEDURE AAA(F1,F2)$ INTEGER F1,F2$
    COMMENT SPECIFICATION OF LIMITS IN THE VERTICAL$
    FOR K= 0 STEP 1 UNTIL Q-1 DO
        BEGIN
            STOREG(K) = F1$ STOREGQ(K) = F2$
        ENDS$ COMMENT AAA$

    PROCEDURE EP$
    IF TOWQ GEQ MAXTOW OR TOWQ EQL 0 THEN
        BEGIN
            WRITE('SUPER CRITICAL')$
            GOTO ENDPR$
        ENDS$ COMMENT EP$

```

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```

INTEGER PROCEDURE SS$
SS= GRW+RESERVE+PR*((GRW+RESERVE)*
(MINTIME*0.08-0.15)-500*MINTIME+7300+TAXI)$

```

```

INTEGER PROCEDURE SSS$
SSS= GRW+RESERVE+PR*(TOWQ-LW+TAXI)$

```

```

INTEGER PROCEDURE SSSS$
SSSS= TOWQ*(GRW+RESERVE+PR*TAXI)/((1+PR)*NN-PR*TOWQ)$

```

```

PROCEDURE NNQ(A)$ VALUE AS INTEGER AS
NN= IF NOT BB THEN TOW ELSE AS

```

```

PROCEDURE TWS
COMMENT SAFEGUARDING AGAINST OVERLOADINGS
IF TOWQ GEQ MAXTOW OR TOWQ EQL 0 THEN
BEGIN
WRITE(PEJT)$ WRITE('DECR LANDING W')$
GOTO ENDP
END$

```

```

COMMENT IF FACTORIZATION IS TRUE, THEN THE OPTIMIZATION
TAKES PLACE FIRST IN THE HORIZONTAL AND THEN
IS FOLLOWED BY IN THE VERTICALS

```

```

IF FACTORISATION THEN

```

```

BEGIN

```

```

AAS AAA(S3,S3)$ NNQ(SS)$ ROUTE= 1111$
SPACEOPT(IF BB THEN FALSE ELSE TRUE,-1,FALSE,
TRUE,NN)$ TWS
AAA(S1,S2)$ GOTO ING

```

```

END

```

```

ELSE

```

```

BEGIN

```

```

AAS AAA(S1,S2)$ NNQ(SS)$
SPACEOPT(IF BB THEN FALSE ELSE TRUE,FFBB,FALSE,
FALSE,NN)$ TWS

```

```

ING..

```

```

EPS NNQ(SSS)$
SPACEOPT (IF BB THEN FALSE ELSE TRUE,FFBB, TRUE,
FALSE,NN)$ TWS
EPS NNQ(SSSS)$
SPACEOPT(TRUE,FFBB,TRUE,TRUE,NN)$ EPS
IF FACTORISATION THEN ROUTE= 1000

```

```

END$

```

```

ENDPR..

```

```

END$ COMMENT PROCESS

```

```

IF ROUTE GEQ 1111 THEN

```

```

BEGIN

```

```

READ(PCF('DC10F'), ST, ST1, DONE, ERR)$
G1Q= ZONEI(ST)$
FOR K= 1 STEP 1 UNTIL Q-1 DO
BEGIN READ(PCF('DC10F'), STOREI(K), DONE, ERR)$

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WRITE(F02, 1, STOREI(K))$
STOREI(K)= STOREIQ(K)= STOREI(K)-A(G1Q+IO*K-1)$
END$
G2Q = ZONEI(ST1)$
WRITE(F02, 2, ST,ST1)$
END$
GEOMGRID(ST,ST1)$
MINTIME=GEODIST(LA1,L01,LA2,L02)/465$
CTQ$
E(0)= E(Q)= 1$ FOR K= 1 STEP 1 UNTIL Q-1 DO
E(K)= A(G1Q+IO*K)-A(G1Q+IO*K-1)$

COMMENT
1. WHEN A FLIGHT PLAN FOR THE OPTIMAL COST TRACK IS NEEDED
CALL 'PROCES(1, 3, 1, 0.03, 1, TRUE, FALSE)'
2. WHEN A FLIGHT PLAN FOR THE OPTIMAL FUEL TRACK NEEDED
CALL 'PROCES(1, 3, 1, 0.03, 0, TRUE, FALSE)'
3. WHEN A FLIGHT PLAN FOR THE LEAST TIME TRACK NEEDED
CALL 'PROCES(1, 3, 1, 0.03, -1, TRUE, FALSE)'$

PROCES(1, 3, 1, 0.03, 0, TRUE, FALSE)$
PROCES(1, 3, 1, 0.03, -1, TRUE, FALSE)$

GOTO RUN
END$
DONE.. END$
WRITE(' '$ WRITE(' '$
WRITE(' *** END OF RUN ***')$
GO TO EOP$

ERR.. WRITE(' *** INPUT DATA ERROR ***')$

EOP..
A ELT DC8,1,810528,065734
COMMENT KNMI/KLM 020169 SPG NAV 20 JNG,
NAVIGATION-FLIGHTPLANNING-MODULE FOR THE PRODUCTION OF
FLIGHTPLANS OVER THE NORTH ATLANTIC.
THE MAIN FEATURES
ARE:
1. INCLUSION OF 6 METEOROLOGICAL PARAMETER FIELDS,
TEMPERATURE AND GEOPOTENTIAL FIELDS FOR 300 250 AND 200 MB
VALID FOR TWO STANDARD TIMES 12 HOURS APART.
2. NAVIGATIONAL GRID BASED ON REPORTING POINTS OF THE KLM.
3. INCLUSION OF A DYNAMIC PROCESS BASED ON INTERPOLATION OF
TWO PARAMETER FIELDS.
4. OPTIMALISATION OF FUEL, COSTS OR FLIGHT TIME IN SPACE AS
WELL AS IN THE HORIZONTAL AS IN THE VERTICAL.
5. IN - AND OUTBOUND TRAFFIC (IO= 1 OUTBOUND IO= -1 INBOUND).
6. FLIGHTPLAN PRODUCTION FOR OPTIMUM TRACKS, SPECIFIC ROUTES
ETC. E.G. ALTERNATIVE ATC MINIMUM ROUTES.
7. BLOCKING E.G. SECTOR BLOCKING OVER THE NORTH ATLANTIC
BLOCKING IN AIRWAYS AND ATC RESTRICTED AREAS.
8. STANDARD CRUISE AND USE OF PERFORMANCE TABLES$

CONSTANT KQ= 14 , W= 3$

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Δ[*>WK#AΔ(Δ)Δ ΔX

Program Listing (DC8).

```

INTEGER    P1,P2,P3,Q1,Q2,Q3,S,TTT,
G1,G2,G3,G4,B1,B2,B3,MQ,G1Q,G2Q,Q,
RES1,RES2,RES3,I,J,N1,N2,N3,M,G,
M0,M1,M2,M3,M4,M5,M6,K,I0,
K1,K2,L1,L2,K1Q,K2Q,L1Q,L2Q,KK1,KK2,LL1,LL2,
ENDU,TEM,TAS,FLUR,TAXI,TOW,GRW,RESERVE,MAXTOW,MAXLW,
DATE,ST,ST1,ROUTE,DISTANCE,FLTIME,BURN,
GRWQ,TOWQ,LW,COST,LE,TELS
REAL      CO,CG,P,C1,X1,X2,Y1,Y2,X,Y,E1,E2,E3,
GG1,GG2,D,ANGLE,LALAT,LALONG,TT,LA1,LO1,LA2,LO2,
XX1,XX2,YY1,YY2,AID1,AID2,AID3,AID4,XSTER,YSTER,
MINTIMES
INTEGER ARRAY HT(1..72,4..19), A(-1..KQ+1), V(0..41),
SR(1..3,0..19), MW(1..3,0..6), CD,CT,CF(1..3,0..17), CTC,
CFC(0..7,0..8), CDC(0..6,0..8)$
ARRAY DD(0..KQ)$
BOOLEAN EDS
BOOLEAN ARRAY BK(0..2,1..6,1..6), BKQ(9..KQ,1..6,1..6)$
FORMAT F01(E2, ' ', A1),
      PEJT (E2, ' ', A1),
      F0T(X5, *I6, A2),
      F0Z(X5, *I7, A2)$
STRING STR(10)$

INTEGER PROCEDURE INTERPOL(F,F1,F2,F1Q,F2Q)$
INTEGER F,F1,F2,F1Q,F2Q$
COMMENT LINEAR INTERPOLATIONS
INTERPOL = ((F- F1) * F2Q + (F2 - F) * F1Q) / (F2 - F1)$

REAL PROCEDURE SUM1(A, B, ARR)$
VALUE A, B$
INTEGER A, B$ ARRAY ARR$
BEGIN INTEGER IS REAL SS
  S= 0$
  FOR I= A STEP 1 UNTIL B DO
    S= S + ARR(I)$
  SUM1 = S$
END$ COMMENT SUM1$

REAL PROCEDURE SUM2(A, B, ARR1, ARR2)$
VALUE A, B$
INTEGER A, B$ ARRAY ARR1, ARR2$
BEGIN INTEGER IS REAL SS
  S= 0$
  FOR I= A STEP 1 UNTIL B DO
    S = S + ARR1(I)*ARR2(I)$
  SUM2 = S$
END$ COMMENT SUM2$

PROCEDURE WW(AA, BB) $ REAL AA$ STRING BB$
WRITE(F01, BB, AA)$

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```

P1 = 31000$ P2 = 35000$ P3 = 39000$ Q1 = 30065$
Q2 = 33999$ Q3 = 38662$ TEL = 0$
FOR S= 0 STEP 1 UNTIL 5 DO
BEGIN

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```

    RES1= S*12$
    FOR J=19 STEP -1 UNTIL 4 DO
    FOR I= RES1 + 1 STEP 1 UNTIL
    RES1 + 12 DO READ(PCF('NASAD'), HT(I,J), ERR, ERR)$

```

```

END$

```

```

FOR S=0 STEP 1 UNTIL 5 DO

```

```

    BEGIN RES1 =S*12$ WRITE(PEJT)$

```

```

        FOR J=19 STEP -1 UNTIL 4 DO

```

```

            WRITE(F02, 12, FOR I=RES1 + 1

```

```

                STEP 1 UNTIL RES1 + 12 DO HT(I,J))$

```

```

        END$

```

```

COMMENT ARRAY 'HT' IS REFILLED WITH INTERPOLATED PARAMETERS
        WHICH APPLY IN GRID POINTS AT FLIGHT LEVELS 31000,
        35000, AND 39000 FT$

```

```

FOR I= 1 STEP 1 UNTIL 12, 37 STEP 1 UNTIL 48 DO

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```

    FOR J= 4 STEP 1 UNTIL 19 DO

```

```

    BEGIN

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```

        M0= HT(I,J)$

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```

        M1= ENTIER(M0/100)$ M2= M0-100*M1$

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```

        M0= HT(I+12,J)$

```

```

        M3= ENTIER(M0/100)$ M4= M0-100*M3$

```

```

        M0= HT(I+24,J)$

```

```

        M5= ENTIER(M0/100)$ M6= M0-100*M5$

```

```

        HT(I,J) = 100*INTERPOL(P1,Q1,Q2,M1,M3)+

```

```

        INTERPOL(P1,Q1,Q2,M2,M4)$

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```

        HT(I+12,J)= 100*INTERPOL(P2,Q2,Q3,M3,M5)+

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```

        INTERPOL(P2,Q2,Q3,M4,M6)$

```

```

        HT(I+24,J)= 100*INTERPOL(P3,Q2,Q3,M3,M5)+

```

```

        INTERPOL(P3,Q2,Q3,M4,M6)

```

```

    END$

```

```

COMMENT THIS ROUTINE CONCLUDES THE PRODUCTION OF THE
        METEOROLOGICAL PARAMETERS GEOPOTENTIAL AND TEMPERATURE IN THE
        FLIGHT LEVELS$

```

```

COMMENT RELATIONSHIP BETWEEN GRAPH POINT NUMBERS AND ZONE INDICES$

```

```

A(-1)= -1$ A(0)= 0$ A(1)= 2$ A(2)= 6$ A(3)= 11$ A(4)= 26$

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A(5)= 41$ A(6)= 56$ A(7)= 71$ A(8)= 86$ A(9)= 90$ A(10)= 96$

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```

A(11)= 102$ A(12)= 107$ A(13)= 111$ A(14)= 114$ A(15)= 115$

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V(0)= 52290477$

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V(1)= 51850115$ V(2) = 53640150$

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```

V(3)= 51000200$ V(4) = 51990539$ V(5) = 53580300$

```

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V(6)= 55000200$ V(7) = 49980632$ V(8) = 51840849$

```

```

V(9)= 52700892$ V(10)= 53500630$ V(11)= 55490459$

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```

V(12)= 54271005$ V(13)= 48905454$ V(14)= 51375560$

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V(15)= 53735697$ V(16)= 58476263$ V(17)= 47005800$

```

```

V(18)= 48545856$ V(19)= 55500000$ V(20)= 57006000$

```

```

V(21)= 53286035$ V(22)= 54836683$ V(23)= 46156006$

```

```

V(24)= 48006000$ V(25)= 49846439$ V(26)= 50506500$

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V(27)= 51006750$ V(28)= 52006900$ V(29)= 45006300$

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V(30)= 46176459$ V(31)= 47506600$ V(32)= 48576826$
V(33)= 50007050$ V(34)= 43836608$ V(35)= 44846867$
V(36)= 45327179$ V(37)= 45467385$ V(38)= 41287003$
V(39)= 42367099$ V(40)= 43007250$ V(41)= 40647378$

```

```

COMMENT DETERMINATION OF CONNECTIVITY AMONG GRAPH POINTS.
      FALSE=CONNECTED, TRUE=BLOCKED $

```

```

FOR I= 1 STEP 1 UNTIL 6 DO

```

```

FOR J= 1 STEP 1 UNTIL 6 DO

```

```

BEGIN

```

```

      FOR MQ= 0,1,2 DO BK(MQ,I,J) = TRUES

```

```

      FOR MQ= 9 STEP 1 UNTIL KQ DO BKQ(MQ,I,J) = TRUE

```

```

END$

```

```

BK(1,1,1)= BK(2,1,1)= BK(1,2,2)= BK(2,2,2)=

```

```

BKQ(9,1,1)= BKQ(10,1,1)= BKQ(11,1,1)= BKQ(12,1,1)=

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```

BKQ(13,1,1)= BKQ(14,1,1)= BKQ(9,2,2)= BKQ(10,2,2)=

```

```

BKQ(11,2,2)= BKQ(12,2,2)= BKQ(13,2,2)= BKQ(10,3,3)=

```

```

BKQ(11,3,3)= BKQ(13,3,3)= BKQ(11,4,4)= BK(2,3,4)= BK(2,4,5)=

```

```

BKQ(12,4,4) = BKQ(10,6,6) = BK(1,1,2) =

```

```

BK(1,2,3) = BK(1,2,4) = BK(2,2,3) =

```

```

BKQ(9,1,2)= BKQ(9,2,3)= FALSE$

```

```

BKQ(9,2,5)= BKQ(9,3,4)= BKQ(9,3,5)= BKQ(9,4,6)= BKQ(10,2,1)=

```

```

BKQ(10,4,3)= BKQ(10,5,3)= BKQ(10,5,4)= BKQ(10,6,5)=

```

```

BKQ(11,1,2)= BKQ(11,3,4)= BKQ(11,5,4)= FALSE$

```

```

BKQ(11,6,5)= BKQ(12,2,1)= BKQ(12,3,2)= BKQ(12,4,3)=

```

```

BKQ(12,5,4)= BKQ(13,1,2)= BKQ(14,2,1)= BKQ(14,3,1)= BK(0,1,1)=

```

```

BK(0,1,2) =FALSE$

```

```

BEGIN

```

```

      REAL ARRAY AB(0..10), LENGTH(1..10),

```

```

      TIME,AIRDIST,TDEV,WIX,WIY,TAX,TAY(1..W)$

```

```

      INTEGER PROCEDURE ZONEI(Q)$ INTEGER Q$

```

```

      COMMENT THIS SUBROUTINE DETERMINES THE INDEX OF THE
      ZONE ASSOCIATED WITH A STATION$NUMBERS

```

```

      BEGIN

```

```

        LOCAL LABEL AGAIN$ INTEGER IS

```

```

        I= -1$

```

```

      AGAIN..

```

```

        I= I+1$ IF A(I)=Q LSS 0 THEN GOTO AGAIN$

```

```

        ZONEI= I

```

```

      END$ COMMENT ZONEI$

```

```

      PROCEDURE DT(K)$ INTEGER K$

```

```

      COMMENT THIS SUBROUTINE DISSECTS LATITUDE AND
      LONGITUDE FROM THE COMPRESSED COORDINATES.

```

```

      EAST OF GREENWHICH THE SIGN OF LONGITUDE CHANGES$

```

```

      BEGIN

```

```

        INTEGER K0$

```

```

        K0= ENTIER(V(K)/10000)$

```

```

        LALAT= K0/100$

```

```

        LALONG= (V(K)-10000*K0)/100

```

```

      END$ COMMENT DISSECTS

```

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```

```

PROCEDURE LIS(U)$ INTEGER US
COMMENT DETERMINATION OF LATITUDE AND LONGITUDE FOR
GRAPH POINTS$

```

```

BEGIN

```

```

  IF U EQL 19 THEN DT(12)

```

```

  ELSE IF U LEQ 11 THEN

```

```

    BEGIN

```

```

      DT(U)$ IF U EQL 0 OR U EQL 1 OR

```

```

      U EQL 2 THEN LALONG= -LALONG

```

```

    END

```

```

  ELSE IF U LEQ 26 THEN

```

```

    BEGIN

```

```

      LALAT= 35+US LALONG= 10

```

```

    END

```

```

  ELSE IF U LEQ 41 THEN

```

```

    BEGIN

```

```

      LALAT= 20+US LALONG= 20

```

```

    END

```

```

  ELSE IF U LEQ 56 THEN

```

```

    BEGIN

```

```

      LALAT= 5+US LALONG= 30

```

```

    END

```

```

  ELSE IF U LEQ 71 THEN

```

```

    BEGIN

```

```

      LALAT= U-11$ LALONG= 40

```

```

    END

```

```

  ELSE IF U LEQ 86 THEN

```

```

    BEGIN

```

```

      LALAT= U-26$ LALONG= 50

```

```

    END

```

```

  ELSE DT(U-74)

```

```

END$ COMMENT LIS$

```

```

PROCEDURE CTQ$

```

```

COMMENT THIS SUBROUTINE PREPARES THE TIME INSTANTS AT WHICH
IN EACH ZONE THE METEOROLOGICAL PARAMETER WILL BE
DERIVED FROM BOTH PARAMETER FIELDS, COMPOSITE CHARTS
IN TIME ARE SIMULATED$

```

```

BEGIN

```

```

  INTEGER JO,MOS

```

```

  REAL A,SUM,RESS$

```

```

  A= 0.4$

```

```

  JO = IF IO EQL 1 THEN KQ ELSE 0$ SUM= 0$

```

```

  FOR I= KQ-JO STEP IO UNTIL JO DO

```

```

    BEGIN

```

```

      SUM= SUM+(IF I GTR 3 AND I LSS 8 THEN 2*A ELSE A)$

```

```

      DD(I)= SUM

```

```

    END$

```

```

  MO = ZONEI(ST)$ RES= IF IO EQL 1 THEN DD(MO) ELSE

```

```

  DD(MO-1)$

```

```

  FOR I= 0 STEP 1 UNTIL KQ DO DD(I)= IF TT GTR 12

```

```

  THEN TT-12 ELSE TT+A/2+DD(I)-RESS$

```

```

END$ COMMENT CTQ$

```

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```

REAL PROCEDURE HH(V,W,F,CHOICE)$ INTEGER F,V,W$
BOOLEAN CHOICES
COMMENT COMPUTATION OF GRID POINT VALUES FOR GEOPOTENTIAL
OR TEMPERATURE (CHOICE = TRUE OR FALSE) $

```

```

BEGIN
  M5= (F-1)*125
  M6= (F+2)*125
  M3= HT(V+M5,W)$
  M4= HT(V+M6,W)$
  M1= ENTIER(M3/100)$
  M2= ENTIER(M4/100)$
  IF NOT CHOICE THEN
    BEGIN
      M1= M3-100*M1$
      M2= M4-100*M2
    END$
  HH= ((12-DD(M))*M1+DD(M)*M2)/12
END$ COMMENT HHS

```

```

REAL PROCEDURE GEOP(V,W,C,CHOICE)$ INTEGER C$
REAL V,W$ BOOLEAN CHOICES
COMMENT COMPUTATION OF GEOPOTENTIAL OR TEMPERATURE IN
ARBITRARY POINTS

```

```

BEGIN
  INTEGER V1,W1$ REAL A,B,B1,B2,B3,B4$
  V1= ENTIER(V)$ W1= ENTIER(W)$
  B1= IF CHOICE THEN HH(V1,W1,C,TRUE)
  ELSE HH(V1,W1,C,FALSE)$
  B2= IF CHOICE THEN HH(V1+1,W1,C,TRUE)
  ELSE HH(V1+1,W1,C,FALSE)$
  B3= IF CHOICE THEN HH(V1+1,W1+1,C,TRUE)
  ELSE HH(V1+1,W1+1,C,FALSE)$
  B4= IF CHOICE THEN HH(V1,W1+1,C,TRUE)
  ELSE HH(V1,W1+1,C,FALSE)$
  A= V1+1-V$ B= W1+1-W$
  GEOP= A*B*B1+(1-A)*B*B2+(1-A)*(1-B)*B3+A*(1-B)*B4
END$ COMMENT GEOPS

```

```

PROCEDURE XYTRANSF(LAT,LON)$ REAL LAT,LON$
BEGIN

```

```

  REAL R,S$
  R= (45-LAT/2)*CG$
  S= (80-LON)*CG$
  X= 0.7909*C0*SIN(R)*SIN(S)/COS(R)$
  Y= (P-C0*SIN(R)*COS(S)/COS(R))*0.7909
END$ COMMENT XYTRANSF$

```

```

REAL PROCEDURE GEODIST(DDD,LAT)$ REAL DDD,LAT$
COMMENT COMPUTATION OF DISTANCE ON THE SPHERE FROM
EUCLIDEAN DISTANCES

```

```

GEODIST= 219.721*DDD*COS((45-LAT/2)*CG)**2$

```

```

PROCEDURE GEOMGRID(PP,GG)$ INTEGER PP,GG$

```

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```

COMMENT COMPUTATION OF EUCLIDEAN DISTANCE AND UNIT VECTORS
BEGIN
  LIS(PP)$ LA1= LALATS L01= LALONG$
  LIS(GG)$ LA2= LALATS L02= LALONG$
  XYTRANSF(LA1,L01)$ X1= X$ Y1= Y$
  XYTRANSF(LA2,L02)$ X2= X$ Y2= Y$
  E3= SQRT((X2-X1)**2+(Y2-Y1)**2)$
  E1= (X2-X1)/E3$
  E2= (Y2-Y1)/E3
END$ COMMENT GEOMGRIDS

PROCEDURE PART2GEOMS
COMMENT DETERMINATION OF LENGTH OF SEGMENT BY SUMMATION OF
      CONTRIBUTIONS FROM SUBSEGMENTS$
BEGIN
  K1= ENTIER(X1)$ K2= K1+1$ L1= ENTIER(Y1)$
  L2= L1+1$ K1Q= ENTIER(X2)$ K2Q= K1Q+1$
  L1Q= ENTIER(Y2)$ L2Q= L1Q+1$
  D= GEODIST(E3,(LA1+LA2)/2)$
  N1= ABS(K1Q-K1)$
  N2= ABS(L1Q-L1)$
  N3 = IF K1Q EQL K1 AND L1Q EQL L1 THEN 0
  ELSE IF N1 LEQ N2 THEN N2 ELSE N1$
  BEGIN
    INTEGER I,J$
    LOCAL LABEL LAB1$
    AB(0)= 0$ AB(N3+1)= 1$
    IF N3 EQL 0 THEN GOTO LAB1$ IF N3 EQL N1 THEN
    BEGIN
      IF K1 GTR K1Q THEN
      BEGIN
        RES1= K1$
        RES2= K2Q$ RES3= -1
      END
      ELSE
      BEGIN
        RES1= K2$ RES2= K1Q$
        RES3= 1
      END$
      FOR I= RES1 STEP RES3 UNTIL RES2 DO
      BEGIN
        J= RES3*(I-RES1)+1$ AB(J)= (I-X1)/
          (X2-X1)
      END
    END
    ELSE
    BEGIN
      IF L1 GTR L1Q THEN
      BEGIN
        RES1= L1$
        RES2= L2Q$ RES3= -1
      END
      ELSE
      BEGIN

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```

RES1= L2$ RES2= L10$
RES3= 1
END$
FOR I= RES1 STEP RES3 UNTIL RES2 DO
BEGIN
J= RES3*(I-RES1)+1$ AB(J)= (I-Y1)/
(Y2-Y1)
END
END$
LAB1..
FOR I= 1 STEP 1 UNTIL N3+1 DO
BEGIN
AID2= ((AB(I)+AB(I-1))*LA2+(2-(AB(I)
+AB(I-1)))*LA1)/2$
LENGTH(I)= GEODIST(E3*(AB(I)-AB(I-1)), AID2)
END
END
END$ COMMENT PART2GEOMS

PROCEDURE METPROC(S)$ INTEGER S$
COMMENT PROCESSING METEOROLOGICAL PARAMETERS$
BEGIN
INTEGER I$
ARRAY TEMP,WNDX,WNDY,ENDUR(1..N3+1)$
GG1= GEOP(X1,Y1,S,TRUE)$
GG2= GEOP(X2,Y2,S,TRUE)$
ANGLE= C1*(GG2-GG1)/(470*D*SIN((LA1+LA2)*CG/2))$
XX1= X1$ YY1= Y1$
FOR I= 1 STEP 1 UNTIL N3+1 DO
BEGIN
XX2= AB(I)*X2+(1-AB(I))*X1$
YY2= AB(I)*Y2+(1-AB(I))*Y1$
AID2= ((AB(I)+AB(I-1))*LA2+(2-(AB(I)+AB(I-1)))*
LA1)/2$
XSTER= (XX1+XX2)/2$
YSTER= (YY1+YY2)/2$
KK1= ENTIER(XSTER)$ KK2= KK1+1$ LL1= ENTIER(YSTER)$
LL2= LL1+1$
TEMP(I)= -GEOP(XSTER,YSTER,S,FALSE)$
AID1= C1*E3/(D*SIN(AID2*CG))$ AID2= XSTER-KK1$
AID3= YSTER-LL1$
WNDX(I)= -AID1*(AID2*(HH(KK2,LL2,S,TRUE)-HH
(KK2,LL1,S,TRUE)))+(1-AID2)*(HH(KK1,LL2,S,TRUE)
-HH(KK1,LL1,S,TRUE)))$
WNDY(I)= AID1*(AID3*(HH(KK2,LL2,S,TRUE)-HH
(KK1,LL2,S,TRUE)))+(1-AID3)*(HH(KK2,LL1,S,TRUE)
-HH(KK1,LL1,S,TRUE)))$
TAS= 0.8034*38.9826*SQRT(273.16+TEMP(I))$
ENDUR(I)= 36000*LENGTH(I)/(TAS*SQRT(1-ANGLE**2)+
(WNDX(I)*E1+WNDY(I)*E2))$
XX1= XX2$ YY1= YY2
END$
ENDU= SUM1(1, N3+1, ENDUR)$
TEM= SUM2(1, N3+1, ENDUR, TEMP)/ENDU$

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```

TAS= 0.8034*38.9826*SQRT(273.16+TEM)$          ****400
RES1= 31+(S-1)*4$                                ****401
TDEV(S)= IF RES1 LEQ 35.332 THEN TEM +1.98*RES1-15 ELSE ****402
55+TEM$                                           ****403
TIME(S)= ENDU$                                    ****404
AIRDIST(S)= ENDU *TAS/36000$ LE= 0$             ****405
WIX(S)= SUM2(1, N3+1, ENDUR, WNDX)/ENDU$        ****406
WIY(S)= SUM2(1, N3+1, ENDUR, WNDY)/ENDU$        ****407
TAX(S)= TAS*(E1*SQRT(1-ANGLE**2)+E2*ANGLE)$      ****408
TAY(S)= TAS*(E2*SQRT(1-ANGLE**2)-E1*ANGLE)$      ****409
END$ COMMENT METPROC$                            ****410
                                                    ****411
COMMENT PROCEDURES 'TABLE' AND 'TABLEQ' ARE FOR TABLE LOOK-UPS ****412
INTEGER PROCEDURE TABLE(P,R,MA)$ INTEGER P,R$ INTEGER ARRAY ****413
MA$                                              ****414
BEGIN                                           ****415
  INTEGER GO,D,B$ REAL RO,C$ LOCAL LABEL LAB20$ ****416
  D=IF P EQL 0 THEN 68000 ELSE IF P EQL 1 THEN -10 ELSE 80000$ ****417
  B=IF P EQL 1 THEN 5 ELSE 4000$                ****418
  C= IF P EQL 1 THEN TDEV(R) ELSE GRWQ$          ****419
  RO= (C-D)/B$                                   ****420
  GO= ENTIER(RO)$                                ****421
  RO= RO-GO$                                      ****422
  IF MA(R,GO+1) EQL -1 THEN                      ****423
  BEGIN                                           ****424
    TABLE= -1$ GOTO LAB20                      ****425
  END$                                           ****426
  TABLE= RO*MA(R,GO+1)+(1-RO)*MA(R,GO)$        ****427
LAB20..                                         ****428
END$ COMMENT TABLE$                           ****429
                                                    ****430
INTEGER PROCEDURE TABLEQ(Q,L,MA0,MA1)$ INTEGER Q,L$ ****431
INTEGER ARRAY MA0,MA1$                          ****432
BEGIN                                           ****433
  INTEGER H,S0,Z,R,S00$                          ****434
  LOCAL LABEL LAB21$                             ****435
  REAL T0, T00$                                   ****436
  H= TABLE(Q,L,MA0)$                            ****437
  IF H EQL -1 THEN                                ****438
  BEGIN                                           ****439
    TABLEQ= -1$ GOTO LAB21                     ****440
  END$                                           ****441
  Z= IF Q EQL 2 THEN 0 ELSE IF Q EQL 3 THEN 50 ELSE 500$ ****442
  R= IF Q EQL 2 THEN 50 ELSE IF Q EQL 3 THEN 100 ELSE 1000$ ****443
  T0= (H - Z)/R$                                  ****444
  T00= (TDEV(L)+20)/5$                            ****445
  S0= ENTIER(T0)$                                 ****446
  S00= ENTIER(T00)$                               ****447
  T0= T0-S0$                                       ****448
  T00= T00-S00$                                    ****449
  IF MA1(S0+1,S00+1) EQL -1 THEN                 ****450
  BEGIN                                           ****451
    TABLEQ= -1$                                ****452
    GOTO LAB21                                   ****453

```

```

ENDS
TABLEQ=T0*T00*MA1(S0+1,S00+1)+(1-T0)*(1-T00)*
MA1(S0,S00)+(1-T0)*T00*MA1(S0,S00+1)+T0*(1-T00)*MA1
(S0+1,S00)$

```

LAB21..

```

ENDS COMMENT TABLEQ$

```

```

PROCEDURE READQ(Y0,Y1,Y2,ARR)$ INTEGER Y0,Y1,Y2$
INTEGER ARRAY ARR$
BEGIN

```

```

    FOR I= Y0 STEP 1 UNTIL Y1 DO
        FOR J=0 STEP 1 UNTIL Y2 DO
            READ(PCF('NASAD'), ARR(I, J), ERR, ERR)
        END$
    END$ COMMENT READ$

```

```

PROCEDURE WRITEQ(Y0, Y1, Y2, ARR)$
INTEGER Y0,Y1,Y2$
INTEGER ARRAY ARR$
BEGIN

```

```

    FOR I= Y0 STEP 1 UNTIL Y1 DO
        WRITE( FOT, Y2 + 1, FOR J= 0 STEP 1
            UNTIL Y2 DO ARR(I, J))$
    END$ COMMENT WRITEQ$

```

```

READQ(1,3,19,SR)$ READQ(1,3,6,MW)$ READQ(1,3,17,CD)$
READQ(1,3,17,CT)$ READQ(1,3,17,CF)$ READQ(0,7,8,CTC)$
READQ(0,7,8,CFC)$ READQ(0,6,8,CDC)$

```

```

WRITE(PEJT)$
WRITEQ(1,3,19,SR)$
WRITE(' '$ WRITE(' '$
WRITEQ(1,3,6,MW)$
WRITE(' '$ WRITE(' '$
WRITEQ(1,3,17,CD)$
WRITE(' '$ WRITE(' '$
WRITEQ(1,3,17,CT)$
WRITE(PEJT)$
WRITEQ(1,3,17,CF)$
WRITE(' '$ WRITE(' '$
WRITEQ(0,7,8,CTC)$
WRITE(PEJT)$
WRITEQ(0,7,8,CFC)$
WRITE(' '$ WRITE(' '$
WRITEQ(0,6,8,CDC)$

```

```

CG= 0.0174532925$ C0= 39.6296148$ C1= 21.47*32.808399$
P= C0*SIN(31.2*CG)/COS(31.2*CG)$

```

RUN..

```

READ(PCF('NASAD'), FLUR, TAXI, GRW, RESERVE, TOW,
MAXTOW,MAXLW,DATE,IO,TTT,ROUTE,DONE, ERR)$
WRITE(' '$ WRITE(' '$ WRITE(' '$
WRITE(' *** INPUT PARAMETERS ***'$
WRITE(FO2, 11, FLUR,TAXI,GRW,RESERVE,TOW,
MAXTOW,MAXLW,DATE,IO,TTT,ROUTE)$

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```

IF ROUTE GEQ 1111 THEN
BEGIN
  READ(PCF('NASAD'), Q, DONE, ERR)$
  WRITE(F02, 1, Q)$
  Q=Q-1$
END
ELSE
BEGIN
  READ(PCF('NASAD'), ST, ST1, DONE, ERR)$
  WRITE(F02, 2, ST, ST1)$
  G1Q= ZONEI(ST)$ G2Q= ZONEI(ST1)$ Q= ABS(G2Q-G1Q)
END$
TT = TTTS

BEGIN
  INTEGER ARRAY STOREI, STOREIQ, STOREG, STOREGQ, E(0..Q),
  F(-1..Q)$
  FORMAT F04(X63, I6, A2),
  F05('TRIP FUEL', I6, A1),
  F06('COST', D8.2, A1)$
  REAL ARRAY DECLTIME, DECLFUEL, DECLDIST(1..W)$
  INTEGER PROCEDURE SQ(H1, H2)$ INTEGER H1, H2$
  SQ= A(G1Q+I0*H1-1)+H2$
  INTEGER PROCEDURE JQ(H1, H2)$ INTEGER H1, H2$
  JQ= F(H1-1)+H2-STOREI(H1)+1$

  PROCEDURE DESCLIMB(S)$ VALUE S$ INTEGER S$
  COMMENT COMPUTATION OF PERFORMANCE IN CLIMB OR DESCENTS
  BEGIN
    INTEGER ALTS
    LOCAL LABEL JUM$
    ALT= 31+(S-1)*4$
    DECLTIME(S)= IF MQ EQL 0 THEN 60*TABLEQ(3, S, CT, CTC)
    /1000 ELSE 3.1+0.41*ALTS$
    DECLDIST(S)= IF MQ EQL 0 THEN TABLEQ(2, S, CD, CDC)
    ELSE 9+3*ALTS$
    DECLFUEL(S)= IF MQ EQL 0 THEN TABLEQ(4, S, CF, CFC)
    ELSE 940+8.5*ALTS$ IF DECLTIME(S) LSS 0 THEN GOTO JUM$

    AID4= DECLDIST(S)*60/(DECLTIME(S)*
    SQRT(TAX(S)**2+TAY(S)**2))$
    DECLDIST(S)= SQRT((0.75*WIX(S)+TAX(S)*AID4)**2+
    (0.75*WIY(S)+TAY(S)*AID4)**2)*(DECLTIME(S)-2)/60$
    AIRDIST(S)= (1-DECLDIST(S)/LE)*AIRDIST(S)$
    TIME(S)= AIRDIST(S)/SQRT(TAX(S)**2+TAY(S)**2)*
    36000$ LE= LE-DECLDIST(S)$

    JUM..

  ENDS COMMENT DECLIMB$

  REAL PROCEDURE ARCTANG(Q1, Q2)$ REAL Q1, Q2$
  ARCTANG= ARCTAN(Q2/Q1)/CG+(IF Q1 LSS 0 THEN 180
  ELSE IF Q2 LSS 0 THEN 360 ELSE 0)$

  PROCEDURE LO(Z1, Z2)$ REAL Z1, Z2 $

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COMMENT COMPUTATION OF LONGITUDE FROM EUCLIDEAN COORDINATES *****562
      IN RECTANGULAR GRIDS *****563
L01= 80-ARCTAN(Z1/(19-Z2))/CG$ *****564

INTEGER PROCEDURE HEADING(L1,L2)$ REAL L1,L2$ *****565
COMMENT COMPUTATION OF HEADING IN FLIGHTS *****566
BEGIN *****567
  REAL M1,M2,ZX,ZY$ *****568
  XSTER= (X1+X2)/2$ YSTER= (Y1+Y2)/2$ *****569
  LO(XSTER,YSTER)$ M1= SIN((80-L01)*CG)$ *****570
  M2= COS((80-L01)*CG)$ *****571
  HEADING= ARCTANQ(-L1*M1+L2*M2,L1*M2 + L2*M1) *****572
END$ COMMENT HEADING$ *****573

PROCEDURE LINE(N1,N2)$ BOOLEAN N1,N2$ *****574
COMMENT PRINT-OUT PROCEDURE$ *****575
BEGIN *****576
  INTEGER I,J,K,L,M,N,P,Q,R,S,T *****577
  FORMAT P1('TOC', 2I5, X12, I4, X10, I4, 3I6, I8, A2), *****578
  P2(I3, X22, I4, X10, I4, 3I6, I8, A2), *****579
  P3('TOD', 4I5, I6, I8, I6, 3I6, I8, A2), *****580
  P4(I3, 4I5, I6, I8, 4I6, I8, A2)$ *****581

  LOCAL LABEL LAB30,LAB31,LAB32$ *****582
  IF N1 THEN GOTO LAB30$ *****583
  IF N2 THEN GOTO LAB31$ *****584
  I=G3$ S=MQ$ T=B3$ *****585
  GEOMGRID(G4, G3)$ *****586
  J= HEADING (TAX(G), TAY(G))$ + *****587
  K= 310 + (G-1)*40$ *****588
  IF NOT N1 AND NOT N2 THEN BEGIN *****589
    L= TDEV(G)$ *****590
    M= SQRT(TAX(G)**2 + TAY(G)**2)$ *****591
  END$ *****592

  LAB30.. *****593
  *****594
  LAB31.. *****595
  *****596
  N= (IF N1 OR N2 THEN .75 ELSE 1)* *****597
    (WIX(G)*E1 + WIY(G)*E2)$ *****598
  M3= IF N1 OR N2 THEN *****599
    DECLTIME(G)*600 ELSE TIME(G)$ *****600
  P= 100*ENTIER(M3/36000) + MOD(M3, 36000)/600$ *****601
  Q= 100*ENTIER(FLTIME/36000) + MOD(FLTIME, 36000)/600$ *****602
  R= BURN - GRWQ$ *****603
  IF N1 THEN *****604
    BEGIN *****605
      WRITE(P1,J,K,L,M,N,DISTANCE,P,Q,R,GRWQ)$ *****606
      GOTO LAB32 *****607
    END$ *****608
  IF N2 THEN *****609
    BEGIN *****610
      WRITE(P2,ST1,N,DISTANCE,P,Q,R,GRWQ)$ *****611
      GOTO LAB32 *****612
    END$ *****613
  IF S EQL T THEN *****614
    WRITE(P3,J,K,L,M,N,LE,DISTANCE,P,Q,R,GRWQ) *****615
  ELSE WRITE(P4,I,J,K,L,M,N,LE,DISTANCE,P,Q,R,GRWQ)$

```

LAB32..

ENDS COMMENT LINES

```
PROCEDURE SPACEOPT(FBQ,FB,BI,BG,RR)$ INTEGER FB,RR$
BOOLEAN FBQ,BI,BG$
COMMENT FBQ DETERMINES WETHER THE FLIGHTPLAN
COMPUTATION WILL BE PERFORMED BACKWARDS(FALSE) OR FOR
WARDS(TRUE).
FB DETERMINES WETHER COSTS(+1) OR FUEL(0) OR FLIGHT
TIME(-1) WILL BE OPTIMIZED. RR IS TAKE OFF WEIGHT OR
LANDINGWEIGHT.
BI DEFINES WETHER THE NAVIGATION REGIME IS FREE IN THE
HORIZONTAL(FALSE) OR BOUNDED BY ONE POINT(TRUE).
BG DEFINES WETHER THE CRUISING ALTITUDE IS FREE(FALSE)
OR BOUNDED(TRUE)$
BEGIN
  LOCAL LABEL ITER, ENDG, CI, REPEAT, EIND$
  INTEGER AA,QUANT,II,JJ,GG,GRWP, DDG, DTG, TMGS
  BOOLEAN ITERATION, BCLIMB,BNQ,BNS
  INTEGER ARRAY ROW,ROWQ,QUANTQ(0..F(Q))$

  PROCEDURE PREP(A1,B1,AA,BB)$ INTEGER A1,B1$
  COMMENT COMPUTATION OF DISTANCE AND FLIGHT TIME, AND
  PRINT-OUT OF THE FLIGHT PLANS
  BOOLEAN AA,BB$
  COMMENT AA REFERS TO CLIMB, BB TO DESCENTS
  BEGIN
    DISTANCE= DISTANCE+A1$ FLTIME= FLTIME+B1$
    LINE(AA,BB)$ BURN= GRWQ
  ENDS COMMENT PREPS

  PROCEDURE EDITINGS
  BEGIN LOCAL LABEL ENDEDS
    FORMAT F03(X44, 'CH', I4, I6, D6.2, A2)$

    PROCEDURE QPS
    BEGIN
      IF FB EGL 1 THEN
        WRITE('COST')
      ELSE IF FB EGL 0 THEN
        WRITE('FUEL')
      ELSE IF FB EGL -1 THEN
        WRITE('FLTIME')$
      GOTO ENDEDS
    ENDS COMMENT QPS

    WRITE(PEJT)$
    *** DETAILED FLIGHT PLAN ***$
    WRITE(' ')$ WRITE(' ')$
    IF ROUTE EGL 1111 THEN
      BEGIN
        WRITE('NON SPECIAL MIN TRACK')$
      QP
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WRITE('

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ENDS		****670
IF ROUTE EQL 4444 THEN		****671
BEGIN		****672
WRITE('ATC I')\$ QPS		****673
ENDS		****674
IF ROUTE EQL 5555 THEN		****675
BEGIN		****676
WRITE('ATC II')\$ QPS		****677
ENDS		****678
IF ROUTE EQL 7777 THEN		****679
BEGIN		****680
WRITE('GRC')\$ QPS		****681
ENDS		****682
IF ROUTE EQL 9999 THEN		****683
BEGIN		****684
WRITE('SPECIAL TRACK')\$ QPS		****685
ENDS		****686
WRITE('MIN TRACK IN SPACE')\$ QPS		****687
ENDED..		****688
WRITE(F03, FLUR, DATE, TT)\$		****689
WRITE(' ')\$		****690
WRITE('NO. HEAD	FL TMP TAS WIND DIST ACCD TIME ACCT BURN WEIGHT	****691
)\$		****692
ENDS COMMENT EDITINGS		****693
PROCEDURE QQ(0)\$ INTEGER 0\$		****694
COMMENT COMPUTATION OF SEGMENT CONTRIBUTION. COST,		****695
TIME, FUEL, WEIGHT ETC.\$		****696
BEGIN		****697
LOCAL LABEL JM1, JM2, JM3, JM, ENDOS		****698
		****699
PROCEDURE CL(M1,M2)\$ REAL M1,M2\$		****700
COMMENT M1 DENOTES SEGMENT FUEL, M2 SEGMENT TIMES		****701
BEGIN		****702
LOCAL LABEL JUS REAL MMS		****703
IF BCLIMB THEN		****704
BEGIN		****705
MM= 0\$ GOTO JU		****706
ENDS		****707
IF ITERATION THEN		****708
BEGIN		****709
MM= IF G GEQ GG THEN -80		****710
ELSE -100\$ GOTO JU		****711
ENDS		****712
MM= IF (0 EQL -1 AND G GEQ GG) OR (0 EQL 1 AND		****713
G LSS GG) THEN 100 ELSE 80\$		****714
JU..		****715
MM= M1+ 0*(GG-G)* (IF MQ NEQ B1 THEN MM ELSE 0)\$		****716
GRWQ= GRWQ + 0*MMS		****717
QUANT= QUANT+(IF FB EQL 1 THEN 1083.3*M2+15*MM		****718
ELSE IF FB EQL 0 THEN MM ELSE 600*M2)\$		****719
ENDS COMMENT CLS		****720
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QUANT = QUANTQ(I)$
ITERATION= IF NOT FBQ AND MQ EQL 0 AND 0 EQL -1
THEN TRUE
ELSE FALSE$ IF ROW(I) EQL 0 THEN GOTO JMS
GRWQ= IF ITERATION THEN ROW(0) ELSE ROW(I)$
IF MQ EQL B1 OR ITERATION THEN
BEGIN
  IF DECLFUEL(G) LSS 0 THEN GOTO JMS
  BCLIMB= TRUE$ CL(DECLFUEL(G), DECLTIME(G))$
  BCLIMB= FALSE$
  DDG= DECLDIST(G)$ DTG= DECLTIME(G)*600 $
  IF ED THEN PREP(DDG, DTG, TRUE, FALSE)$
END$
IF NOT FBQ THEN GOTO JM2$

JM1..
AID4= IF TDEV(G) LSS -10 THEN 64.0&+6
ELSE TABLE(1,G,MW)$
IF GRWQ GEQ AID4 THEN GOTO JMS
IF NOT FBQ THEN GOTO JM3$

JM2..
GRWP= GRWQ$ GRWQ= GRWQ + 0* AIRDIST(G)/ 2*
(IF G EQL 1 THEN 4.94 +0.0000693* GRWQ ELSE
IF G EQL 2 THEN 0.54 + 0.0001043* GRWQ
ELSE -0.65+ 0.000117* GRWQ)$
AA= TABLE(0,G,SR)$ GRWQ= GRWP$
IF AA LSS 0 THEN GOTO JMS
CL(AIRDIST(G)*10**4/AA*TIME(G)/600)$
TMG= TIME(G)$
IF ED THEN PREP(LE, TMG, FALSE, FALSE)$
IF NOT FBQ THEN GOTO JM1$

JM3..
IF MQ EQL B3 AND NOT ITERATION THEN
BEGIN
  BCLIMB=
  TRUE$ CL(DECLFUEL(G),DECLTIME (G))$
  BCLIMB= FALSE$
  DDG= DECLDIST(G)$ DTG= DECLTIME(G)*600 $
  IF ED THEN PREP(DDG, DTG, FALSE, TRUE)$
END$
GOTO ENDQ$

JM..
GRWQ= 0$ QUANT= 64.0&+6$

ENDQ..
END$
COMMENT QG$

ED= IF B1 AND B6 THEN TRUE ELSE FALSE$
FOR AA= 0 STEP 1 UNTIL F(Q) DO
BEGIN
  ROW(AA)= ROWQ(AA)= 0$ QUANTQ(AA)= 64.0&+6
END$
QUANT= 0$ BCLIMB= FALSE$
IF FBQ THEN

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BEGIN	****778
ROW(0)= RRS QUANTQ(0)= 0	****779
END	****780
ELSE	****781
BEGIN	****782
ROW(F(Q))= RRS QUANTQ(F(Q))= 0	****783
ENDS	****784
IF ED THEN	****785
BEGIN	****786
DISTANCE= FLTIME= 0\$ BURN= ROW(0)\$	****787
EDITINGS WRITE(F04, RR)\$	****788
ENDS	****789
IF FBQ THEN	****790
BEGIN	****791
B1= 0\$ B2= 1\$ B3= Q-1	****792
END	****793
ELSE	****794
BEGIN	****795
B1= Q-1\$ B2= -1\$ B3= 0	****796
ENDS	****797
COMMENT ZONE CYCLE BEGINS\$	****798
FOR MQ= B1 STEP B2 UNTIL B3 DO	****799
BEGIN	****800
G1= IF FBQ THEN MQ+1 ELSE MQ\$	****801
G2= IF FBQ THEN MQ ELSE MQ+1\$	****802
M= 10*MQ+G1Q+(IF IO EQL -1 THEN -1 ELSE 0)\$	****803
	****804
	****805
COMMENT A CYCLE FOR GRAPH POINTS ALONG MERIDIAN	****806
BEGINS\$	****807
FOR JJ= STOREI(G1) STEP 1 UNTIL STOREIQ(G1) DO	****808
BEGIN	****809
G3= SQ(G1,JJ)\$ J= JQ(G1,JJ)\$	****810
COMMENT A CYCLE FOR GRAPH POINTS	****811
ALONG NEXT MERIDIAN BEGINS\$	****812
FOR II= STOREI(G2) STEP 1 UNTIL STOREIQ(G2) DO	****813
BEGIN	****814
IF NOT B1 THEN	****815
BEGIN	****816
IF(M GEQ 3 AND M LEQ 8) AND ABS	****817
(II-JJ) GEQ 10 THEN GOTO C1\$	****818
BNQ= (FBQ AND IO EQL -1) OR (NOT FBQ AND	****819
IO EQL 1)\$	****820
BN= (FBQ AND IO EQL 1) OR (NOT FBQ AND	****821
IO EQL -1)\$	****822
IF M LSS 3 THEN	****823
BEGIN	****824
IF(BNQ AND BK	****825
(M,JJ,II)) OR (BN AND BK(M,II,	****826
JJ)) THEN GOTO C1	****827
ENDS	****828
IF M GTR 8 THEN	****829
BEGIN	****830
IF (BNQ AND	****831

BKQ(M,JJ,II)) OR (BN AND BKQ
(M,II,JJ)) THEN GOTO CI

END

ENDS

G4= SQ(G2,II)\$ I= JQ(G2,II)\$

IF FBQ THEN GEOMGRID(G4,G3)ELSE

GEOMGRID(G3,G4)\$

PART2GEOMS

IF MQ NEQ B1 THEN GG=STOREG(MQ - B2)\$

COMMENT A CYCLE FOR FLIGHT LEVELS BEGINS\$

FOR G= STOREG(MQ) STEP 1 UNTIL

STOREGQ(MQ) DO

BEGIN

IF NOT FBQ AND MQ EQL 0 THEN

BEGIN

TEL = 0\$ IF G NEQ GG THEN

GOTO ENDG\$

N1= ROW(0)\$ ROW(0)= GRWQ=

MAXTOW-20000\$

TEL = TEL +1\$ IF G LSS 1

THEN

BEGIN

G= GG\$ GRWQ= 0\$

GOTO ENDG

ENDS

METPROC(G)\$ DESCLIMB(G)\$

IF DECLFUEL(G) LSS 0 THEN

BEGIN

TEL= 0\$ G= G-1\$ GOTO REPEAT

ENDS

QQ(-1)\$ IF GRWQ EQL 0 THEN GOTO ENDG\$

N2= ROW(I) - GRWQ\$ IF N2 GTR 10

AND ROW(0) EQL MAXTOW THEN GOTO

ENDG\$

ROW(0)= ROW(0) + (IF TEL GTR 10

THEN N2/2 ELSE N2)\$

GRWQ= ROW(0)\$ IF ABS(N2) LSS 10

OR TEL GTR 10 THEN

BEGIN

ROW(0)= N1\$ GOTO ITER

END

ELSE GOTO REPEAT\$

END

ELSE

BEGIN

METPROC(G)\$

IF MQ EQL 0 OR MQ EQL 0-1 THEN

BEGIN

GRWQ= RRS DESCLIMB(G)

ENDS

IF FBQ THEN QQ(-1) ELSE QQ(1)\$

REPEAT..

ITER..

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        IF GRWQ EQL 0 THEN GOTO ENDG
    ENDS
    IF QUANT LEQ QUANTQ(J) THEN
    BEGIN
        ROW(J)= GRWQ$ QUANTQ(J)= QUANTS
        ROWQ(J)= 1$ IF B1 AND NOT B6
        THEN STOREG(MQ)= G$
        IF ITERATION THEN G= G6
    ENDS

```

ENDG..

ENDS COMMENT FLIGHT-LEVEL CYCLES

CI..

ENDS COMMENT ALONG-NEXT-MERIDIAN CYCLES

ENDS COMMENT ALONG-CURRENT-MERIDIAN CYCLES

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    IF B1 AND NOT B6 THEN
        STOREGQ(MQ) = STOREG(MQ)
    ENDS COMMENT ZONE CYCLES

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        IF ROW(0) EQL 0 THEN GOTO EINDS
        IF B1 THEN GOTO EINDS J=IF FBQ THEN F(Q) ELSE F(0)$
    FOR MQ= B3 STEP -B2 UNTIL B1 DO
    BEGIN
        K= IF FBQ THEN MQ ELSE MQ+1$ I= ROWQ(J)$
        STOREIQ(MQ +(IF B3 EQL 0 THEN 1 ELSE 0))= I-F(K-1)+
        STOREI(K)-1$ J= 1$
    ENDS

```

FOR MQ= 0 STEP 1 UNTIL Q DO STOREI(MQ)= STOREIQ(MQ)\$

EIND..

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    TOWQ= ROW(0)$ M1= IF FBQ THEN QUANTQ(F(Q)) ELSE
    QUANTQ(0)$
    LW= ROW(F(Q))$ IF ED THEN
    BEGIN

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        WRITE(' ')$
        WRITE(F05, TOWQ-LW)$
        WRITE(F06, IF FB EQL 1 THEN M1/100 ELSE
        ((TOWQ-LW)*15+1083.3*FLTIME/600)/100)$
    ENDS

```

ENDS COMMENT SPACEOPTS

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    PROCEDURE FF(UU,VV)$ INTEGER ARRAY UU,VV$
    BEGIN

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```

        F(-1)= -1$ FOR K= 0 STEP 1 UNTIL Q DO
        F(K)= F(K-1)+VV(K)-UU(K)+1
    ENDS COMMENT FFS

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    PROCEDURE PROCES(S1,S2,S3,PR,FFBB,BB,FACTORISATION)$
    INTEGER S1,S2,S3,FFBB$ REAL PR$
    BOOLEAN BB,FACTORISATIONS
    COMMENT S1 AND S2 DETERMINE THE LIMITS OF FLIGHT
    LEVELS.
    S3 IS A DUMMY,EXCEPT WHEN

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FACTORISATION IS TRUE,
THEN S3 IS A DATUM FOR THE FLIGHT
LEVEL

IN WHICH THE M.F.P. IS COMPUTED,
PR IS PERCENTAGE TRIP FUEL
FFBB DETERMINES WETHER COSTS(+1),
FUEL(0) OR TIME(-1) IS OPTIMIZED,
BB..USE LANDING WEIGHT(TRUE),USE
TAKE OFF WEIGHT(FALSE)

FACTORISATION(TRUE) INITIALISES
PROCES IN THE HORIZONTAL ON THE
BASIS OF FLIGHT TIME,
FOLLOWED BY COMPILATION OF FLIGHT
PLAN IN THE VERTICAL ON THE BASIS
OF COSTS,FUEL OR TIMES

BEGIN

INTEGER NNS

LOCAL LABEL ENDPR,INGS

PROCEDURE AAS

COMMENT SPECIFICATION OF LIMITS IN HORIZONTAL OF
GRAPH POINTS ALONG MERIDIANS

BEGIN

LOCAL LABEL UTRECHTS

STOREI(0)=STOREIQ(0)=ST - A(G1Q-1)\$

STOREI(Q)= STOREIQ(Q)= ST1-A(G2Q-1)\$

IF ROUTE GEQ 1111 THEN GOTO UTRECHTS

FOR K= 1 STEP 1 UNTIL Q-1 DO

BEGIN

STOREI(K)= 1\$ STOREIQ(K)= E(K)

ENDS

UTRECHT..

FF(STOREI,STOREIQ)

ENDS COMMENT AAS

PROCEDURE

AAA(F1,F2)\$ INTEGER F1,F2\$

COMMENT SPECIFICATION OF LIMITS IN THE VERTICALS

FOR K= 0 STEP 1 UNTIL Q-1 DO

BEGIN

STOREG(K) = F1\$ STOREGQ(K) = F2\$

ENDS COMMENT AAAS

PROCEDURE EPS

IF TOWQ GEQ MAXTOW OR TOWQ EQL 0 THEN

BEGIN

WRITE('SUPER CRITICAL')\$

GOTO ENDPRS

ENDS COMMENT EPS

INTEGER PROCEDURE SSS

SS= GRW+RESERVE+PR*((GRW+RESERVE)*

(MINTIME*0.08-0.15)-500*MINTIME+7300+TAXI)\$

INTEGER PROCEDURE SSS\$

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SSS= GRW+RESERVE+PR*(TOWQ-LW+TAXI)\$

INTEGER PROCEDURE SSS\$

SSS\$= TOWQ*(GRW+RESERVE+PR*TAXI)/((1+PR)*NN-PR*TOWQ)\$

PROCEDURE NNQ(A)\$ VALUE AS INTEGER AS

NN= IF NOT BB THEN TOW ELSE AS

PROCEDURE TWS

COMMENT SAFEGUARDING AGAINST OVERLOADINGS

IF TOWQ GEQ MAXTOW OR TOWQ EQL 0 THEN

BEGIN

WRITE(PEJT)\$ WRITE('DECR LANDING W')\$

GOTO ENDPR

END\$

COMMENT IF FACTORIZATION IS TRUE, THEN THE OPTIMIZATION
TAKES PLACE FIRST IN THE HORIZONTAL AND THEN
IS FOLLOWED BY IN THE VERTICALS

IF FACTORISATION THEN

BEGIN

AAS AAA(S3,S3)\$ NNQ(SS)\$ ROUTE= 1111\$

SPACEOPT(IF BB THEN FALSE ELSE TRUE,-1,FALSE,

TRUE,NN)\$ TWS

AAA(S1,S2)\$ GOTO ING

END

ELSE

BEGIN

AAS AAA(S1,S2)\$ NNQ(SS)\$

SPACEOPT(IF BB THEN FALSE ELSE TRUE,FFBB,FALSE,

FALSE,NN)\$ TWS

ING..

EPS NNQ(SSS)\$

SPACEOPT (IF BB THEN FALSE ELSE TRUE,FFBB, TRUE,

FALSE,NN)\$ TWS

EPS NNQ(SSSS)\$

SPACEOPT(TRUE,FFBB,TRUE,TRUE,NN)\$ EPS

IF FACTORISATION THEN ROUTE= 1000

END\$

ENDPR..

END\$ COMMENT PROCESS

IF ROUTE GEQ 1111 THEN

BEGIN

READ(PCF('NASAD'), ST, ST1, DONE, ERR)\$

G1Q= ZONEI(ST)\$

FOR K= 1 STEP 1 UNTIL Q-1 DO

BEGIN READ(PCF('NASAD'), STOREI(K), DONE, ERR)\$

WRITE(FO2, 1, STOREI(K))\$

STOREI(K)= STOREIQ(K)= STOREI(K)-A(G1Q+I0*K-1)\$

END\$

G2Q = ZONEI(ST1)\$

WRITE(FO2, 2, ST,ST1)\$

****994

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ENDS
GEOMGRID(ST,ST1)\$ MINTIME=
GEODIST(E3,(LA1+LA2)/2)/465\$ CTQS
E(0)= E(Q)= 1\$ FOR K= 1 STEP 1 UNTIL Q-1 DO
E(K)= A(G1Q+IO*K)-A(G1Q+IO*K-1)\$

COMMENT

1. WHEN A FLIGHT PLAN FOR THE OPTIMAL COST TRACK IS NEEDED
CALL 'PROCES(1, 3, 1, 0.03, 1, TRUE, FALSE)'
2. WHEN A FLIGHT PLAN FOR THE OPTIMAL FUEL TRACK NEEDED
CALL 'PROCES(1, 3, 1, 0.03, 0, TRUE, FALSE)'
3. WHEN A FLIGHT PLAN FOR THE LEAST TIME TRACK NEEDED
CALL 'PROCES(1, 3, 1, 0.03, -1, TRUE, FALSE)'

PROCES(1, 3, 1, 0.03, -1, TRUE, FALSE)\$
PROCES(1, 3, 1, 0.03, 0, TRUE, FALSE)\$

GOTO RUN

ENDS

DONE.. ENDS
WRITE(' ') \$ WRITE(' ') \$
WRITE(' *** END OF RUN ***') \$
GO TO EOPS

ERR..

WRITE(' *** INPUT DATA ERROR ***') \$

EOP..

ELT NWS:1,810227,039147
*****<FGNAX23 *KWBC *160000<<QX\0.079213Q\03193103052310364032037513303948
3Q\131931027343103842320465231054460Q\232029025363004244300545330065443Q\3321
27035372705245280675428081406Q\431731024323002842300235329018498Q\531830027333
003342290345328038478Q\632028034352805143280615327071461Q\73222705336270784527
0935527106426Q\115213Q\032325050382506547260785626088378Q\132524053402406848
240765624079362Q\232723056422307050230775723078352Q\33292206144220765122082572
2081356Q\432526068392609047270995627107371Q\532826067422608149260845526084331Q
Q\633125064442507350250745425070326Q\733224065452407051240705524066315Q\15121
3Q\033222068452208253220885722084342Q\133422072472208554220905622084348Q\2336
21073482208454220875522079339Q\333721072492207954220795522071338Q\433423063462
306651230645423060310Q\533522058472306151230595423054307Q\63372205448230555123
0535423049308Q\733921050492204952230465323042292Q\187213Q\033922071502207654
230725423063331Q\134122067512307254230665423056311Q\23442305852230645324059532
4050303Q\334723045542405153240475224043287Q\434022046502204452230395224035298Q
Q\534222042512304151240365225033281Q\634523035522403652250335126032271Q\734723
028532503052260305127031270Q\223213Q\035024033562403854250375225035286Q\1
435224028582503155250305225029286Q\235325025582502555250245225023286Q\33532401
7572401655240165224016275Q\435024023552602553270275127029279Q\5351250225627024
54270255128026280Q\635225020572702154280215128021280Q\735326014572801454280145
229014285Q\259213Q\035320009572000755200085321009283Q\1353140125814012561401
05315007289Q\235213018591302057130155413010292Q\080213Q\03163001730290294129
0325328031504Q\131828024322703942270445326047487Q\2320270413426060432606954260
764626Q\332227060362608445260965526106438Q\431627016302703140270365327040504Q\1
531826033322605141260575426059488Q\632026046342606643260765526082451Q\73222705
6362607845260935526103434Q\116213Q\032527070392709347271045627113379Q\132927
068422708149270875527093336Q\233127063442706850270705527072311Q\33322705444280
5650280575527058298Q\432428060392707947270955627104375Q\5327290584129068492807

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AT **VD<:ALANA AX

83261	82800	82857	81755	83951	84749	85253	87254	88357	88655	88555	88555
82860	82958	83055	84252	85450	86450	87551	88653	89254	89754	89854	90155
82757	84056	85153	86451	87850	88949	89850	90451	90752	90952	90851	90850
84355	85453	86851	88349	90248	91249	91749	91650	91450	91350	91450	91650
84651	86451	88149	89847	91547	92547	92848	92349	91950	91650	91750	91650
86049	86850	88547	90346	92045	92945	93146	92648	92149	91849	92049	92050
85450	86349	88446	90345	92145	93045	93145	92846	92446	92146	92246	92145
85049	85647	86945	88844	90945	92444	92945	92945	92745	92545	92645	92345
85352	85048	85646	87045	89344	91344	92444	92945	93245	93245	93145	93345
84952	85049	85146	86044	87944	89745	91345	92345	93045	93345	93045	93045
87254	86050	85646	85944	87144	88544	90145	91445	92345	92645	92345	92145
88152	87351	87048	86746	86845	87645	89146	90546	91546	91646	91645	91645
89352	88752	88351	87949	87748	87948	88949	90149	90848	91048	91148	91048
90152	89853	89453	89252	89150	89050	89650	90550	90650	90950	91050	91050
90851	90451	90251	90051	90050	90050	90650	91150	91150	91350	91250	91150
90451	90451	90851	90350	90348	90250	91750	92150	91650	92150	91750	91750

92950	93450	93554	93955	95155	95252	96954	97257	98758	98657	101154	101660
93750	94351	94953	95855	97155	97955	99157	99559	99959	100159	101258	101760
95150	95551	96452	98055	99656	100558	101559	101860	101561	101561	101960	102460
95949	96651	97953	99955	101756	103158	103660	103561	102961	102661	102860	103559
95950	97351	99054	101155	102955	104257	104657	104357	103758	103359	103259	103359
96749	97950	99753	101754	103555	104655	105055	104855	104456	103857	103458	103158
96950	98049	99553	101454	103256	104655	105054	105054	104854	104255	103755	103055
97450	97648	98751	100553	102555	104055	104754	105054	105054	104655	104455	104155
98048	97747	98048	99250	100854	102755	104154	104654	104954	104954	104954	104655
98049	97947	97845	98646	99850	101153	102454	103354	104254	104854	105253	105454
98952	98449	98045	98144	98847	99850	100753	101953	103554	104654	105153	105453
99455	99153	98648	98546	98747	99049	99751	101152	102854	104054	104754	105154
101562	100358	99653	99851	99649	99450	99751	100652	101954	103254	104354	105454
100962	101060	100856	100855	100854	100654	100554	100954	101854	102854	103854	104754
101659	101660	101456	101356	101356	101456	101656	101955	102654	103054	103654	104554
101860	101360	101755	101755	101755	101756	102555	102654	103454	103354	103354	103754

108055 108055 108155 108855 108955 110552 109952 112252 112552 113855 114358 115560
108955 108854 109055 109856 110758 111657 112458 113458 113758 114157 114858 115360
109351 109652 110255 111458 112862 113563 114563 115163 115163 115261 115460 115661
110147 110851 111655 113160 114465 115768 116667 116667 116667 116464 116263 116260
110651 111453 112757 114763 116268 117469 118068 117868 117668 117365 116765 116065
111351 112153 113658 115764 117269 118369 118768 118467 118167 117766 117166 116465
111646 112751 114257 116164 117667 118668 118867 118666 118666 118365 117865 117365
111945 113048 114253 116059 117463 118465 118865 118965 118965 118965 118665 118365
113044 113146 113450 114953 116357 117458 118260 118862 119064 119263 119164 118965
113344 113044 113046 114048 115150 116251 117255 118357 119058 119459 119562 119765
113248 113247 113045 113445 114145 114746 115849 117252 118355 119157 119561 120063
114151 113950 113648 113746 114043 114944 116247 117550 118555 119259 119961
114753 114751 114550 114448 114446 114444 114643 115444 116748 117953 119057 120159
115755 115453 115253 115150 115149 115147 115144 115444 116747 117851 118955 120061
116255 116155 115854 115652 115951 116049 116047 116447 117249 118053 118757 119565
116955 117055 116755 116053 116852 117049 116648 117250 118251 118258 118359 118666

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83261	83162	83261	82857	83357	84753	86050	85250	85350	87250	88650	90150
82559	83558	84458	85056	85454	86351	87550	87750	87850	88650	89750	90350
83356	84256	85555	87052	87948	88647	89549	90050	90251	90550	91150	91950
84152	85053	86652	88649	90046	91046	91648	91950	91851	91650	91750	91650
85150	86151	87750	89648	91245	92245	92548	92750	92451	92150	91750	91550
85249	86050	88250	90048	91645	92645	92947	92949	92650	92250	91750	91551
85050	86350	87950	89648	91245	92544	92944	93046	92847	92348	91950	91551
84847	85548	86448	87946	89944	91643	92543	92944	92945	92647	92348	92148
85253	85450	85848	86746	88444	90143	91442	92343	92645	92746	92946	93246
85053	86051	85949	86247	87346	88745	90044	91144	91944	92545	93044	93243
86950	86954	86852	86649	87048	87947	89046	90045	91045	91945	92845	93445
87350	87853	87954	87652	87650	88150	88749	89348	90248	91247	92246	92945
88753	88754	88953	89054	89051	89150	89250	89350	89950	90849	91748	92445
89852	89652	89653	90252	90351	90350	90250	90350	90650	91150	91550	91548
91246	90348	90950	91250	91450	91550	91250	91350	91450	91550	91550	91650
91749	91650	91950	92250	92550	92450	91750	91750	91750	91750	91650	91650

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93855	93255	92955	93455	94455	96355	96655	98155	97759	99260	100261	101362
94355	94455	94655	95455	96655	97755	98455	99556	100259	100860	101361	101762
95355	95655	96055	97755	99255	100255	101055	101957	102659	102860	102760	102862
96557	97556	98456	99956	101656	102557	103156	103658	104059	103960	103660	102661
96554	97855	99456	101157	102957	103957	104456	104656	104657	104258	103560	102760
96953	98054	99655	101656	103457	104457	104855	104755	104656	104058	103460	102961
97048	98153	99655	101455	103356	104456	104955	104955	104755	104156	103859	103562
98049	98151	98952	100453	102254	103750	104556	104855	104854	104655	104357	104058
98251	97849	98248	99248	100850	102453	103655	104254	104653	104754	104955	105355
97353	97749	97940	98644	99746	101049	102152	103152	103953	104554	104954	105352
98255	98452	98548	98746	99345	100047	100849	101750	102851	103953	104754	105355
99663	99558	99654	99748	99848	100449	101150	101851	102952	104154	104755	
100065	100562	100859	100856	100654	100552	100951	101352	101852	102653	103754	104455
101761	101662	101761	101860	101657	101755	101954	102054	102454	102955	103555	104055
102660	102661	102561	102461	102361	102757	102955	102855	102955	103155	103355	103255
103560	103561	103459	102659	102760	103458	103755	103655	103455	103355	103355	103255

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110755 111355 112350 113662 114966 115968 116869 117569 117869 117568 117167 116562
111655 112356 113659 115084 116369 117269 117868 118367 118566 118267 117667 117164
111650 112754 114257 115762 117166 118067 118566 118764 118763 118464 118065 118065
111744 112649 113852 115557 117161 118263 118863 119061 118860 118461 118063 117764
111342 112245 113146 114651 116255 117657 118659 118960 118960 118560 118360 118360
111544 112244 112743 113645 115247 116750 118054 118657 118959 118861 118761 118460
112245 112545 112744 113443 114443 115645 117048 117852 118455 118859 119061 119262
112945 113045 113145 113644 114244 115044 116144 117046 117751 118456 118860 119263
113750 113646 113947 114346 114545 114944 115443 116144 116948 117954 118658 119060
114455 114453 114652 115150 115247 115546 115945 116145 116647 117453 118357 118759
115955 115755 115854 115953 115950 116147 116346 116547 116849 117452 118154 118454
116455 116655 116455 116455 116353 116450 116649 117150 117453 117854 117955 118055
117455 117255 116755 116755 116455 116455 116452 118055 118055 118055 118055 118055

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400	470	480	490	500	515	530	545	560
1450	1445	1460	1480	1500	1550	1600	1645	1690
2220	2280	2340	2420	2500	2620	2740	2870	3000
2950	3050	3180	3350	3500	3700	3920	4200	4470
3660	3850	4050	4280	4500	4850	5150	5670	6320
4370	4590	4880	5150	5500	6000	6670	7530	8520
5050	5260	5650	5950	6500	7200	8500	9900	12150
5650	5900	6280	6720	7500	8700	11050	-1	-1

West bound

(1) 0 111

-1 142900 93000 51281

*** INPUT PARAMETERS ***

1 1500 75000 10000

0 115

L2
-9.0546E-01 -6.2619E-01
-0.0118E
0.5015E+00

L2
-9.3907E-01 -3.5552E-01
0.151E

1.7445E+02 1.7445E+02

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GENERAL

This program which was written for experiments of three dimensional flight planning for DC8-D3 aircrafts over the North Atlantic has been converted for use in UNIVAC 1108 in ALGOL 60 and will be enhanced to be appropriate for flight planning for DC10 and B747 aircrafts.

Reference is made to pages and formulas in 'Optimal Track Selection and 3-Dimensional Flight Planning' written by H. M. DE JONG, KNMI No. 93.

INPUT/OUTPUT DATA DESCRIPTION

INPUT

METEOROLOGICAL DATA

There are six data tables for compressed meteorological data (geopotential height(in gpdam)and temperature(centigrade degree)).

See p. 126, Fig. 39.

Geopotential values and temperature are depicted from the grid points in a Cartesian grid superposed on a polar stereographic chart projection with standard parallel at 60 degree N.

This grid is part of the well-known octagonal grid prepared by the National Meteorological Center.

The y-axis runs parallel with the 80 degree W meridian.

The area covered is rectangle comprising 12 x 16 grid points.

See output listing.

Those six tables show meteorological data (each table 12 x 16) for 200, 250, and 300 mbar for two validity times 12 hours apart.

PERFORMANCE DATAORIGINAL PAGE IS
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See output listing.

TABLE 1 shows specific range for flight levels 310, 350, and 390

(see p.116, table 1). This is an important economic index which is the air distance covered by a turbo-jet aircraft per unit of fuel consumption.

This datum is almost independent of temperature and depends on the aircraft weight only at a prefixed flight level.

TABLE 2 shows maximum weight(kg) per flight levels 310, 350 and 390

(see p. 122, table 9). The maximally allowable weight depends on flight altitude and temperature deviation from standard.

TABLE 3 shows climb distance (nautical mile) as a function of weight (kg) and flight levels 310, 350, and 390.

See P.118, table 5.

TABLE 4 shows climb time (1/1000 hrs) as a function of weight (kg) and flight levels. See p.117, table 3

TABLE 5 shows climb fuel (kg) as a function of weight and flight levels.

See p.119, table 7.

TABLE 6 shows climb time temperature correction as temperature deviation and climb time (1/1000 hrs) at standard temperature.

See p. 117, table 4.

TABLE 7 shows climb fuel temperature correction (kg). See p.119, table 8.

TABLE 8 shows climb distance temperature correction (n.m).

See p.118, table 6

INITIALIZING INPUT PARAMETERS:

FLUR = sequence number.

TAXI = taxi fuel (kg).

GRW = zero fuel weight (kg).

RESERVE = reserve fuel (kg).

TOW = -1 computaion starting in end-point of flight.

MAXTOW = maximum take-off weight.

MAXLW = maximum landing weight.

DATE = date/month/year.

ID = -1; east bound flight, 1; west bound flight.

TTT = time of departure.

ROUTE = route indicator.

SI = starting graph point number.

ST1 = destination graph point number.

Note here that all input data are read from card images of PCF file.

PCF file name is NASAD.

OUTPUT

In the flight plan (see output listing),

NO. = graph point number.

HEAD = heading in flight.

FL = flight level in 100 ft.

TMP = off standard temperature in centigrade degrees.

TAS = true air speed.

WIND = tail (head) wind along the track.

DIST = distance of flight segment.

ACCD = accumulated distance flown(n.m).

TIME = time along segment flown.

ACCT = accumulated time flown (hr, min).

BURN = fuel consumed in segment (kg).

WEIGHT = weight (kg).

TOC = top of climb.

TOD = top of descent.

EXTRA COMMENTS FOR THE PROGRAM.ORIGINAL PAGE IS
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46 - 49

Procedure INTERPOL computes a linear interpolation.

51 - 59

Procedure SUM1 and SUM2 compute summations.

These procedures are used for computing average values in procedure METPRDC.

72 - 73

Procedure WW is a write-procedure.

76 - 77

p1, p2, and p3 are flight levels.

q1, q2, and q3 are pressure altitude for standard pressure levels 300, 250, and 200 mbar.

78 - 84

reads in compressed values for geopotential height and temperature in 200, 250, and 300 mbar, valid for two standard times, 12 hours apart and fills array HT with those data.

85 - 90

writes out the inputted data for checking purposes.

92 - 113

produces the meteorological parameters (compressed geopotential and temperature data, which apply in grid points at flight levels 310, 350 and 390. Therefore the inputted data for the standard pressure altitude are destroyed

115 - 118

The graph points are labelled by numbers running from 0 to 115.

(note that the graph point number shown in Fig. 37, F.110 runs from 1 to 116).

The graph is such that the point sets consist of subsets of points arranged along 'meridians' (index running from 0 to 15).

Array A(index) contains the graph point number assigned to the most northerly point on each meridian.

Array A is used for the computation of zone index (procedure ZONEI).

119 - 133

Array V has values assigned for geographic coordinates for graph points and check points on continents : latitude (4 digits) and longitude (4 digits) in degrees and hundredths. See Fig. 37, P.110.

135 - 142

fills Boolean array BK and BKQ with 'TRUE' ; (initialization).

143 - 156

denotes blocking in continental airways (connectivity in the graph). Boolean array entries of BK and BKQ indicate which graph points are connected or blocked (TRUE=blocked and FALSE=connected). Array BK is used for the zone index < 3 and array BKQ is used for the zone index > 8.

BK(a,b,c)=FALSE means point 'b' on meridian 'a' is connected with point 'c' on meridian 'a+1'.

Here point 'b' denotes the 'b' th point from the bottom on the meridian. Example: see Fig. 37. BK(2,2,2) = FALSE means graph point number 3 on meridian 2 is connected with graph point number 5 on meridian 3

153 - 172

Procedure ZONEI determines the index of the zone associated with a graph point number. Parameter Q = graph point number. For example, a graph point number 49 gives ZONEI(49)=6.

174 - 183

Procedure DT dissects latitude and longitude from the compressed coordinates

LALAT means latitude and LALONG means longitude.

Parameter K is an index of array V.

185 - 216

Procedure LIS determines actual latitude and longitude value for a graph point. (see procedure DT).

The sign of longitude is changed in east of Greenwich.

Parameter U=graph point number.

218 - 237

Procedure CTQ prepares a time instant array DD, zonally specified, to be used for the time interpolation later on.

A=0.4 denotes an estimated flight time of 24 min. per continental zone.

There are 15 instant values (index 0 - index 14).

239 - 256

Procedure HH computes grid point values for geopotential or temperature (CHOICE=TRUE computes geopotential value, while CHOICE=FALSE computes temperature value) in flight level index F (index 1 denotes 31000 ft and indices 2 and 3 denote 35000 and 39000 ft respectively).

Parameters V and W denote index numbers of array HT (meteorological).

Interpolation takes place according to zone-assigned time instants DD().

258 - 275

Procedure GEOP computes geopotential (when CHOICE=TRUE) or temperature (when CHOICE=FALSE) value in arbitrary point, using adjacent grid point values from array HT (see procedure HH) and bi-linear interpolation.

Parameters V and W will be modified to denote index numbers of array HT. Parameter C = flight level index.

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277 - 284

Procedure XYTRANSF converts the geographical coordinates (LAT, LON) of a point on earth into the Cartesian coordinates (Y, X).

See P. 62-63.

286 - 289

Procedure GEODIST computes distance on the sphere from Euclidian distance DDD given in units of the rectangular grid on the map.

LAT denotes latitude.

291 - 301

Procedure GEOMGRID computes Euclidian distance and unit vector pointing along an arc in the graph between two arbitrary graph points with respect to rectangular grid system.

FP and GG denote graph point numbers of end points.

E3 denotes Euclidean distance.

E1 and E2 denote unit vectors for x,y components respectively.

303 - 363

Procedure PART2GEOM determines length of segment by summation of contributions from subsegments (LENGTH(I)).

These subsegments are identified by intersection of an arc with coordinate lines in Euclidean grid.

Normalized coordinates (running from 0 to 1) are stored in array AB.

These values serve also as weighting factors later on.

D denotes distance computed for averaged degree of latitude on the sphere. Array LENGTH(I) contains lengths of subsegments on the sphere. AID2 denotes interpolated degree of latitude.

See P. 84-85.

365 - 410

Procedure METPROC processes meteorological parameters.

Parameter S=flight level index (1,2 or 3).

DETAILS

370 - 371

computes geopotential value at end-points of a flight segment.

372

computes drift angle by using Bellamy's formula (see P. 78).

376 - 381

estimates coordinates in mid point P of segment. $P=(X_{ster}, Y_{ster})$.

384

estimates temperature in mid point P at flight level S.

Temperature has minus sign.

397 - 392

wind components, geostrophic wind. Formulas shown in P.69-70 is not used (reason: not to smooth too drastically from geopotential fields, and to economize in speed of computation by computer).

See formulas 5.22 and 5.23 in p.66.

Array WNDX and WNDY contain x-component and y-component of wind resp.

393

computes true air speed (TAS) for the specific type of aircraft.

For values of constants see Smithsonian tables, Meteorological text books or ICAD Standard Atmosphere.

394 - 395

computes flight time components using vector sum of wind and TAS, and segment length (LENGTH (I)).

398 - 409

determines average values for meteorological and other parameters along segment under consideration using previously calculated contributions.

TEM=temperature. TDEV(S)=temperature deviation.

TIME(S)=flight time in flight level index S.

AIRDIST(S)=air distance.

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LE=distance of flight segment.

WIX(S) and WIY(S) = wind components.

TAX(S) and TAY(S) = true air speed components.

413 - 429

Procedure TABLE and TABLEQ are for table look-up procedure for performance data. See P.116-119 and output listings.

441 - 497

Procedure READQ reads in performance data and procedure WRITEQ directly writes out those inputted data for checking purpose.

499 - 500

coefficients used in algorithms.

502 - 507

reads in and writes out initializing input parameters for flight plan.

508 - 520

In case of prescribed track flight, the routine reads in Q (number of graph points on the prescribed route).

In another case, it reads in ST(starting point number) and ST1(ending point number) and decides Q value.

In the latter, $Q = (\text{number of zones between source and destination}) - 1$.

529 - 532

Procedure SQ and JQ are conversion formulas for indices used in subsegment algorithms (by using entries of array A(index) or array F(index)).

534 - 555

Procedure DESCLIMB computes performance by using the table look-up procedure in climb(if MQ=0) or descend(if MQ not= 0).

Array DECLTIME gets climb time or descent time.

Array DECLDIST gets climb distance or descent distance.

Array DECLFUEL gets climb fuel or descent fuel.

Array AIRDIST gets climb air distance or descent air distance.

Array TIME gets climb time or descent time.

Note that in the descent zone, performance data table is not used.

So specific expressions by company's planning policy are chosen.

See formula 6.31 in P.120-121.

557 - 559

Procedure ARCTANG is for computation of heading degree by using arc tangent formula.

561 - 564

Procedure LD is for computation of longitude from Euclidean coordinates in rectangular grid. See P.62, formula 5.17 and 5.18.

Z1 and Z2 denote Euclidean coordinates.

566 - 574

Procedure HEADING computes heading in degree as required for flight planning purposes.

L1 and L2 denote x-component and y-component of true air speed.

576 - 617

procedure LINE writes out optimized flight plan.

See the output listing of the flight plan.

619 - 926

Procedure SPACEOPT is a key procedure for optimization.

In this procedure crucial is that some parameters may not surpass upper bounds, for example aircraft weight.

This requires the inclusion of several protective statements in order to ensure proper functioning of the operational scheme in-flight.

FBQ determines whether the flight plan computation will be performed backward(false) or forward(true).

FB determines whether cost(+1) or fuel(0) or flight time(-1) will be optimized.

BI determines whether the navigation regime is free in the horizontal (false) or bounded by one point(true).

BG determines whether the cruising altitude is free(false) or bounded (true).

RR is take-off weight or landing weight.

DETAILS:

637 - 645

Procedure PREP computes distance and flight time, and prints out one line of flight plan.

A1=segment distance. B1=segment flight time.

AA=true denotes 'climb' and BB=true means 'descent'.

See the output listing of the flight plan.

647 - 694

Procedure EDITING prints out proper heading lines.

696 - 768

Procedure QQ computes segment contribution, fuel, etc.

When o=-1 computation is for in-flight direction.

When o=+1 computation is for opposite flight direction.

702 - 722

Procedure CL computes the aircraft weight(GRWG) and total fuel, flight time or costs at end-point of a flown segment. (the contribution of fuel in steps included).

Parameter M1 denotes segment fuel(kg) and M2 segment time(min).

In the climb phase no step contribution is taken into account as

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required(BCLIMB=TRUE)

GG denotes flight level index at the graph point when the computation starts. G denotes the flight level index to be investigated.

Step consumption: UP=100 kg/4000ft

DOWN=-80 kg/4000ft.

(surplus of segment fuel)

ITERATION becomes TRUE when (1) back-tracking (2) first zone is reached (3) TDW is unknown and Wb is known (see P.120).

In array ROW the aircraft weight is stored.

GRWQ denotes aircraft weight at the end point of segment.

QUANT denotes cost, fuel or time at the end point of flown segment.

729 - 736

computation in climb or descent by procedure CL.

If ED is TRUE then it prints out the results.

739 - 741

safeguarding statements.

744 - 752

computes segment contribution of changes in aircraft weight.

Note that fuel consumption is expressed as loss of aircraft weight.

The table for specific range (P.116) is used.

Formula 6.27 (P.115) requires an estimate of weight halfway a flight segment. For that purpose coefficients as shown in table 2, P.116 are required (r1, r2).

753

jumping back to label JM1 is for safeguarding that the actually derived aircraft weight does not surpass the maximally allowed weight.

755 - 762

computes the contribution for the last segment.

If ED is TRUE then it prints out the results.

765

GRWQ and QUANT attain absurd values for safeguarding operational performance

771

ED becomes TRUE when all degrees of freedom in the horizontal and the vertical are lost, for example when a call of procedure SPACEOPT takes place in the final mode for flight plan computation along the (optimal) track found in previous calls.

(when navigation regimes is bounded by one point and cruising altitude is bounded).

772 - 797

Initialization and preparation of all parameters needed for the algorithmic process of optimization.

FBQ=TRUE means flight plan computation will be performed forwards, while FBQ=FALSE backwards.

Array F is filled in line 928-932 (see procedure FF).

The process can be activated for arbitray begin- and end-points.

In order to reduce storage space a renumbering is made for all subset points. So array F is defined and functions completely analogous to array A for whole graph point set.

Array STOREI and STOREIQ contain the assigned numbers of labelled end-points on meridians in the subgraph.

Zone cycle runs from line 799 to 904.

The zone cycle repeats as many times as the number of zones.

A cycle for graph points along meridian runs from line 806 to 900.

This cycle repeats as many times as the number of graph points in the current meridian.

A cycle for graph points along next meridian runs from line 811 to 848.
This cycle repeats as many times as the number of graph points in the next meridian.

A cycle for flight levels runs from line 842 to 896.

This cycle repeats as many times as the number of flight levels used.

810

conversion for indices used in subsequent algorithms.

815 - 835

If the navigation is free (BI=FALSE) in the horizontal, it checks whether a segment (II, JJ) is blocked or not.

BK or BKQ = TRUE means airway is blocked.

If blocked, it skips computation for the segment.

836 - 840

conversion for indices (point G4).

determines geographic elements for a segment between points G3 and G4.

See procedures GEOMGRID and PART2GEOM.

846 - 875

In case of backtracking in a flight plan computation an iteration process is put into action in the climb zone.

This is done in order to determine the (unknown) take-off weight by iteration in such a way that the climb parameters do match with the parameters found during backtracking when arriving in the climb zone.

The iteration starts with a take-off weight 20000 kg below the (known) maximum take-off weight.

Array ROW contains the (optimal) value of aircraft weight found during optimization, using a zone-cycle.

The iteration finishes when either the weight difference at the point of matching is less than 10 kg or the number of iteration steps

exceeds 10 (poor convergence).

In each step take-off weight is adjusted, see line 865-875.

879 - 887

similar computations but not backtracking case or not take-off weight adjustment case.

888 - 894

These statements are crucial optimization criteria.

909 - 925

Preparation of elements which are required for a subsequent call for procedure SPACEOPT with lessened number of degrees of freedom including a final call for computation and presentation of flight plan data. In this final stage no degrees of freedom are left. Procedure SPACEOPT then merely operates along a predefined track (the solution of previous calls).

928 - 932

Procedure FF determines a zone index array F for a subset of graph points analogous to array A. (array F is a sub-zone array).

934 - 1035

A call for procedure PROCES results in the production of a flight plan along whatever route is desired.

DETAILS

962 - 973

Specification of limits in horizontal of graph points along meridians. Array STOREL and array STOREIG store lower limits and upper limits respectively for the number of graph points on each meridian. If route ≥ 1111 , then production of flight plan along a prescribed route

In this case the procedure SPACEOPT works in a degenerate mode.

975 - 980

Specification of limits in the vertical.

Array STOREG and array STOREGQ store lower limits and upper limits respectively for the number of flight levels on each meridian.

982 - 987

Procedure EP indicates that the flight planning computation blows up.

989 - 1000

See P. 123-124 for procedures SS, SSS and SSSS.

These procedures compute landing weights.

NN contains landing weight or take-off weight.

1002 - 1008

Procedure TW is for safeguarding against overloading.

1011 - 1035

activates process as follow:

If FACTORIZAION is TRUE, then the optimization takes place first in the horizontal and is followed by an optimization in the vertical.

The following steps occur:

- (a) optimization in the horizontal based on time.
- (b) optimization in the vertical, using the track solution found in (a) and based on fuel, time or costs.
- (c) computation of flight plan along solution found in (b).

If the optimization takes place in free space, the sequence of calls results in:

- (i) optimization in space based on time, fuel or costs.
- (ii) optimization in the vertical through horizontal track found in (i), based on time, fuel or costs.
- (iii) compilation flight plan along track solution found in (ii).

Note that (ii) could be bypassed as the solution is found already

in (i). But (ii) can be generated with a slightly different landing weight. The compilation of a flight plan along a prescribed route passes through all three procedure calls.

This means that in fact the computation is repeated threefold, however with properly tuned landing or take-off weights.

In order to protect against subsequent calls of procedure PROCES, ROUTE is assigned by 1000.

1037 - 1048

Read statement in case that a flight plan compilation is desired along a prescribed track.

This track is specified by graph points indicated by their numbers.

1049 - 1052

Computation of an estimate of flight time to be used for the estimation of other parameters.

The same with distance.

Procedure CTQ makes time instant array DD for each zone(meridian).

Array E is for storing the number of graph points used on a meridian.

1062 - 1065

performs a process for the production of a flight plan.

Actual parameters when calling procedure ;

use landing weight (BB=TRUE).

cost optimization (FFBB=1).

FFBB=0 means fuel opt, FFBB=-1 means time opt.

regularity percentage (PR=0.03).

flight levels used between S1=1 for 31000 and S2=3 for 39000.

S3=1; the value is immaterial if FACTORIZATION is FALSE.

For required flight plans ;

1. when a flight plan for the optimal cost track is needed,

call 'proces (1,3,1,0.03,1,TRUE,FALSE)'.

2. when a flight plan for the optimal fuel track is needed,

call 'proces (1,3,1,0.03,0,TRUE,FALSE)'.

3. when a flight plan for the least time track is needed,

call 'proces (1,3,1,0.03,-1,TRUE,FALSE)'.

For the flight plan 1, 2 or 3 above, FACTORIZATION=FALSE.

For other flight planning simulations, FACTORIZATION=TRUE.

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